

**REMARKS**

Applicants wish to express their appreciation for the Examiner's indication that claims 12-16 are allowed over the art of record and claims 7-11 would be allowable if rewritten to overcome the rejection under 35 U.S.C. 112, second paragraph.

**Summary of the Office Action**

In the Office Action, the title of the invention was objected to for being non-descriptive.

Claims 1-11 stand rejected under 35 U.S.C. § 112, second paragraph.

Claims 1-4 stand rejected under 35 U.S.C. § 103 (a) as being unpatentable over European Patent No. 09 595 42 to *Sugimoto, et al* in view of U.S. Patent No. 6,114,054 to *Klein, et al*.

**Summary of the Response to the Office Action**

By this Amendment, Applicant amends the title of the invention and claim 1.

Accordingly, claims 1-16 are pending for further consideration.

**All Claims are Allowable**

Claims 1-11 were rejected under 35 U.S.C. § 112, second paragraph, as being indefinite for failing to particularly point out and distinctly claim the subject matter which Applicant regards as the invention. The Examiner is thanked for the helpful comments regarding the indefiniteness rejection of independent claim 1. This rejection is respectfully traversed.

Specifically, claim 1 includes reference to the 1993 Japanese Industrial Standard, JIS: Z8721, *Colour specification - Specification according to their three attributes*, hereinafter known as "1993 JIS: Z8721." The 1993 JIS: Z8721 document (an English-language version of Japanese Industrial Standard, 1993 JIS: Z8721 is attached for the Examiner's convenience and for entry into the record) is identified as a document for measuring hue, lightness value, and chroma. Because the claims include this specific 1993 standard, the metes and bounds of the

claim are known and will not vary over time. Accordingly, it is respectfully submitted that the claims are definite, and withdrawal of the rejections under 35 U.S.C. § 112, second is respectfully requested.

**All Subject Matter Complies With 35 U.S.C. § 103(a)**

Claims 1-4 were rejected under 35 U.S.C. § 103(a) as being unpatentable over European Patent No. 09 595 42 to *Sugimoto, et al* in view of U.S. Patent No. 6,114,054 to *Klein, et al*. This rejection is respectfully traversed. Applicant respectfully submits that neither *Sugimoto* nor *Klein* teach or suggest at least a brightness and chroma quality for a marking layer as recited in claim 1.

*Sugimoto* discloses a spark plug glaze layer formed on an alumina-based insulator constructed of materials with very little or no lead (Pb) constituents that demonstrate good resistance to cracking. The glaze can be fired at temperatures as low as 800-950°C, and has excellent flashover resistance. See the abstract of *Sugimoto*.

*Klein* discloses a method for coloring ceramic surfaces that includes the steps of providing a host lattice material composed of a colorless oxide compound that crystallizes into one of a spinel lattice or a rutile lattice and that may be water-soluble; providing an aqueous coloring solution, a first water-soluble compound including a metal ion that is one of a two-valent metal ion or a three-valent metal ion and that colors the host lattice material, and a second water-soluble compound including a metal ion that is one of a five-valent metal ion or six-valent metal ion and that provides a electrostatic balance; and generating a mixed-phase pigment in the surface of the ceramic mass. See the abstract of *Klein*.

To establish a *prima facie* case of obviousness, three basic criteria must be met (see MPEP §§ 2142-2143). First, there must be some suggestion or motivation, either in the references themselves or in the knowledge generally available to one of ordinary skill in the art, to combine reference teachings. Second, there must be a reasonable expectation of success. Third, the prior art references must teach or suggest all the claim limitations.

In the present case, neither *Sugimoto* nor *Klein*, either alone or in combination teach or suggest at least the features of a "glaze layer [which] comprises 5 mol% or less of a Pb . . . the tint of the marking layer seen through the glaze layer is 3 or less in brightness as specified by 1993 JIS: Z8721 as well as 3 or less in chroma" as recited in claim 1. Thus, the Office Action fails to establish a *prima facie* case of obviousness because it does not teach all the recited claim features. Therefore, Applicant respectfully requests that the rejection of claims 1-4 under 35 U.S.C. § 103(a) be withdrawn.

The Office Action states that the "tint of the marking layer seen through the glaze layer...is...inherent provided the marking layer and the glaze layers comprise the same components in the same predetermined mass %." On the contrary, "[t]o establish inherency, the extrinsic evidence must make clear that the missing descriptive matter is necessarily present in the thing described in the reference, and that it would be so recognized by persons of ordinary skill. Inherency, however, may not be established by probabilities or possibilities. The mere fact that a certain thing may result from a given set of circumstances is not sufficient.'" In re Robertson, 169 F.3d 743, 745, 49 USPQ2d 1949, 1950-51 (Fed. Cir. 1999) (citations omitted).

The Office Action does not establish that the brightness and chroma of a marking layer is greatly affected by its composition and that of the glaze layer. Accordingly, for at least this reason, the inherency argument is not supported or sustainable in the Office Action. In addition,

there is no suggestion in the art or extrinsic evidence of record that would indicate that the above recited features of claim 1 are necessarily present in either *Sugimoto* or *Klein et al.* Accordingly, the above recited features of Applicants' claim 1 cannot be considered inherently disclosed by *Sugimoto* or *Klein et al.*

### **CONCLUSION**

In view of the foregoing, Applicant respectfully requests reconsideration and the timely allowance of the pending claims. Should the Examiner feel that there are any issues outstanding after consideration of the response, the Examiner is invited to contact the Applicant's undersigned representative to expedite prosecution.

If there are any other fees due in connection with the filing of this response, please charge the fees to our Deposit Account No. 50-0310. If a fee is required for an extension of time under 37 C.F.R. §1.136 not accounted for above, such an extension is requested and the fee should also be charged to our Deposit Account.

Attached hereto is a marked-up version of the changes made to the specification and/or claims by the current amendment. The attached page is captioned "**Version with markings to show changes made.**"

Respectfully submitted,

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Version With Markings to Show Changes Made

IN THE TITLE:

The title has been amended to read as follows:

-- SPARK PLUG WITH GLAZE AND MARKING --

IN THE CLAIMS:

Claim 1 has been amended as follows:

1. (Amended) A spark plug comprising:

an insulator;

a marking layer formed on a surface of the insulator; and

a glaze layer covering the marking layer so that the marking layer can be seen through the glaze layer,

wherein the glaze layer comprises 5 mol% or less of a Pb component in terms of PbO, and the tint of the marking layer seen through the glaze layer is 3 or less in ~~the~~ brightness as specified by 1993 JIS: Z8721 as well as 3 or less in ~~the~~ chroma as specified by 1993 JIS: Z8721, or 4 or less in ~~the~~ brightness as specified by 1993 JIS: Z8721 as well as 2 or less in ~~the~~ chroma as specified by 1993 JIS: Z8721.

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6.

Fee Payment

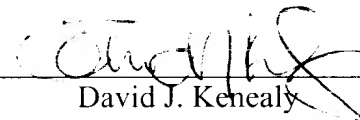
- ☐ No fee is to be paid at this time.
- ☒ Please charge Deposit Amount No. 50-0310 the total amount of \$ 930.00 for the three month extension fee due.. The Commissioner is hereby authorized to charge any additional extension of time fee or additional fee for claims due to Deposit Account No. 50-0310.
- ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, including fees due under 37 C.F.R. §§ 1.16 and 1.17, or credit any overpayment to Deposit Account 50-0310.

Respectfully Submitted,

**MORGAN, LEWIS & BOCKIUS LLP**

Dated: March 31, 2003

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# JIS

## JAPANESE INDUSTRIAL STANDARD

Colour specification —  
Specification according  
to their three attributes

JIS Z 8721—1993

Translated and Published

by

Japanese Standards Association

In the event of any doubt arising,  
the original Standard in Japanese is to be final authority.



JAPANESE INDUSTRIAL STANDARD

JIS Z 8721 :1993

Colour specification—Specification according to their three attributes

February, 1998

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ERRATA

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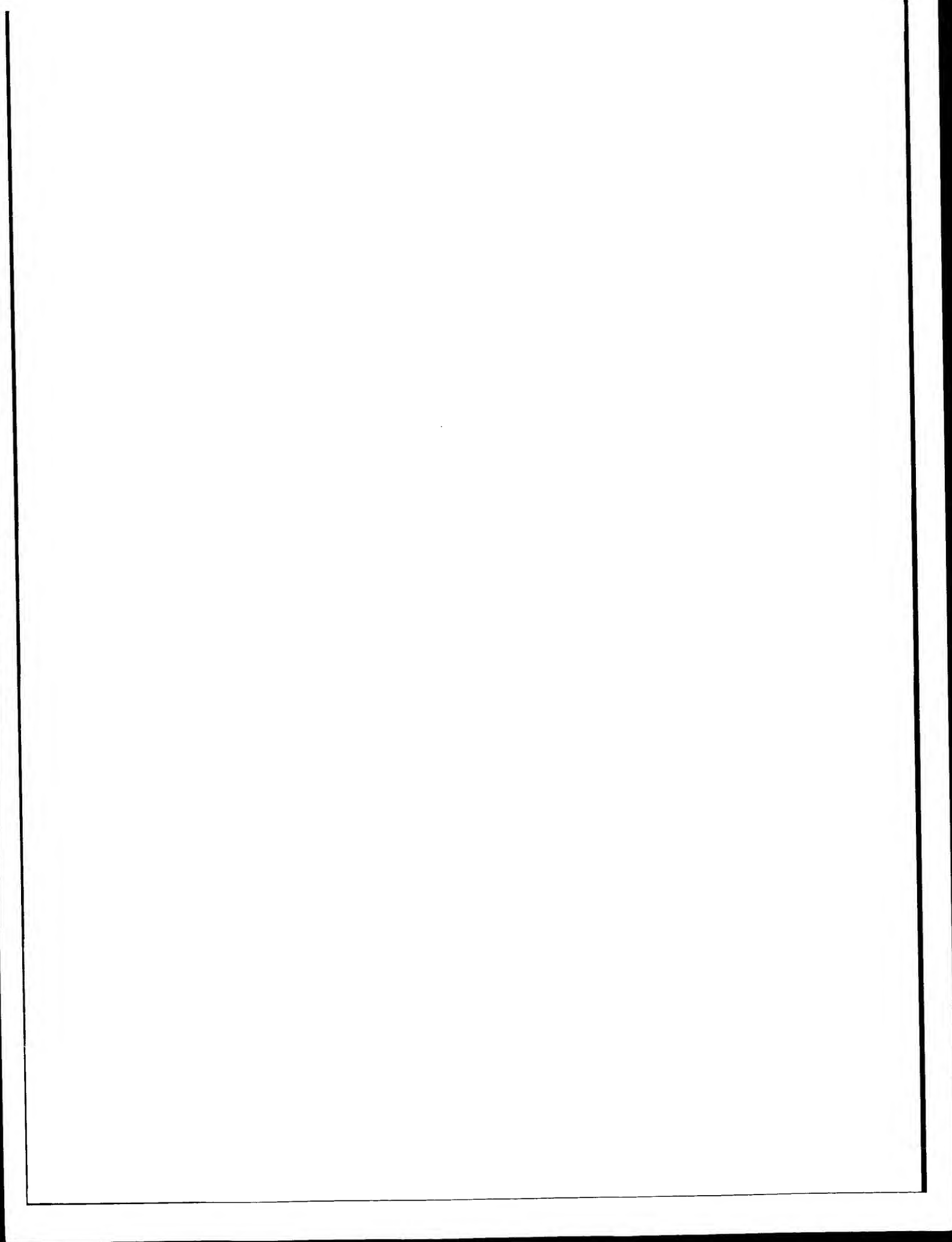
*Page 17*

Attached Table 2 (continued)

In column 3 (right-hand column y of 5.0 GY) in the 14th line from the bottom, replace "0.335 9" with "0.355 9".

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Remarks: This errata is for correcting the first edition of this Standard.  
Japanese Standards Association



## JAPANESE INDUSTRIAL STANDARD

J I S

Colour specification - Specification according  
to their three attributes

Z 8721-1993

1. Scope This Japanese Industrial Standard specifies the system to specify surface colours (hereafter referred to as "colours"), by indicating their three attributes, i.e. hue, lightness, and chroma of colour perception with notations on scales.

Remarks: The following standards are cited in this Standard:

- JIS Z 8105 Glossary of colour terms
- JIS Z 8701 Specification of colours according to the CIE 1931 standard colorimetric system and the CIE 1964 supplementary standard colorimetric system
- JIS Z 8716 Fluorescent lamp as a simulator of CIE standard illuminant D<sub>65</sub> for a visual comparison of surface colours - Type and characteristics
- JIS Z 8719 Evaluation method of degree of metamerism for change in illuminants
- JIS Z 8720 Standard illuminants and sources for colorimetry
- JIS Z 8722 Methods of colour measurement - Reflecting or transmitting objects
- JIS Z 8723 Methods of visual comparison for surface colours
- JIS Z 8741 Method of measurement for specular glossiness

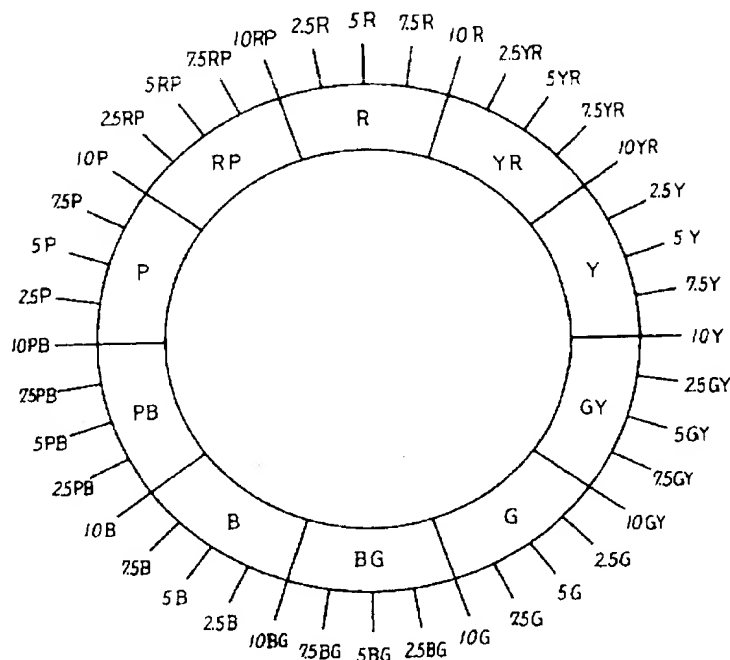
2. Definitions For the purposes of this Standard, the definitions given in JIS Z 8105 and the following definition apply.

Constant hue plane A plane where the colours of constant hue are arranged so as to position in the order of their lightness and chroma.

3. Notation to specify three attributes

3.1 Notation to specify hue Of the attributes of colour perception, the hue  $H$ , scaled perceived hue, as shown in hue circle of Fig. 1 on which lightness and chroma are fixed, shall be notated with symbols shown in the inner circle of Fig. 1 and numerals prefixed to them. The hue circle has been graduated in approximately equal steps of hue perception.

Fig. 1. Graduation of hue circle

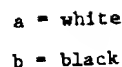


**3.2 Notation to specify lightness** Of the attributes of colour perception, the value  $V$ , scaled perceived lightness, shall be specified by a notation consisting of a numeral shown in Fig. 2. The numerals have been so obtained as shown in Fig. 2, that the entire lightness perception range from ideal black as 0 to ideal white as 10 may be divided on the basis of the achromatic colour into approximately equal steps of lightness perception.

To specify the value of a chromatic colour, the value of an achromatic colour of which luminance factor  $Y_c$  is equivalent to that of the chromatic colour shall be taken.

**3.3 Notation to specify chroma** Of the attributes of colour perception, the chroma  $C$ , scaled perceived chroma, shall be specified by a numeral shown in Fig. 2. The numerals have been so obtained, as shown in Fig. 2, that the colours of a fixed hue and, at the same time, of a fixed value may be arranged to equal step of chroma perception in the sequence of 1, 2, 3, ... of increasing order of chroma, which shall be started at 0 of the achromatic colour.

Z 8721-1993



4.1 Notation to specify colours The notation to specify colors shall be expressed, as shown below, by hue  $H$ , value  $V$  and chroma  $C$  for the chromatic colours and by value  $V$  for the achromatic colours in accordance with the methods shown in 3.1 to 3.3:

- Example 1. 5R4/10 (read 5R, 4, and 10)

**Example 2.** 7.5P 2.5/2.5 (read 7.5P, 2.5 and 2.5).

- When an achromatic colour sensed slightly to be colored is required to be specified including hue and chroma, it shall be done so as written in Example 4 by bracketing with ( ) the main hue  $H$  and chroma  $C$  shown by the symbols in the inner circle of Fig. 1 and in the form of  $NV/(HC)$ .

Example 3. N8

Example 4. N5.5/(R0.3)

4.2 Numerals to be prefixed to notation to specify colours When determining the numerals to be prefixed to the notation to specify respective hue  $H$ , value  $V$  and chroma  $C$ , they shall be integer or down to decimal one place.

5. Basis of the colour system according to three attributes The basis of the colour system according to its three attributes shall be luminance factor  $Y_c$  shown in Attached Tables 1 and 2 and the values of chromaticity coordinates  $x_c$  and  $y_c$  <sup>(1)</sup>.

The relations between the hue and chroma of equal lightness and the values of chromaticity coordinates  $x_c$ ,  $y_c$  are shown in Attached Figs. 1 to 9.

Note <sup>(1)</sup> The values are based on the CIE 1931 standard colorimetric system under the standard illuminant C.

Remarks: The basic values of the CIE 1931 standard colorimetric system under the standard illuminant  $D_{65}$  are given in Annex.

6. Determination of notation to specify colours The notations to specify colours shall be determined by the method (1) or (2) below. For the accurate specifying, the method (1) shall be applied.

- (1) Determination of notation using values  $Y_c$ ,  $x_c$ ,  $y_c$  The determination derived from the values,  $Y_c$ ,  $x_c$  and  $y_c$  shall be made by interpolation or extrapolation<sup>(3)</sup> from the values of chromaticity coordinates  $x_c$ ,  $y_c$  and  $Y_c$  of tristimulus values obtained according to JIS Z 8722<sup>(2)</sup> using Attached Tables 1 and 2.

The measurement shall be performed using values measured under the conditions that regular reflection components shall not be involved.

Notes <sup>(2)</sup> Tables of weighting functions in JIS Z 8719 may be used.

<sup>(3)</sup> Example of calculation by interpolation is shown in Informative reference 1.

- (2) Determination of notation by direct comparison with standard colour atlas The determination by direct comparison with standard colour atlas shall be made by visual comparison with standard colours atlas specified in 7.

The visual comparison shall be made by the method described in JIS Z 8723.

The light sources to be used for illumination shall be as follows:

- (a) Standard source C specified in 4.2.2 of JIS Z 8720.
- (b) Simulator source  $D_{65}$  specified in 4.1 of JIS Z 8723.

(c) Lamp specified in JIS Z 8716.

Remarks: The numerals of notation to specify colours determined by the visual comparison with the standard colour chips are expressed by the numerals corresponding to integer multiple of 0.5 step for hue  $H$ , that of 0.2  $V$  step for value and that of 0.5  $C$  step for chroma.

## 7. Standard colour atlas

7.1 Standard colour atlas The standard colour atlas shall consist of the colour chips according to the basis of the colour system specified in 5.

7.2 Types of standard colour atlas The types of standard colour atlas shall be as described below according to presence or absence of surface gloss in its colour chips.

- (1) Standard colour atlas, matte edition Relative specular glossiness<sup>(\*)</sup> of the colour chips shall be 5 % or less.
- (2) Standard colour atlas, glossary edition Relative specular glossiness<sup>(\*)</sup> of the colour chips shall be 60 % or more.

Note (\*) It shall be in accordance with the method 3 in JIS Z 8741.

7.3 Tolerance on colour of standard colour chips The tolerance on colour of standard colour chips shall be as shown in Table 1.

Table 1. Tolerance on colour of standard colour chips

Colour	Attribute	Tolerance
Achromatic colour	Value	For colour chips exceeding $V = 3.5$ , value $\Delta Y$ corresponding to $\Delta V = \pm 0.1$ .  For colour chips of which Value is not more than $V = 3.5$ , value $\Delta Y$ corresponding to $\Delta V = \pm 0.2$ .
	Chroma	Values $\Delta x$ and $\Delta y$ corresponding to $\Delta C = 0.2$ .
Chromatic colour	Hue	For colour at $C = 6$ or more, values $\Delta x$ and $\Delta y$ corresponding to $\Delta H = \pm 1$ .  For colour chips of which Chroma is less than $C = 6$ , values $\Delta x$ and $\Delta y$ corresponding to $\Delta H = \pm 4/C$ .
	Value	For colour chips exceeding $V = 3.5$ , value $\Delta Y$ corresponding to $\Delta V = \pm 0.1$ .  For colour chips of which Value is not more than $V = 3.5$ , value $\Delta Y$ corresponding to $\Delta V = \pm 0.2$ .
	Chroma	Values $\Delta x$ and $\Delta y$ corresponding to $\Delta C = \pm 0.4$ .

Remarks: The tolerances specified in Table 1 apply to standard colour chips whether matte or glossy.

**7.4 Construction of standard colour atlas** The standard colour atlas shall consist of the standard colour charts and the accessories for colour comparison use, as follows:

- (1) Masks of three types: for high, medium, and low value use
- (2) A colour chart of value scale consisting of 18 colour chips N1 to N9.5 (with 0.5  $V$  steps)
- (3) A colour chart of hue circle consisting of 10 hues 5R to 5RP (with 10  $H$  steps)
- (4) Colour charts of every constant hue, (colour chart based on value and chroma of constant hue). The hue shall be 40 in number as shown in outercircle of Fig. 1; the value of achromatic colour shall be graduated into 8 steps  $V = 2, 3, 4, 5, 6, 7, 8, 9$ ; and the chroma shall be stepped as  $C = 0$  (achromatic), 1, 2, 3, 4, 6, 8, 10, 12 ... to the highest chroma possible.
- (5) Explanatory book
- (6) Other necessary matters

**7.5 Inspection** The standard colours atlas shall be subjected to the tests in accordance with JIS Z 8722 for colour of the standard colour chips. The results shall meet the requirements of 7.3. In addition, the construction of the book of standard colour atlas shall be inspected, and the results shall comply with the requirements of 7.4.



Attached Table 1. Relation between value  $V$  and  $Y_c$  of luminance factor

$V$	$Y_c$	$V$	$Y_c$	$V$	$Y_c$	$V$	$Y_c$	$V$	$Y_c$
0.00	0.000	0.50	0.567	1.00	1.180	1.50	1.971	2.00	3.048
0.01	0.012	0.51	0.579	1.01	1.193	1.51	1.989	2.01	3.073
0.02	0.024	0.52	0.590	1.02	1.207	1.52	2.008	2.02	3.098
0.03	0.036	0.53	0.601	1.03	1.221	1.53	2.026	2.03	3.124
0.04	0.047	0.54	0.613	1.04	1.235	1.54	2.045	2.04	3.149
0.05	0.059	0.55	0.624	1.05	1.249	1.55	2.064	2.05	3.175
0.06	0.071	0.56	0.636	1.06	1.263	1.56	2.083	2.06	3.201
0.07	0.082	0.57	0.647	1.07	1.277	1.57	2.102	2.07	3.227
0.08	0.094	0.58	0.658	1.08	1.291	1.58	2.121	2.08	3.253
0.09	0.106	0.59	0.670	1.09	1.306	1.59	2.141	2.09	3.279
0.10	0.117	0.60	0.682	1.10	1.320	1.60	2.160	2.10	3.306
0.11	0.129	0.61	0.693	1.11	1.334	1.61	2.180	2.11	3.332
0.12	0.140	0.62	0.705	1.12	1.349	1.62	2.199	2.12	3.359
0.13	0.152	0.63	0.716	1.13	1.364	1.63	2.219	2.13	3.386
0.14	0.163	0.64	0.728	1.14	1.378	1.64	2.239	2.14	3.413
0.15	0.174	0.65	0.740	1.15	1.393	1.65	2.259	2.15	3.440
0.16	0.186	0.66	0.751	1.16	1.408	1.66	2.280	2.16	3.468
0.17	0.197	0.67	0.763	1.17	1.423	1.67	2.300	2.17	3.495
0.18	0.208	0.68	0.775	1.18	1.438	1.68	2.320	2.18	3.523
0.19	0.220	0.69	0.787	1.19	1.453	1.69	2.341	2.19	3.551
0.20	0.231	0.70	0.799	1.20	1.468	1.70	2.362	2.20	3.579
0.21	0.242	0.71	0.811	1.21	1.483	1.71	2.383	2.21	3.607
0.22	0.254	0.72	0.823	1.22	1.499	1.72	2.404	2.22	3.636
0.23	0.265	0.73	0.835	1.23	1.514	1.73	2.425	2.23	3.664
0.24	0.276	0.74	0.847	1.24	1.530	1.74	2.446	2.24	3.693
0.25	0.287	0.75	0.859	1.25	1.546	1.75	2.468	2.25	3.722
0.26	0.299	0.76	0.871	1.26	1.561	1.76	2.489	2.26	3.751
0.27	0.310	0.77	0.883	1.27	1.577	1.77	2.511	2.27	3.780
0.28	0.321	0.78	0.896	1.28	1.593	1.78	2.533	2.28	3.809
0.29	0.332	0.79	0.908	1.29	1.609	1.79	2.555	2.29	3.839
0.30	0.343	0.80	0.920	1.30	1.625	1.80	2.577	2.30	3.869
0.31	0.354	0.81	0.933	1.31	1.642	1.81	2.599	2.31	3.899
0.32	0.366	0.82	0.945	1.32	1.658	1.82	2.621	2.32	3.929
0.33	0.377	0.83	0.958	1.33	1.675	1.83	2.644	2.33	3.959
0.34	0.388	0.84	0.970	1.34	1.691	1.84	2.666	2.34	3.989
0.35	0.399	0.85	0.983	1.35	1.708	1.85	2.689	2.35	4.020
0.36	0.410	0.86	0.996	1.36	1.725	1.86	2.712	2.36	4.050
0.37	0.421	0.87	1.008	1.37	1.741	1.87	2.735	2.37	4.081
0.38	0.433	0.88	1.021	1.38	1.758	1.88	2.758	2.38	4.112
0.39	0.444	0.89	1.034	1.39	1.775	1.89	2.782	2.39	4.144
0.40	0.455	0.90	1.047	1.40	1.793	1.90	2.805	2.40	4.175
0.41	0.466	0.91	1.060	1.41	1.810	1.91	2.829	2.41	4.207
0.42	0.477	0.92	1.073	1.42	1.827	1.92	2.852	2.42	4.238
0.43	0.488	0.93	1.086	1.43	1.845	1.93	2.876	2.43	4.270
0.44	0.500	0.94	1.099	1.44	1.863	1.94	2.900	2.44	4.302
0.45	0.511	0.95	1.113	1.45	1.880	1.95	2.925	2.45	4.335
0.46	0.522	0.96	1.126	1.46	1.898	1.96	2.949	2.46	4.367
0.47	0.533	0.97	1.139	1.47	1.916	1.97	2.973	2.47	4.400
0.48	0.545	0.98	1.153	1.48	1.934	1.98	2.998	2.48	4.432
0.49	0.556	0.99	1.166	1.49	1.952	1.99	3.023	2.49	4.465

Attached Table 1. (continued)

V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>
2.50	4.498	3.00	6.391	3.50	8.778	4.00	11.70	4.50	15.19
2.51	4.532	3.01	6.434	3.51	8.831	4.01	11.76	4.51	15.27
2.52	4.565	3.02	6.476	3.52	8.884	4.02	11.83	4.52	15.34
2.53	4.599	3.03	6.520	3.53	8.938	4.03	11.89	4.53	15.42
2.54	4.633	3.04	6.563	3.54	8.991	4.04	11.96	4.54	15.49
2.55	4.667	3.05	6.606	3.55	9.045	4.05	12.02	4.55	15.57
2.56	4.701	3.06	6.650	3.56	9.099	4.06	12.09	4.56	15.65
2.57	4.735	3.07	6.694	3.57	9.154	4.07	12.15	4.57	15.72
2.58	4.770	3.08	6.738	3.58	9.208	4.08	12.22	4.58	15.80
2.59	4.805	3.09	6.783	3.59	9.263	4.09	12.29	4.59	15.88
2.60	4.840	3.10	6.827	3.60	9.318	4.10	12.35	4.60	15.96
2.61	4.875	3.11	6.872	3.61	9.373	4.11	12.42	4.61	16.04
2.62	4.910	3.12	6.917	3.62	9.429	4.12	12.48	4.62	16.11
2.63	4.946	3.13	6.962	3.63	9.485	4.13	12.55	4.63	16.19
2.64	4.981	3.14	7.007	3.64	9.541	4.14	12.62	4.64	16.27
2.65	5.017	3.15	7.053	3.65	9.597	4.15	12.69	4.65	16.35
2.66	5.053	3.16	7.099	3.66	9.653	4.16	12.75	4.66	16.43
2.67	5.089	3.17	7.145	3.67	9.710	4.17	12.82	4.67	16.51
2.68	5.126	3.18	7.191	3.68	9.766	4.18	12.89	4.68	16.59
2.69	5.162	3.19	7.237	3.69	9.823	4.19	12.96	4.69	16.67
2.70	5.199	3.20	7.284	3.70	9.880	4.20	13.03	4.70	16.75
2.71	5.236	3.21	7.330	3.71	9.938	4.21	13.09	4.71	16.83
2.72	5.273	3.22	7.377	3.72	9.996	4.22	13.16	4.72	16.91
2.73	5.311	3.23	7.425	3.73	10.053	4.23	13.23	4.73	16.99
2.74	5.348	3.24	7.472	3.74	10.112	4.24	13.30	4.74	17.07
2.75	5.386	3.25	7.520	3.75	10.170	4.25	13.37	4.75	17.15
2.76	5.424	3.26	7.567	3.76	10.228	4.26	13.44	4.76	17.24
2.77	5.462	3.27	7.615	3.77	10.287	4.27	13.51	4.77	17.32
2.78	5.500	3.28	7.664	3.78	10.346	4.28	13.58	4.78	17.40
2.79	5.539	3.29	7.712	3.79	10.405	4.29	13.65	4.79	17.48
2.80	5.577	3.30	7.761	3.80	10.465	4.30	13.72	4.80	17.57
2.81	5.616	3.31	7.810	3.81	10.524	4.31	13.79	4.81	17.65
2.82	5.655	3.32	7.859	3.82	10.584	4.32	13.87	4.82	17.73
2.83	5.694	3.33	7.908	3.83	10.644	4.33	13.94	4.83	17.82
2.84	5.734	3.34	7.957	3.84	10.705	4.34	14.01	4.84	17.90
2.85	5.773	3.35	8.007	3.85	10.765	4.35	14.08	4.85	17.98
2.86	5.813	3.36	8.057	3.86	10.826	4.36	14.15	4.86	18.07
2.87	5.853	3.37	8.107	3.87	10.887	4.37	14.23	4.87	18.15
2.88	5.893	3.38	8.157	3.88	10.948	4.38	14.30	4.88	18.24
2.89	5.934	3.39	8.208	3.89	11.010	4.39	14.37	4.89	18.32
2.90	5.974	3.40	8.259	3.90	11.071	4.40	14.44	4.90	18.41
2.91	6.015	3.41	8.310	3.91	11.133	4.41	14.52	4.91	18.49
2.92	6.056	3.42	8.361	3.92	11.195	4.42	14.59	4.92	18.58
2.93	6.097	3.43	8.412	3.93	11.257	4.43	14.67	4.93	18.66
2.94	6.138	3.44	8.464	3.94	11.320	4.44	14.74	4.94	18.75
2.95	6.180	3.45	8.516	3.95	11.383	4.45	14.81	4.95	18.84
2.96	6.222	3.46	8.568	3.96	11.446	4.46	14.89	4.96	18.92
2.97	6.264	3.47	8.620	3.97	11.509	4.47	14.96	4.97	19.01
2.98	6.306	3.48	8.672	3.98	11.573	4.48	15.04	4.98	19.10
2.99	6.348	3.49	8.725	3.99	11.636	4.49	15.11	4.99	19.18

Attached Table 1. (continued)

V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>
5.00	19.27	5.50	23.97	6.00	29.30	6.50	35.29	7.00	41.98
5.01	19.36	5.51	24.07	6.01	29.41	6.51	35.42	7.01	42.12
5.02	19.45	5.52	24.17	6.02	29.53	6.52	35.55	7.02	42.27
5.03	19.54	5.53	24.27	6.03	29.64	6.53	35.68	7.03	42.41
5.04	19.62	5.54	24.37	6.04	29.75	6.54	35.80	7.04	42.55
5.05	19.71	5.55	24.47	6.05	29.87	6.55	35.93	7.05	42.69
5.06	19.80	5.56	24.57	6.06	29.98	6.56	36.06	7.06	42.83
5.07	19.89	5.57	24.67	6.07	30.10	6.57	36.19	7.07	42.98
5.08	19.98	5.58	24.78	6.08	30.21	6.58	36.32	7.08	43.12
5.09	20.07	5.59	24.88	6.09	30.33	6.59	36.45	7.09	43.26
5.10	20.16	5.60	24.98	6.10	30.44	6.60	36.58	7.10	43.41
5.11	20.25	5.61	25.08	6.11	30.56	6.61	36.71	7.11	43.55
5.12	20.34	5.62	25.19	6.12	30.68	6.62	36.84	7.12	43.70
5.13	20.43	5.63	25.29	6.13	30.79	6.63	36.97	7.13	43.84
5.14	20.52	5.64	25.39	6.14	30.91	6.64	37.10	7.14	43.99
5.15	20.61	5.65	25.50	6.15	31.03	6.65	37.23	7.15	44.13
5.16	20.71	5.66	25.60	6.16	31.14	6.66	37.36	7.16	44.28
5.17	20.80	5.67	25.71	6.17	31.26	6.67	37.49	7.17	44.42
5.18	20.89	5.68	25.81	6.18	31.38	6.68	37.62	7.18	44.57
5.19	20.98	5.69	25.92	6.19	31.50	6.69	37.75	7.19	44.72
5.20	21.07	5.70	26.02	6.20	31.62	6.70	37.89	7.20	44.86
5.21	21.17	5.71	26.13	6.21	31.74	6.71	38.02	7.21	45.01
5.22	21.26	5.72	26.23	6.22	31.85	6.72	38.15	7.22	45.16
5.23	21.35	5.73	26.34	6.23	31.97	6.73	38.28	7.23	45.30
5.24	21.45	5.74	26.45	6.24	32.09	6.74	38.42	7.24	45.45
5.25	21.54	5.75	26.55	6.25	32.21	6.75	38.55	7.25	45.60
5.26	21.63	5.76	26.66	6.26	32.33	6.76	38.68	7.26	45.75
5.27	21.73	5.77	26.77	6.27	32.45	6.77	38.82	7.27	45.90
5.28	21.82	5.78	26.87	6.28	32.57	6.78	38.95	7.28	46.05
5.29	21.92	5.79	26.98	6.29	32.69	6.79	39.09	7.29	46.20
5.30	22.01	5.80	27.09	6.30	32.82	6.80	39.22	7.30	46.35
5.31	22.11	5.81	27.20	6.31	32.94	6.81	39.36	7.31	46.50
5.32	22.20	5.82	27.31	6.32	33.06	6.82	39.49	7.32	46.65
5.33	22.30	5.83	27.41	6.33	33.18	6.83	39.63	7.33	46.80
5.34	22.40	5.84	27.52	6.34	33.30	6.84	39.77	7.34	46.95
5.35	22.49	5.85	27.63	6.35	33.43	6.85	39.90	7.35	47.10
5.36	22.59	5.86	27.74	6.36	33.55	6.86	40.04	7.36	47.25
5.37	22.69	5.87	27.85	6.37	33.67	6.87	40.18	7.37	47.40
5.38	22.78	5.88	27.96	6.38	33.79	6.88	40.31	7.38	47.56
5.39	22.88	5.89	28.07	6.39	33.92	6.89	40.45	7.39	47.71
5.40	22.98	5.90	28.18	6.40	34.04	6.90	40.59	7.40	47.86
5.41	23.08	5.91	28.29	6.41	34.17	6.91	40.73	7.41	48.01
5.42	23.17	5.92	28.40	6.42	34.29	6.92	40.87	7.42	48.17
5.43	23.27	5.93	28.51	6.43	34.41	6.93	41.00	7.43	48.32
5.44	23.37	5.94	28.63	6.44	34.54	6.94	41.14	7.44	48.48
5.45	23.47	5.95	28.74	6.45	34.66	6.95	41.28	7.45	48.63
5.46	23.57	5.96	28.85	6.46	34.79	6.96	41.42	7.46	48.78
5.47	23.67	5.97	28.96	6.47	34.92	6.97	41.56	7.47	48.94
5.48	23.77	5.98	29.07	6.48	35.04	6.98	41.70	7.48	49.10
5.49	23.87	5.99	29.19	6.49	35.17	6.99	41.84	7.49	49.25

Attached Table 1. (continued)

V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>	V	Y <sub>c</sub>
7.50	49.41	8.00	57.62	8.50	66.68	9.00	76.69	9.50	87.75
7.51	49.56	8.01	57.79	8.51	66.87	9.01	76.90	9.51	87.99
7.52	49.72	8.02	57.96	8.52	67.07	9.02	77.11	9.52	88.22
7.53	49.88	8.03	58.14	8.53	67.26	9.03	77.33	9.53	88.45
7.54	50.03	8.04	58.31	8.54	67.45	9.04	77.54	9.54	88.69
7.55	50.19	8.05	58.48	8.55	67.64	9.05	77.75	9.55	88.92
7.56	50.35	8.06	58.66	8.56	67.83	9.06	77.96	9.56	89.16
7.57	50.51	8.07	58.83	8.57	68.03	9.07	78.18	9.57	89.39
7.58	50.67	8.08	59.01	8.58	68.22	9.08	78.39	9.58	89.63
7.59	50.82	8.09	59.18	8.59	68.41	9.09	78.60	9.59	89.87
7.60	50.98	8.10	59.36	8.60	68.61	9.10	78.82	9.60	90.10
7.61	51.14	8.11	59.54	8.61	68.80	9.11	79.03	9.61	90.34
7.62	51.30	8.12	59.71	8.62	69.00	9.12	79.25	9.62	90.58
7.63	51.46	8.13	59.89	8.63	69.19	9.13	79.46	9.63	90.82
7.64	51.62	8.14	60.07	8.64	69.39	9.14	79.68	9.64	91.06
7.65	51.78	8.15	60.24	8.65	69.58	9.15	79.90	9.65	91.30
7.66	51.95	8.16	60.42	8.66	69.78	9.16	80.11	9.66	91.54
7.67	52.11	8.17	60.60	8.67	69.98	9.17	80.33	9.67	91.78
7.68	52.27	8.18	60.78	8.68	70.17	9.18	80.55	9.68	92.02
7.69	52.43	8.19	60.96	8.69	70.37	9.19	80.77	9.69	92.26
7.70	52.59	8.20	61.14	8.70	70.57	9.20	80.98	9.70	92.50
7.71	52.76	8.21	61.32	8.71	70.77	9.21	81.20	9.71	92.74
7.72	52.92	8.22	61.50	8.72	70.97	9.22	81.42	9.72	92.99
7.73	53.08	8.23	61.68	8.73	71.16	9.23	81.64	9.73	93.23
7.74	53.25	8.24	61.86	8.74	71.36	9.24	81.86	9.74	93.47
7.75	53.41	8.25	62.04	8.75	71.56	9.25	82.08	9.75	93.72
7.76	53.57	8.26	62.22	8.76	71.76	9.26	82.31	9.76	93.96
7.77	53.74	8.27	62.40	8.77	71.97	9.27	82.53	9.77	94.21
7.78	53.90	8.28	62.58	8.78	72.17	9.28	82.75	9.78	94.45
7.79	54.07	8.29	62.77	8.79	72.37	9.29	82.97	9.79	94.70
7.80	54.23	8.30	62.95	8.80	72.57	9.30	83.19	9.80	94.95
7.81	54.40	8.31	63.13	8.81	72.77	9.31	83.42	9.81	95.20
7.82	54.57	8.32	63.32	8.82	72.97	9.32	83.64	9.82	95.44
7.83	54.73	8.33	63.50	8.83	73.18	9.33	83.87	9.83	95.69
7.84	54.90	8.34	63.68	8.84	73.38	9.34	84.09	9.84	95.94
7.85	55.07	8.35	63.87	8.85	73.59	9.35	84.32	9.85	96.19
7.86	55.24	8.36	64.05	8.86	73.79	9.36	84.54	9.86	96.44
7.87	55.40	8.37	64.24	8.87	73.99	9.37	84.77	9.87	96.69
7.88	55.57	8.38	64.43	8.88	74.20	9.38	85.00	9.88	96.94
7.89	55.74	8.39	64.61	8.89	74.40	9.39	85.22	9.89	97.19
7.90	55.91	8.40	64.80	8.90	74.61	9.40	85.45	9.90	97.45
7.91	56.08	8.41	64.99	8.91	74.82	9.41	85.68	9.91	97.70
7.92	56.25	8.42	65.17	8.92	75.02	9.42	85.91	9.92	97.95
7.93	56.42	8.43	65.36	8.93	75.23	9.43	86.14	9.93	98.21
7.94	56.59	8.44	65.55	8.94	75.44	9.44	86.37	9.94	98.46
7.95	56.76	8.45	65.74	8.95	75.65	9.45	86.60	9.95	98.71
7.96	56.93	8.46	65.93	8.96	75.86	9.46	86.83	9.96	98.97
7.97	57.10	8.47	66.11	8.97	76.06	9.47	87.06	9.97	99.23
7.98	57.27	8.48	66.30	8.98	76.27	9.48	87.29	9.98	99.48
7.99	57.45	8.49	66.49	8.99	76.48	9.49	87.52	9.99	99.74
								10.00	100.00

Remarks: The function between the value V and the Y<sub>c</sub> of luminance factor is calculated by the following formula:

In this case it is made under the condition of perfect diffuse surface, two degree visual field and standard illuminant C.

$$Y_c = 1.1913 V - 0.22532 V^2 + 0.23351 V^3 - 0.020483 V^4 + 0.00081936 V^5$$

Attached Table 2. Basis of colour system according to three attributes  
(chromatic colours)

V/C	Y <sub>c</sub> (%)	R							
		2.5 R		5.0 R		7.5 R		10.0 R	
		x	y	x	y	x	y	x	y
9/6	76.69	0.366 5	0.318 3	0.373 4	0.325 6	0.381 2	0.334 8	0.388 0	0.343 9
4		0.344 5	0.317 9	0.349 5	0.322 6	0.355 1	0.328 3	0.360 0	0.334 8
3		0.332 6*	0.317 4*	0.336 1*	0.320 7*	0.340 1*	0.324 5*	0.343 6*	0.328 9*
2		0.321 0	0.316 8	0.324 0	0.318 8	0.326 3	0.321 0	0.328 4	0.323 3
1		0.313 1*	0.316 4*	0.314 8*	0.317 3*	0.315 7*	0.318 1*	0.316 5*	0.318 8*
8/10	57.62	0.412 5	0.316 0	0.424 9	0.327 0	0.438 8	0.341 9	0.449 0	0.358 9
8		0.390 0	0.317 1	0.400 1	0.326 3	0.411 8	0.338 5	0.421 2	0.352 6
6		0.367 1	0.317 5	0.374 3	0.324 8	0.383 0	0.333 5	0.391 0	0.344 2
4		0.346 0	0.317 7	0.351 0	0.322 4	0.356 4	0.327 9	0.362 1	0.334 9
3		0.334 3*	0.317 4*	0.337 7*	0.320 5*	0.341 5*	0.324 4*	0.345 5*	0.329 2*
2		0.323 6	0.316 9	0.325 4	0.318 6	0.327 7	0.321 1	0.330 1	0.323 7
1		0.315 1*	0.316 5*	0.315 7*	0.317 1*	0.316 7*	0.318 3*	0.317 7*	0.319 2*
7/16	41.98	0.488 5	0.303 9	—	—	0.534 1	0.345 2	0.551 9	0.372 9
14		0.466 0	0.308 2	0.484 8	0.323 8	0.505 9	0.345 0	0.523 4	0.370 0
12		0.443 5	0.311 9	0.459 5	0.325 2	0.477 7	0.343 5	0.493 0	0.365 9
10		0.418 3	0.314 4	0.432 0	0.326 0	0.447 0	0.341 3	0.460 0	0.359 6
8		0.396 1	0.316 0	0.406 7	0.325 6	0.419 6	0.338 2	0.430 8	0.353 3
6		0.372 8	0.317 0	0.380 5	0.324 4	0.388 8	0.333 6	0.398 4	0.345 2
4		0.349 9	0.317 1	0.355 2	0.322 2	0.361 1	0.328 2	0.367 1	0.336 0
3		0.338 9*	0.317 1*	0.342 6*	0.320 6*	0.347 0*	0.325 1*	0.351 2*	0.330 6*
2		0.328 4	0.317 0	0.330 6	0.319 0	0.333 5	0.322 0	0.336 0	0.325 3
1		0.318 7*	0.316 8*	0.319 6*	0.317 5*	0.321 0*	0.319 0*	0.322 1*	0.320 4*
6/18	29.30	0.526 2	0.292 8	0.555 2	0.313 8	0.582 9	0.339 6	0.600 9	0.372 0
16		0.504 1	0.298 3	0.529 7	0.317 9	0.556 0	0.342 0	0.574 1	0.371 3
14		0.479 0	0.304 1	0.502 0	0.321 2	0.526 5	0.343 1	0.546 8	0.369 7
12		0.456 8	0.308 2	0.476 0	0.323 4	0.496 1	0.342 8	0.515 0	0.366 7
10		0.432 0	0.311 8	0.448 0	0.325 0	0.465 5	0.341 2	0.481 2	0.361 9
8		0.406 5	0.314 4	0.418 7	0.325 1	0.431 8	0.338 3	0.444 9	0.355 0
6		0.383 2	0.315 8	0.392 1	0.324 4	0.400 0	0.334 0	0.410 3	0.347 3
4		0.356 6	0.316 3	0.362 8	0.322 1	0.369 2	0.329 1	0.376 8	0.338 1
3		0.343 9*	0.316 5*	0.348 2*	0.320 6*	0.353 5*	0.326 1*	0.359 1*	0.332 5*
2		0.331 8	0.316 6	0.334 3	0.319 0	0.338 1	0.322 8	0.341 7	0.326 8
1		0.320 5*	0.316 6*	0.321 4*	0.317 5*	0.323 5*	0.319 5*	0.325 1*	0.321 3*
5/20	19.27	0.578 4	0.271 9	0.614 2	0.297 0	0.638 8	0.321 6	—	—
18		0.554 0	0.280 4	0.591 8	0.303 8	0.616 1	0.327 7	0.629 7	0.364 2
16		0.530 0	0.288 0	0.563 7	0.310 2	0.590 1	0.333 1	0.603 7	0.365 7
14		0.504 7	0.295 0	0.534 1	0.315 8	0.559 0	0.337 0	0.577 1	0.366 4
12		0.482 0	0.300 2	0.507 1	0.319 4	0.528 0	0.338 9	0.548 1	0.366 0
10		0.453 3	0.305 8	0.474 7	0.322 7	0.492 7	0.339 9	0.511 3	0.363 0
8		0.425 2	0.310 1	0.441 3	0.324 0	0.456 3	0.338 7	0.471 3	0.357 5
6		0.396 0	0.313 0	0.407 8	0.323 8	0.418 0	0.334 8	0.429 9	0.349 9
4		0.366 0	0.314 8	0.374 0	0.322 0	0.380 6	0.329 4	0.387 9	0.339 8
3		0.350 7*	0.315 4*	0.356 3*	0.320 7*	0.361 2*	0.326 2*	0.366 8*	0.333 9*
2		0.336 0	0.315 8	0.339 2	0.319 2	0.342 5	0.322 9	0.346 5	0.327 8
1		0.322 3*	0.316 1*	0.323 5*	0.317 7*	0.325 2*	0.319 6*	0.327 4*	0.321 8*
4/20	11.70	—	—	—	—	0.680 6	0.298 8	—	—
18		0.589 8	0.262 2	0.632 9	0.288 1	0.653 8	0.310 0	—	—
16		0.562 0	0.272 4	0.603 9	0.297 8	0.626 0	0.319 2	0.640 9	0.353 3
14		0.536 9	0.281 0	0.573 4	0.305 7	0.595 9	0.326 9	0.615 4	0.356 8
12		0.507 2	0.289 7	0.538 5	0.312 9	0.560 3	0.332 1	0.580 1	0.353 8
10		0.477 4	0.296 9	0.504 3	0.317 6	0.523 5	0.335 1	0.541 8	0.358 0
8		0.447 2	0.303 1	0.469 0	0.320 9	0.485 0	0.335 9	0.499 5	0.355 7
6		0.414 1	0.308 5	0.429 9	0.322 6	0.441 5	0.334 0	0.453 5	0.350 0
4		0.380 6	0.312 5	0.391 6	0.322 3	0.399 0	0.330 0	0.407 8	0.341 2
3		0.363 5*	0.313 9*	0.371 3*	0.321 4*	0.376 5*	0.327 0*	0.383 2*	0.335 6*
2		0.346 1	0.315 0	0.350 8	0.320 0	0.353 8	0.323 6	0.358 2	0.329 4
1		0.328 3*	0.315 8*	0.330 3*	0.318 3*	0.331 5*	0.320 0*	0.333 6*	0.322 9*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	R							
		2.5 R		5.0 R		7.5 R		10.0 R	
		x	y	x	y	x	y	x	y
3/16	6.391	0.611 6	0.245 6	0.652 0	0.266 0	0.681 7	0.287 2	—	—
14		0.582 8	0.257 9	0.620 4	0.278 9	0.649 2	0.301 2	0.670 3	0.324 9
12		0.553 6	0.269 1	0.588 4	0.290 4	0.615 8	0.312 9	0.632 2	0.336 1
10		0.519 1	0.281 1	0.550 0	0.302 4	0.573 0	0.324 0	0.587 1	0.344 0
8		0.482 1	0.291 8	0.506 4	0.311 4	0.525 1	0.329 7	0.539 3	0.347 7
6		0.440 9	0.300 9	0.459 2	0.316 8	0.473 8	0.331 6	0.485 4	0.346 7
4		0.402 1	0.307 6	0.414 8	0.319 0	0.424 0	0.330 2	0.430 8	0.341 2
3		0.381 2*	0.310 5*	0.390 3*	0.319 3*	0.397 1*	0.327 9*	0.402 3*	0.336 9*
2		0.359 1	0.313 0	0.364 5	0.319 0	0.369 0	0.324 8	0.372 8	0.331 4
1		0.335 5*	0.315 0*	0.337 7*	0.318 0*	0.340 0*	0.320 9*	0.342 1*	0.324 6*
2/14	3.048	0.573 4	0.208 3	0.630 2	0.228 7	0.679 1	0.252 0	0.716 5	0.273 4
12		0.543 8	0.225 4	0.593 0	0.246 5	0.639 2	0.270 4	0.673 2	0.293 7
10		0.512 2	0.242 8	0.555 7	0.263 3	0.595 2	0.287 4	0.624 7	0.312 0
8		0.477 6	0.259 3	0.514 3	0.280 0	0.543 3	0.302 7	0.571 3	0.325 9
6		0.439 0	0.276 0	0.464 2	0.293 4	0.487 5	0.312 3	0.509 5	0.333 1
4		0.402 1	0.290 0	0.418 4	0.303 2	0.433 5	0.316 9	0.448 1	0.333 0
3		0.382 7*	0.296 7*	0.394 6*	0.307 4*	0.405 0*	0.317 9*	0.415 2*	0.330 9*
2		0.361 4	0.303 3	0.369 2	0.311 1	0.375 1	0.318 1	0.381 1	0.327 4
1		0.337 5*	0.309 8*	0.341 3*	0.314 1*	0.343 6*	0.317 6*	0.346 0*	0.322 5*
1/10	1.180	0.505 8	0.190 0	0.560 4	0.210 0	0.611 1	0.229 0	0.666 1	0.249 9
8		0.481 2	0.210 3	0.528 2	0.229 7	0.572 2	0.248 7	0.617 8	0.271 3
6		0.451 5	0.232 9	0.488 5	0.251 5	0.523 5	0.269 8	0.558 4	0.292 1
4		0.416 6	0.256 9	0.442 0	0.272 8	0.466 0	0.288 8	0.493 3	0.306 8
3		0.398 7*	0.268 6*	0.418 5*	0.282 7*	0.436 2*	0.296 5*	0.455 4*	0.312 0*
2		0.376 8	0.281 6	0.390 8	0.292 9	0.402 0	0.303 4	0.412 8	0.315 4
1		0.348 2*	0.297 1*	0.355 7*	0.303 9*	0.360 9*	0.309 9*	0.364 7*	0.316 9*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	YR							
		2.5 YR		5.0 YR		7.5 YR		10.0 YR	
		x	y	x	y	x	y	x	y
9/ 8	76.69	—	—	—	—	0.422 0	0.393 0	0.419 9	0.406 9
6		0.392 7	0.355 0	0.394 8	0.365 9	0.395 0	0.376 3	0.394 1	0.387 7
4		0.364 1	0.342 2	0.366 8	0.350 9	0.367 9	0.358 5	0.367 7	0.366 8
3		0.347 6*	0.334 6*	0.350 9*	0.341 8*	0.353 0*	0.348 3*	0.353 6*	0.355 3*
2		0.332 0	0.327 3	0.335 3	0.332 5	0.338 0	0.337 7	0.339 2	0.343 0
1		0.318 9*	0.320 9*	0.321 3*	0.323 8*	0.323 5*	0.326 9*	0.324 6*	0.330 0*
8/20	57.62	—	—	—	—	0.539 1	0.451 8	0.524 5	0.470 9
18		—	—	—	—	0.531 6	0.448 0	0.517 9	0.467 0
16		—	—	—	—	0.519 5	0.442 4	0.507 9	0.461 3
14		—	—	0.508 8	0.414 5	0.502 5	0.433 8	0.494 0	0.453 0
12		0.485 2	0.384 7	0.484 9	0.405 0	0.481 6	0.423 2	0.475 3	0.441 4
10		0.455 2	0.376 1	0.457 6	0.393 8	0.456 8	0.410 0	0.452 7	0.426 8
8		0.427 5	0.366 2	0.431 0	0.382 0	0.430 6	0.395 2	0.428 0	0.410 2
6		0.396 0	0.354 7	0.398 8	0.366 3	0.400 0	0.377 0	0.399 4	0.389 6
4		0.366 7	0.342 9	0.369 0	0.351 0	0.369 9	0.358 6	0.370 1	0.367 4
3		0.349 7*	0.335 2*	0.353 0*	0.342 1*	0.354 7*	0.348 4*	0.355 5*	0.355 7*
2		0.333 4	0.327 6	0.337 3	0.333 0	0.339 5	0.337 9	0.340 7	0.343 4
1		0.319 6*	0.321 0*	0.322 7*	0.324 2*	0.324 6*	0.327 1*	0.325 6*	0.330 3*
7/20	41.98	0.582 4	0.404 6	0.565 7	0.429 8	—	—	—	—
18		0.569 5	0.402 4	0.556 4	0.426 7	0.541 7	0.449 2	0.527 6	0.470 0
16		0.552 2	0.398 9	0.543 7	0.422 8	0.531 9	0.444 9	0.518 8	0.465 0
14		0.529 7	0.393 8	0.525 2	0.416 8	0.517 4	0.438 1	0.507 4	0.458 1
12		0.500 1	0.386 1	0.500 7	0.408 1	0.497 0	0.428 2	0.490 0	0.448 0
10		0.467 1	0.376 8	0.471 1	0.397 2	0.470 4	0.415 1	0.466 7	0.433 5
8		0.437 1	0.367 9	0.440 2	0.384 2	0.441 5	0.399 6	0.439 9	0.416 4
6		0.405 3	0.357 0	0.409 1	0.370 1	0.410 7	0.382 0	0.410 2	0.396 0
4		0.371 5	0.343 9	0.375 0	0.353 0	0.377 2	0.361 3	0.377 8	0.371 9
3		0.355 1*	0.336 9*	0.358 4*	0.344 0*	0.360 5*	0.350 7*	0.361 2*	0.359 0*
2		0.339 2	0.329 8	0.342 1	0.334 9	0.343 7	0.339 7	0.344 3	0.345 4
1		0.324 1*	0.322 9*	0.326 0*	0.325 6*	0.326 9*	0.328 3*	0.327 3*	0.331 2*
6/18	29.30	0.587 9	0.402 1	0.571 5	0.427 0	—	—	—	—
16		0.569 8	0.399 0	0.559 7	0.423 9	0.546 8	0.447 8	—	—
14		0.548 8	0.394 7	0.542 3	0.418 8	0.532 0	0.441 2	0.520 0	0.462 3
12		0.521 5	0.388 7	0.519 9	0.411 9	0.514 5	0.433 1	0.505 0	0.453 6
10		0.489 1	0.380 6	0.492 1	0.402 2	0.490 4	0.422 0	0.484 3	0.441 6
8		0.453 3	0.370 8	0.459 2	0.390 0	0.459 6	0.406 4	0.457 0	0.424 9
6		0.418 0	0.360 0	0.422 9	0.375 0	0.424 2	0.387 6	0.424 0	0.403 0
4		0.380 6	0.346 7	0.384 0	0.356 4	0.386 0	0.365 2	0.386 1	0.376 7
3		0.362 8*	0.339 6*	0.365 6*	0.347 0*	0.367 4*	0.353 9*	0.367 7*	0.362 9*
2		0.345 3	0.332 1	0.347 4	0.337 3	0.348 7	0.342 1	0.349 1	0.348 3
1		0.327 8*	0.324 3*	0.329 0*	0.327 1*	0.329 7*	0.329 7*	0.330 0*	0.332 8*
5/16	19.27	0.593 3	0.398 9	—	—	—	—	—	—
14		0.573 1	0.395 3	0.564 2	0.420 1	0.550 6	0.445 0	—	—
12		0.548 2	0.390 9	0.542 2	0.414 1	0.533 5	0.437 8	0.521 1	0.460 0
10		0.517 5	0.384 4	0.516 1	0.406 4	0.510 8	0.427 6	0.502 5	0.448 9
8		0.479 5	0.375 8	0.483 0	0.396 0	0.482 0	0.414 1	0.477 0	0.433 8
6		0.436 5	0.364 0	0.442 0	0.380 8	0.444 0	0.395 4	0.442 8	0.412 8
4		0.392 5	0.349 4	0.396 8	0.361 4	0.399 1	0.371 4	0.399 5	0.384 0
3		0.371 3*	0.341 7*	0.374 8*	0.350 7*	0.376 5*	0.358 2*	0.377 1*	0.368 1*
2		0.350 6	0.333 7	0.353 0	0.339 5	0.354 0	0.344 5	0.354 6	0.351 4
1		0.330 2*	0.325 2*	0.331 5*	0.328 0*	0.331 8*	0.330 5*	0.332 2*	0.334 1*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	YR							
		2.5 YR		5.0 YR		7.5 YR		10.0 YR	
		x	y	x	y	x	y	x	y
4/12	11.70	0.580 9	0.391 0	0.572 9	0.416 9	—	—	—	—
10		0.547 5	0.385 6	0.543 2	0.409 7	0.535 6	0.434 2	0.525 0	0.457 3
8		0.507 1	0.377 7	0.507 0	0.399 4	0.503 8	0.420 4	0.496 5	0.441 4
6		0.461 2	0.367 4	0.465 1	0.385 9	0.465 5	0.402 9	0.461 8	0.421 3
4		0.414 1	0.353 9	0.418 7	0.367 9	0.420 8	0.380 9	0.418 9	0.394 8
3		0.388 6*	0.345 7*	0.392 4*	0.356 7*	0.394 2*	0.366 4*	0.393 3*	0.377 9*
2		0.362 4	0.336 7	0.365 1	0.344 2	0.366 2	0.350 4	0.366 0	0.359 0
1		0.336 1*	0.326 9*	0.337 4*	0.330 7*	0.337 8*	0.333 5*	0.338 0*	0.338 4*
3/10	6.391	0.594 1	0.381 8	—	—	—	—	—	—
8		0.547 5	0.377 1	0.545 6	0.404 0	0.539 0	0.430 6	0.530 5	0.455 9
6		0.495 4	0.369 2	0.496 6	0.390 8	0.493 0	0.411 6	0.487 2	0.432 6
4		0.436 0	0.356 3	0.437 6	0.371 5	0.437 8	0.386 5	0.434 1	0.401 8
3		0.406 2*	0.348 3*	0.407 9*	0.360 3*	0.408 2*	0.371 5*	0.405 1*	0.383 4*
2		0.375 7	0.339 1	0.377 1	0.347 6	0.377 1	0.354 9	0.374 7	0.363 0
1		0.343 8*	0.328 5*	0.344 7*	0.333 0*	0.344 4*	0.336 5*	0.343 0*	0.340 6*
2/ 8	3.048	0.599 5	0.359 0	—	—	—	—	—	—
6		0.528 0	0.358 1	0.542 6	0.392 5	0.547 5	0.427 1	—	—
4		0.459 8	0.350 8	0.467 4	0.373 8	0.469 0	0.396 4	0.467 6	0.416 8
3		0.422 9*	0.344 5*	0.427 9*	0.361 5*	0.429 0*	0.378 5*	0.427 0*	0.393 4*
2		0.385 2	0.336 5	0.388 0	0.347 6	0.388 9	0.359 0	0.387 2	0.368 8
1		0.347 3*	0.327 1*	0.348 5*	0.332 4*	0.349 2*	0.338 2*	0.348 2*	0.343 1*
1/ 8	1.180	0.672 1	0.305 8	—	—	—	—	—	—
6		0.604 8	0.327 0	—	—	—	—	—	—
4		0.531 1	0.337 1	0.566 0	0.379 5	—	—	—	—
3		0.481 1*	0.337 5*	0.501 8*	0.371 3*	—	—	—	—
2		0.425 8	0.334 4	0.437 7	0.358 0	0.443 0	0.377 5	0.444 6	0.398 2
1		0.367 9*	0.327 4*	0.369 6*	0.338 0*	0.366 5*	0.344 0*	0.362 5*	0.349 0*



Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	Y							
		2.5 Y		5.0 Y		7.5 Y		10.0 Y	
		x	y	x	y	x	y	x	y
9/20	76.69	—	—	0.483 0	0.509 2	—	—	—	—
18		—	—	0.478 2	0.504 9	0.466 3	0.518 8	0.454 0	0.532 0
16		—	—	0.471 1	0.497 7	0.459 5	0.510 4	0.447 7	0.522 5
14		—	—	0.460 2	0.486 9	0.450 3	0.499 3	0.439 3	0.510 1
12		0.456 9	0.452 7	0.445 5	0.471 9	0.436 9	0.482 9	0.427 1	0.492 0
10		0.437 0	0.436 9	0.427 5	0.452 9	0.420 1	0.462 2	0.412 0	0.469 4
8		0.415 4	0.418 6	0.408 0	0.431 9	0.401 9	0.439 2	0.395 7	0.445 0
6		0.391 0	0.397 2	0.385 8	0.407 1	0.381 1	0.412 3	0.376 1	0.415 5
4		0.365 5	0.373 8	0.362 1	0.379 9	0.359 1	0.383 2	0.355 8	0.385 2
3		0.352 5*	0.361 0*	0.350 2*	0.365 6*	0.348 1*	0.368 4*	0.345 6*	0.369 9*
2		0.339 0	0.347 2	0.337 8	0.350 4	0.336 5	0.352 7	0.334 9	0.353 7
1		0.324 9*	0.332 4*	0.324 5*	0.334 1*	0.324 0*	0.335 5*	0.323 2*	0.336 0*
8/20	57.62	0.509 1	0.490 0	—	—	—	—	—	—
18		0.503 3	0.485 5	0.484 7	0.506 9	0.470 9	0.522 0	0.457 0	0.536 6
16		0.495 7	0.480 0	0.479 1	0.501 2	0.465 3	0.515 8	0.452 5	0.529 5
14		0.484 2	0.471 2	0.469 9	0.492 0	0.457 4	0.506 2	0.445 0	0.518 1
12		0.467 8	0.458 9	0.456 2	0.478 8	0.445 5	0.491 7	0.434 1	0.502 0
10		0.446 9	0.442 3	0.437 6	0.460 1	0.428 3	0.471 2	0.419 0	0.479 1
8		0.423 1	0.423 1	0.415 8	0.437 8	0.408 8	0.446 6	0.400 8	0.452 0
6		0.396 9	0.400 9	0.391 3	0.411 7	0.386 2	0.417 5	0.380 3	0.421 6
4		0.368 4	0.375 1	0.365 0	0.382 6	0.362 2	0.386 1	0.358 1	0.388 3
3		0.354 6*	0.362 1*	0.352 4*	0.367 6*	0.350 3*	0.370 4*	0.347 2*	0.372 1*
2		0.340 6	0.348 4	0.339 4	0.351 8	0.337 9	0.354 0	0.335 9	0.355 2
1		0.325 9*	0.333 3*	0.325 5*	0.334 8*	0.324 6*	0.336 2*	0.323 7*	0.336 9*
7/16	41.98	0.504 9	0.484 3	0.487 5	0.504 7	0.472 8	0.521 5	0.458 2	0.537 5
14		0.495 0	0.477 3	0.479 1	0.496 5	0.465 2	0.512 8	0.451 6	0.527 7
12		0.480 6	0.466 6	0.467 7	0.485 7	0.454 7	0.500 5	0.442 0	0.513 1
10		0.460 6	0.451 6	0.450 9	0.469 6	0.440 0	0.483 0	0.428 9	0.493 7
8		0.435 3	0.431 2	0.427 1	0.446 2	0.418 4	0.456 8	0.409 0	0.464 1
6		0.407 3	0.407 3	0.400 9	0.419 8	0.394 3	0.426 4	0.386 4	0.430 5
4		0.376 1	0.380 0	0.371 8	0.388 5	0.367 7	0.392 5	0.362 4	0.395 1
3		0.360 0*	0.365 8*	0.357 0*	0.371 7*	0.353 8*	0.374 5*	0.349 8*	0.376 3*
2		0.343 6	0.350 7	0.341 9	0.354 0	0.339 6	0.355 8	0.336 9	0.356 9
1		0.327 0*	0.334 3*	0.326 3*	0.335 6*	0.325 0*	0.336 4*	0.323 7*	0.336 9*
6/14	29.30	0.506 1	0.482 9	0.490 5	0.503 8	0.475 4	0.522 0	0.459 3	0.539 2
12		0.492 8	0.473 0	0.478 0	0.492 0	0.463 8	0.508 7	0.448 8	0.523 7
10		0.476 0	0.460 7	0.463 9	0.479 0	0.451 2	0.494 3	0.437 2	0.506 8
8		0.451 7	0.442 1	0.442 6	0.458 8	0.432 1	0.471 9	0.420 1	0.481 2
6		0.420 3	0.417 6	0.414 0	0.430 5	0.406 0	0.440 0	0.396 0	0.445 2
4		0.384 0	0.386 7	0.379 4	0.395 5	0.374 5	0.400 4	0.367 9	0.403 3
3		0.366 1*	0.370 8*	0.362 6*	0.377 2*	0.358 9*	0.380 5*	0.354 0*	0.382 4*
2		0.348 0	0.354 0	0.345 7	0.358 0	0.343 1	0.360 1	0.339 8	0.361 1
1		0.329 4*	0.336 0*	0.328 3*	0.337 8*	0.326 9*	0.338 8*	0.325 2*	0.339 2*
5/12	19.27	0.508 2	0.481 2	0.493 2	0.501 9	0.476 7	0.520 8	0.459 0	0.539 0
10		0.490 5	0.468 3	0.477 7	0.487 6	0.463 2	0.505 7	0.446 8	0.520 9
8		0.468 5	0.452 4	0.457 9	0.469 2	0.445 0	0.485 0	0.430 7	0.496 7
6		0.438 0	0.429 2	0.430 2	0.443 5	0.419 9	0.455 1	0.407 2	0.462 1
4		0.396 8	0.395 4	0.391 5	0.405 7	0.385 0	0.412 0	0.376 2	0.415 8
3		0.375 2*	0.376 6*	0.370 8*	0.384 3*	0.366 1*	0.388 3*	0.359 3*	0.390 4*
2		0.353 4	0.357 0	0.350 0	0.362 0	0.347 0	0.364 0	0.342 2	0.364 8
1		0.331 6*	0.336 8*	0.329 6*	0.339 2*	0.328 2*	0.339 8*	0.325 6*	0.339 8*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	Y							
		2.5 Y		5.0 Y		7.5 Y		10.0 Y	
		x	y	x	y	x	y	x	y
4/10	11.70	0.512 0	0.480 0	—	—	—	—	—	—
8		0.486 5	0.462 5	0.474 5	0.481 0	0.459 5	0.499 0	0.443 0	0.515 3
6		0.454 2	0.439 1	0.445 1	0.455 0	0.433 1	0.468 8	0.419 0	0.479 5
4		0.413 8	0.407 6	0.406 9	0.418 8	0.398 2	0.427 2	0.387 1	0.432 1
3		0.389 3*	0.387 6*	0.383 6*	0.395 5*	0.376 8*	0.400 9*	0.367 7*	0.403 2*
2		0.363 3	0.365 4	0.359 0	0.370 1	0.354 2	0.372 7	0.347 6	0.373 2
1		0.336 6*	0.341 5*	0.334 1*	0.343 4*	0.331 6*	0.344 1*	0.328 0*	0.343 7*
3/ 6	6.391	0.478 4	0.453 1	0.467 0	0.471 1	0.452 6	0.488 9	0.434 5	0.502 6
4		0.427 7	0.416 6	0.419 1	0.428 3	0.408 6	0.437 9	0.396 1	0.445 2
3		0.399 6*	0.394 4*	0.392 3*	0.402 5*	0.384 1*	0.408 5*	0.373 9*	0.412 4*
2		0.370 3	0.370 0	0.364 6	0.374 8	0.358 9	0.377 8	0.351 3	0.378 9
1		0.340 3*	0.343 9*	0.336 9*	0.345 8*	0.334 0*	0.346 7*	0.329 6*	0.346 4*
2/ 4	3.048	0.462 7	0.439 2	0.454 3	0.457 3	0.440 1	0.472 3	0.418 8	0.478 9
3		0.421 6*	0.409 0*	0.413 4*	0.419 9*	0.400 8*	0.426 9*	0.385 0*	0.428 7*
2		0.382 5	0.378 5	0.375 7	0.383 9	0.366 0	0.385 8	0.355 6	0.384 8
1		0.345 3*	0.347 6*	0.341 3*	0.349 4*	0.335 8*	0.348 9*	0.330 6*	0.347 4*
1/ 2	1.180	0.436 2	0.417 7	0.423 0	0.426 5	0.404 2	0.428 7	0.380 2	0.421 2
1		0.355 3*	0.353 0*	0.347 9*	0.353 3*	0.340 6*	0.352 4*	0.333 2*	0.350 3*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	GY							
		2.5 GY		5.0 GY		7.5 GY		10.0 GY	
		x	y	x	y	x	y	x	y
9/18	76.69	0.435 4	0.550 8	0.410 8	0.569 9	0.360 2	0.592 0	0.303 2	0.574 8
16		0.428 8	0.538 3	0.405 8	0.554 1	0.358 1	0.565 4	0.307 9	0.544 0
14		0.421 2	0.523 7	0.399 3	0.532 9	0.355 1	0.533 9	0.311 5	0.512 9
12		0.410 8	0.502 8	0.391 1	0.508 2	0.351 8	0.504 2	0.313 9	0.482 9
10		0.397 3	0.476 1	0.381 0	0.479 1	0.347 1	0.473 5	0.315 5	0.455 8
8		0.383 4	0.449 0	0.369 8	0.449 7	0.341 4	0.441 5	0.315 7	0.425 9
6		0.367 0	0.417 8	0.357 2	0.417 9	0.335 1	0.411 1	0.315 3	0.400 8
4		0.349 9	0.386 6	0.343 7	0.386 1	0.327 4	0.379 3	0.314 4	0.371 1
3		0.341 3*	0.370 7*	0.336 4*	0.370 1*	0.323 7*	0.364 8*	0.313 5*	0.358 2*
2		0.332 1	0.353 9	0.328 4	0.353 4	0.319 8	0.350 0	0.312 4	0.345 4
1		0.321 8*	0.335 9*	0.319 7*	0.335 6*	0.315 4*	0.334 1*	0.311 2*	0.331 7*
8/24	57.62	—	—	—	—	—	—	0.278 1	0.684 0
22		—	—	—	—	—	—	0.284 6	0.656 4
20		—	—	0.412 7	0.585 5	0.359 2	0.623 5	0.291 8	0.625 5
18		0.437 1	0.555 7	0.410 4	0.578 5	0.358 5	0.606 3	0.298 7	0.591 9
16		0.432 7	0.547 5	0.406 1	0.564 1	0.356 9	0.579 8	0.304 3	0.557 8
14		0.426 1	0.534 4	0.401 1	0.546 8	0.354 6	0.549 0	0.309 1	0.524 7
12		0.415 4	0.513 3	0.392 4	0.519 9	0.351 1	0.514 4	0.312 4	0.492 6
10		0.402 1	0.486 9	0.381 6	0.487 9	0.346 3	0.479 1	0.314 0	0.460 1
8		0.385 8	0.455 0	0.369 6	0.454 2	0.340 8	0.445 2	0.314 9	0.428 4
6		0.369 0	0.423 0	0.357 3	0.421 4	0.333 9	0.412 9	0.315 0	0.401 4
4		0.350 4	0.388 7	0.343 3	0.387 2	0.326 6	0.380 9	0.314 0	0.372 7
3		0.341 8*	0.372 4*	0.336 1*	0.370 9*	0.323 1*	0.365 7*	0.313 1*	0.359 4*
2		0.332 7	0.355 5	0.328 4	0.354 2	0.319 4	0.350 2	0.312 1	0.345 9
1		0.322 4*	0.337 1*	0.319 8*	0.336 2*	0.315 2*	0.333 9*	0.311 1*	0.331 7*
7/22	41.98	—	—	—	—	—	—	0.272 8	0.689 3
20		—	—	—	—	—	—	0.281 6	0.656 3
18		—	—	—	—	0.355 5	0.624 2	0.290 5	0.618 6
16		0.436 6	0.557 8	0.407 6	0.578 3	0.354 9	0.600 0	0.298 1	0.583 5
14		0.430 9	0.545 9	0.402 7	0.561 5	0.353 2	0.570 0	0.304 7	0.545 8
12		0.421 3	0.527 0	0.394 9	0.536 7	0.350 2	0.532 8	0.309 2	0.509 5
10		0.409 1	0.503 0	0.385 2	0.505 1	0.346 1	0.495 0	0.312 3	0.473 2
8		0.391 9	0.468 4	0.372 2	0.466 9	0.340 6	0.455 8	0.314 0	0.438 7
6		0.372 8	0.431 6	0.358 1	0.429 1	0.334 1	0.419 1	0.314 2	0.405 8
4		0.353 4	0.395 3	0.343 7	0.392 9	0.326 7	0.384 8	0.313 3	0.376 4
3		0.343 3*	0.376 4*	0.336 3*	0.374 6*	0.322 9*	0.368 3*	0.312 5*	0.361 7*
2		0.332 8	0.356 9	0.328 4	0.335 9	0.319 0	0.351 6	0.311 7	0.346 9
1		0.321 8*	0.336 9*	0.319 8*	0.336 5*	0.314 8*	0.334 4*	0.310 9*	0.331 8*
6/20	29.30	—	—	—	—	—	—	0.264 8	0.700 4
18		—	—	—	—	—	—	0.276 3	0.661 6
16		—	—	—	—	0.349 8	0.628 2	0.287 2	0.619 9
14		0.435 4	0.559 4	0.404 2	0.578 8	0.349 8	0.598 5	0.296 2	0.580 2
12		0.426 9	0.541 4	0.398 0	0.556 4	0.348 8	0.559 6	0.303 7	0.535 8
10		0.415 9	0.519 0	0.389 1	0.526 4	0.346 3	0.519 6	0.308 6	0.494 9
8		0.400 6	0.488 5	0.377 2	0.488 0	0.341 8	0.476 8	0.311 6	0.456 3
6		0.379 9	0.447 0	0.362 2	0.443 8	0.335 1	0.432 1	0.312 8	0.417 5
4		0.357 2	0.403 8	0.346 1	0.400 8	0.327 5	0.392 2	0.312 4	0.382 2
3		0.345 8*	0.382 3*	0.337 6*	0.380 0*	0.323 5*	0.373 5*	0.311 8*	0.365 8*
2		0.334 2	0.360 7	0.328 8	0.359 2	0.319 3	0.355 0	0.311 2	0.349 6
1		0.322 3*	0.338 8*	0.319 6*	0.338 1*	0.314 9*	0.336 1*	0.310 6*	0.333 2*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	GY							
		2.5 GY		5.0 GY		7.5 GY		10.0 GY	
		x	y	x	y	x	y	x	y
5/18	19.27	—	—	—	—	—	—	0.254 9	0.717 9
16		—	—	—	—	—	—	0.270 2	0.670 0
14		—	—	—	—	0.342 9	0.633 5	0.283 8	0.620 8
12		0.433 3	0.560 2	0.401 1	0.580 2	0.345 0	0.594 9	0.294 0	0.575 1
10		0.422 4	0.536 9	0.392 8	0.548 5	0.345 1	0.549 0	0.302 8	0.523 7
8		0.408 8	0.506 8	0.381 5	0.509 3	0.341 2	0.497 6	0.308 0	0.475 9
6		0.387 9	0.464 6	0.366 3	0.461 4	0.335 4	0.448 3	0.310 8	0.430 1
4		0.362 1	0.414 3	0.348 2	0.409 7	0.327 4	0.399 4	0.311 1	0.388 1
3		0.348 6*	0.388 8*	0.338 6*	0.385 0*	0.323 1*	0.377 1*	0.311 1*	0.369 0*
2		0.335 2	0.363 6	0.328 9	0.361 2	0.318 8	0.356 0	0.311 0	0.350 8
1		0.322 2*	0.339 3*	0.319 3*	0.338 3*	0.314 4*	0.335 8*	0.310 7*	0.333 3*
4/16	11.70	—	—	—	—	—	—	0.242 2	0.736 0
14		—	—	—	—	—	—	0.259 0	0.685 8
12		—	—	—	—	0.334 8	0.646 8	0.275 8	0.628 2
10		—	—	0.398 3	0.585 0	0.339 5	0.591 3	0.290 8	0.567 2
8		0.417 4	0.530 0	0.386 8	0.538 4	0.340 0	0.534 8	0.300 8	0.509 5
6		0.396 8	0.485 7	0.371 8	0.485 2	0.335 5	0.473 9	0.306 9	0.455 0
4		0.370 8	0.432 9	0.353 8	0.428 4	0.328 1	0.415 7	0.310 0	0.401 8
3		0.354 6*	0.401 8*	0.342 7*	0.397 8*	0.323 4*	0.387 2*	0.310 7*	0.377 5*
2		0.338 2	0.370 6	0.331 2	0.367 8	0.318 5	0.360 4	0.310 9	0.355 0
1		0.322 9*	0.341 4*	0.320 1*	0.340 1*	0.313 9*	0.336 4*	0.310 7*	0.334 5*
3/14	6.391	—	—	—	—	—	—	0.228 3	0.742 3
12		—	—	—	—	—	—	0.253 1	0.670 0
10		—	—	—	—	0.326 6	0.644 8	0.272 4	0.602 6
8		—	—	0.392 4	0.583 2	0.334 1	0.570 0	0.288 7	0.536 1
6		0.406 9	0.511 0	0.375 0	0.510 9	0.333 3	0.496 7	0.299 2	0.471 7
4		0.377 2	0.448 4	0.355 4	0.442 9	0.327 0	0.428 8	0.305 3	0.412 3
3		0.359 3*	0.412 5*	0.343 8*	0.407 2*	0.322 6*	0.395 4*	0.307 3*	0.383 9*
2		0.341 2	0.376 8	0.331 9	0.372 9	0.318 0	0.364 4	0.308 8	0.357 8
1		0.324 3*	0.343 9*	0.320 4*	0.342 0*	0.313 7*	0.337 5*	0.309 7*	0.334 9*
2/12	3.048	—	—	—	—	—	—	0.190 7	0.779 8
10		—	—	—	—	—	—	0.230 7	0.681 4
8		—	—	—	—	0.316 0	0.650 9	0.262 8	0.583 7
6		—	—	0.383 9	0.574 8	0.326 0	0.537 9	0.285 2	0.497 2
4		0.388 1	0.475 2	0.358 2	0.465 0	0.324 8	0.445 7	0.298 6	0.424 0
3		0.363 4*	0.423 9*	0.344 2*	0.416 4*	0.321 0*	0.402 6*	0.303 4*	0.389 0*
2		0.342 1	0.380 3	0.330 9	0.374 3	0.316 5	0.365 0	0.306 9	0.358 0
1		0.324 4*	0.344 4*	0.319 2*	0.340 4*	0.312 5*	0.335 4*	0.309 1*	0.333 0*
1/ 6	1.180	—	—	—	—	—	—	0.223 2	0.639 2
4		—	—	0.376 5	0.594 2	0.313 3	0.538 0	0.272 2	0.490 3
3		—	—	0.354 4*	0.481 9*	0.315 3*	0.450 2*	0.288 9*	0.425 3*
2		0.354 0	0.408 8	0.335 9	0.398 2	0.315 4	0.381 0	0.300 6	0.372 0
1		0.327 0*	0.347 0*	0.321 2*	0.343 8*	0.313 7*	0.339 4*	0.308 3*	0.337 0*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	G							
		2.5 G		5.0 G		7.5 G		10.0 G	
		x	y	x	y	x	y	x	y
9/16	76.69	0.263 0	0.496 6	—	—	—	—	—	—
14		0.271 1	0.472 6	—	—	—	—	—	—
12		0.278 6	0.449 1	0.252 8	0.416 0	0.241 9	0.398 5	0.232 5	0.379 6
10		0.285 1	0.427 5	0.263 9	0.400 1	0.254 5	0.385 5	0.245 7	0.370 2
8		0.291 2	0.405 4	0.273 5	0.385 4	0.265 2	0.373 8	0.257 4	0.361 8
6		0.296 6	0.384 6	0.283 2	0.369 7	0.276 3	0.360 7	0.270 3	0.351 3
4		0.301 8	0.360 6	0.293 3	0.351 9	0.288 2	0.346 1	0.284 0	0.340 2
3		0.303 9*	0.350 3*	0.297 6*	0.343 9*	0.293 5*	0.339 3*	0.290 3*	0.334 9*
2		0.305 8	0.340 0	0.301 7	0.335 7	0.298 7	0.332 3	0.296 5	0.329 3
1		0.307 8*	0.328 9*	0.305 8*	0.326 7*	0.304 1*	0.324 8*	0.303 0*	0.323 2*
8/24	57.62	0.209 1	0.603 3	—	—	—	—	—	—
22		0.222 1	0.579 9	0.182 1	0.494 0	—	—	—	—
20		0.233 9	0.556 1	0.195 6	0.480 6	0.184 5	0.449 2	0.173 4	0.416 4
18		0.245 1	0.530 9	0.210 3	0.465 2	0.198 0	0.437 2	0.186 6	0.408 6
16		0.256 3	0.504 5	0.224 0	0.450 0	0.212 0	0.425 2	0.201 2	0.399 2
14		0.266 1	0.478 0	0.236 8	0.434 8	0.225 4	0.412 5	0.214 8	0.390 3
12		0.274 3	0.455 4	0.248 9	0.419 1	0.238 0	0.400 2	0.228 2	0.381 1
10		0.282 9	0.430 1	0.261 3	0.402 6	0.251 5	0.386 7	0.243 0	0.371 0
8		0.289 6	0.406 5	0.272 3	0.386 5	0.263 9	0.373 3	0.256 4	0.361 1
6		0.295 2	0.385 1	0.282 2	0.370 2	0.275 4	0.360 8	0.269 3	0.351 2
4		0.300 9	0.361 4	0.292 4	0.352 3	0.287 4	0.346 4	0.282 8	0.340 3
3		0.303 2*	0.350 9*	0.296 7*	0.344 2*	0.292 7*	0.339 6*	0.289 2*	0.334 9*
2		0.305 3	0.340 4	0.300 9	0.335 9	0.298 1	0.332 6	0.295 7	0.329 3
1		0.307 5*	0.329 1*	0.305 3*	0.326 8*	0.303 8*	0.325 0*	0.302 6*	0.323 2*
7/26	41.98	0.168 9	0.654 9	0.139 7	0.531 2	0.130 3	0.485 8	—	—
24		0.187 5	0.626 5	0.152 1	0.520 0	0.141 5	0.477 8	0.131 0	0.437 7
22		0.202 9	0.601 7	0.165 9	0.507 4	0.153 9	0.468 3	0.143 4	0.430 6
20		0.218 1	0.574 4	0.180 5	0.493 3	0.168 8	0.457 0	0.158 9	0.422 0
18		0.232 8	0.546 7	0.196 7	0.477 1	0.184 1	0.444 8	0.173 4	0.413 5
16		0.244 8	0.520 3	0.211 1	0.461 6	0.198 2	0.433 0	0.188 1	0.404 9
14		0.256 8	0.493 1	0.226 2	0.445 0	0.213 9	0.419 9	0.203 3	0.395 6
12		0.267 2	0.466 7	0.241 6	0.426 7	0.229 5	0.405 8	0.219 5	0.385 4
10		0.277 5	0.439 5	0.255 4	0.408 7	0.244 5	0.391 4	0.235 2	0.374 8
8		0.286 1	0.412 9	0.268 7	0.390 1	0.259 5	0.376 4	0.251 3	0.363 5
6		0.293 3	0.387 3	0.280 1	0.372 1	0.272 8	0.362 2	0.266 2	0.352 6
4		0.299 2	0.364 4	0.290 2	0.354 8	0.285 0	0.348 2	0.280 3	0.341 5
3		0.302 0*	0.353 0*	0.295 2*	0.345 9*	0.291 1*	0.340 9*	0.287 3*	0.335 7*
2		0.304 7	0.341 3	0.300 1	0.336 6	0.297 2	0.333 3	0.294 5	0.329 7
1		0.307 4*	0.329 1*	0.305 1*	0.326 8*	0.303 5*	0.325 1*	0.302 0*	0.323 3*
6/28	29.30	0.114 5	0.712 2	0.090 8	0.569 5	0.085 8	0.512 7	—	—
26		0.134 0	0.687 1	0.107 9	0.556 0	0.101 0	0.501 8	0.094 1	0.452 0
24		0.153 6	0.660 5	0.125 2	0.540 8	0.115 9	0.491 0	0.107 0	0.445 8
22		0.173 9	0.631 8	0.143 2	0.525 2	0.132 5	0.479 5	0.123 0	0.437 8
20		0.192 2	0.603 5	0.160 9	0.509 1	0.148 5	0.467 7	0.138 2	0.429 9
18		0.210 2	0.573 7	0.178 5	0.492 4	0.165 4	0.455 1	0.155 1	0.420 8
16		0.227 8	0.543 0	0.196 0	0.475 1	0.183 2	0.441 4	0.172 2	0.411 3
14		0.242 6	0.513 3	0.213 0	0.457 1	0.200 1	0.427 8	0.189 5	0.401 5
12		0.257 4	0.481 4	0.229 3	0.439 0	0.217 1	0.413 8	0.206 0	0.391 4
10		0.269 0	0.453 0	0.246 6	0.418 1	0.235 0	0.397 9	0.224 7	0.379 6
8		0.279 9	0.423 9	0.261 2	0.399 0	0.251 0	0.382 9	0.242 0	0.367 9
6		0.289 2	0.396 3	0.274 8	0.379 5	0.266 2	0.367 2	0.259 1	0.355 8
4		0.296 7	0.369 5	0.286 8	0.359 5	0.280 7	0.352 2	0.274 9	0.344 3
3		0.300 4*	0.356 6*	0.292 8*	0.349 0*	0.288 3*	0.343 5*	0.283 8*	0.337 5*
2		0.303 9	0.343 7	0.298 8	0.338 2	0.295 8	0.334 4	0.292 9	0.330 3
1		0.307 2*	0.330 4*	0.304 6*	0.327 3*	0.303 1*	0.325 2*	0.301 8*	0.323 1*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	G							
		2.5 G		5.0 G		7.5 G		10.0 G	
		x	y	x	y	x	y	x	y
5/28	19.27	0.079 4	0.738 5	0.060 9	0.589 8	0.058 5	0.522 4	0.057 2	0.459 0
26		0.099 2	0.715 5	0.078 4	0.576 1	0.073 0	0.513 1	0.069 0	0.454 2
24		0.118 8	0.691 8	0.095 3	0.562 8	0.087 8	0.503 9	0.081 1	0.449 1
22		0.137 7	0.667 4	0.114 4	0.546 3	0.105 0	0.492 7	0.095 8	0.442 8
20		0.157 9	0.639 2	0.131 8	0.532 1	0.121 2	0.481 7	0.112 0	0.436 0
18		0.178 2	0.609 5	0.148 9	0.517 1	0.137 2	0.470 5	0.127 5	0.428 8
16		0.200 5	0.575 9	0.169 5	0.498 1	0.157 1	0.456 1	0.146 9	0.419 2
14		0.221 1	0.541 1	0.191 2	0.477 3	0.177 6	0.441 5	0.167 1	0.408 9
12		0.238 5	0.507 1	0.210 4	0.457 8	0.196 4	0.427 1	0.185 2	0.399 2
10		0.256 5	0.470 5	0.232 9	0.433 1	0.220 0	0.408 2	0.209 5	0.385 3
8		0.271 0	0.438 0	0.251 1	0.410 7	0.239 5	0.391 5	0.229 7	0.373 0
6		0.284 1	0.404 5	0.269 0	0.386 0	0.259 8	0.372 4	0.251 9	0.358 7
4		0.294 3	0.373 5	0.284 1	0.362 8	0.277 5	0.354 5	0.271 1	0.345 5
3		0.298 8*	0.358 8*	0.291 1*	0.351 0*	0.286 1*	0.345 1*	0.281 1*	0.338 3*
2		0.303 0	0.344 5	0.297 8	0.339 2	0.294 5	0.335 5	0.291 0	0.331 0
1		0.306 8*	0.330 4*	0.304 1*	0.327 6*	0.302 5*	0.325 9*	0.300 7*	0.323 6*
4/26	11.70	0.052 8	0.750 2	0.040 7	0.601 0	0.039 2	0.525 8	0.040 0	0.454 5
24		0.076 0	0.725 0	0.061 4	0.585 7	0.058 1	0.515 1	0.055 3	0.449 2
22		0.100 9	0.697 5	0.084 1	0.568 4	0.077 0	0.504 0	0.070 2	0.444 0
20		0.123 0	0.670 6	0.101 8	0.554 3	0.092 8	0.494 2	0.085 0	0.438 8
18		0.144 6	0.643 1	0.118 8	0.540 0	0.108 6	0.484 2	0.100 6	0.433 0
16		0.168 2	0.611 1	0.140 2	0.521 4	0.129 3	0.470 3	0.121 2	0.424 5
14		0.190 9	0.577 9	0.162 7	0.501 5	0.150 0	0.456 2	0.139 8	0.416 8
12		0.212 8	0.542 5	0.184 3	0.480 7	0.170 6	0.441 9	0.160 2	0.407 0
10		0.235 5	0.500 6	0.211 5	0.453 2	0.198 9	0.421 9	0.187 6	0.393 3
8		0.256 1	0.459 7	0.235 9	0.426 6	0.223 2	0.402 2	0.212 4	0.379 9
6		0.273 5	0.421 5	0.258 1	0.399 2	0.246 7	0.382 2	0.237 4	0.365 5
4		0.289 1	0.382 1	0.278 1	0.370 4	0.270 2	0.360 2	0.262 8	0.349 8
3		0.295 6*	0.364 0*	0.287 4*	0.355 8*	0.281 4*	0.348 6*	0.275 6*	0.341 3*
2		0.301 2	0.347 0	0.295 9	0.341 7	0.291 9	0.337 1	0.288 0	0.332 7
1		0.306 0*	0.331 1*	0.303 5*	0.328 4*	0.301 5*	0.326 2*	0.299 6*	0.324 3*
3/22	6.391	0.039 0	0.746 8	0.034 0	0.601 1	0.033 2	0.520 6	0.033 3	0.444 4
20		0.072 0	0.712 7	0.062 0	0.580 2	0.056 8	0.508 2	0.052 8	0.439 3
18		0.104 9	0.676 6	0.088 2	0.560 5	0.079 8	0.495 4	0.071 8	0.434 0
16		0.134 1	0.642 0	0.112 0	0.541 4	0.102 3	0.481 8	0.092 5	0.427 5
14		0.162 6	0.605 2	0.138 2	0.519 7	0.126 2	0.466 7	0.116 1	0.419 2
12		0.190 2	0.564 2	0.166 0	0.494 8	0.151 6	0.450 5	0.141 1	0.409 5
10		0.217 0	0.521 1	0.193 5	0.468 2	0.180 0	0.431 0	0.168 8	0.397 4
8		0.243 5	0.475 2	0.222 8	0.438 0	0.208 8	0.410 1	0.197 0	0.384 1
6		0.264 2	0.434 2	0.247 1	0.410 0	0.234 6	0.390 1	0.224 0	0.369 9
4		0.283 6	0.391 5	0.271 1	0.378 0	0.261 8	0.366 7	0.252 5	0.353 7
3		0.292 3*	0.370 2*	0.282 8*	0.360 7*	0.275 8*	0.352 9*	0.268 6*	0.343 8*
2		0.299 9	0.350 0	0.293 5	0.343 9	0.289 0	0.339 1	0.284 4	0.333 7
1		0.305 9*	0.331 8*	0.302 8*	0.328 8*	0.300 7*	0.326 5*	0.298 6*	0.324 3*
2/16	3.048	0.032 9	0.735 8	0.027 7	0.598 6	0.027 6	0.515 3	0.028 5	0.432 7
14		0.082 0	0.686 0	0.068 8	0.569 1	0.062 9	0.497 3	0.059 9	0.427 0
12		0.130 7	0.630 8	0.112 0	0.535 8	0.102 2	0.475 9	0.093 4	0.418 3
10		0.177 3	0.569 8	0.156 0	0.498 1	0.144 2	0.450 5	0.132 1	0.405 9
8		0.219 2	0.504 2	0.197 9	0.458 3	0.184 2	0.424 4	0.170 5	0.391 1
6		0.249 3	0.452 2	0.231 8	0.423 1	0.220 0	0.398 3	0.209 2	0.373 9
4		0.276 3	0.399 8	0.264 0	0.384 5	0.254 0	0.370 5	0.244 2	0.355 9
3		0.288 0*	0.374 1*	0.278 8*	0.364 1*	0.271 1*	0.355 0*	0.263 5*	0.345 0*
2		0.297 8	0.350 7	0.291 8	0.345 0	0.286 9	0.340 0	0.282 0	0.334 1
1		0.305 3*	0.331 0*	0.302 5*	0.328 6*	0.300 3*	0.326 7*	0.298 0*	0.324 2*
1/8	1.180	0.062 0	0.689 6	0.055 9	0.571 0	0.053 0	0.494 3	0.051 1	0.415 8
6		0.171 1	0.561 9	0.146 8	0.499 6	0.134 4	0.450 5	0.124 9	0.401 9
4		0.245 4	0.448 9	0.229 0	0.421 8	0.215 9	0.396 7	0.204 0	0.372 4
3		0.271 7*	0.402 0*	0.259 6*	0.386 7*	0.248 8*	0.371 2*	0.238 8*	0.356 2*
2		0.291 0	0.363 4	0.283 3	0.356 4	0.275 8	0.348 4	0.268 9	0.340 7
1		0.303 7*	0.334 4*	0.300 1*	0.332 4*	0.296 4*	0.329 7*	0.293 1*	0.327 0*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	BC							
		2.5 BC		5.0 BC		7.5 BC		10.0 BC	
		x	y	x	y	x	y	x	y
9/10	76.69	0.238 2	0.356 8	0.230 1	0.340 5	0.221 5	0.322 6	—	—
8		0.250 9	0.350 7	0.243 7	0.337 8	0.236 1	0.322 5	—	—
6		0.265 2	0.343 3	0.259 9	0.333 8	0.254 3	0.322 0	0.250 1	0.311 8
4		0.280 5	0.334 9	0.276 8	0.328 7	0.272 8	0.320 8	0.270 0	0.314 0
3		0.287 6*	0.330 9*	0.284 9*	0.326 1*	0.281 9*	0.319 9*	0.280 4*	0.315 1*
2		0.294 7	0.326 7	0.293 0	0.323 2	0.291 1	0.318 8	0.290 7	0.315 9
1		0.302 1*	0.321 9*	0.301 3*	0.320 0*	0.300 5*	0.317 6*	0.300 7*	0.316 4*
8/18	57.62	0.175 9	0.378 2	—	—	—	—	—	—
16		0.191 5	0.373 2	0.181 4	0.345 0	0.172 1	0.316 8	—	—
14		0.205 7	0.368 1	0.195 8	0.343 2	0.186 8	0.317 9	0.178 8	0.293 6
12		0.219 6	0.363 0	0.210 1	0.341 2	0.201 0	0.318 8	0.193 7	0.297 8
10		0.235 2	0.356 6	0.226 4	0.338 3	0.218 4	0.319 6	0.212 0	0.302 5
8		0.250 0	0.350 0	0.241 9	0.335 2	0.235 2	0.319 8	0.230 2	0.306 3
6		0.264 7	0.342 9	0.258 8	0.331 8	0.252 5	0.319 8	0.248 9	0.309 9
4		0.279 1	0.335 1	0.275 2	0.327 8	0.271 8	0.320 0	0.268 6	0.313 0
3		0.286 4*	0.331 1*	0.283 4*	0.325 5*	0.280 9*	0.319 3*	0.278 9*	0.314 2*
2		0.294 0	0.326 8	0.291 9	0.322 8	0.290 0	0.318 3	0.289 4	0.315 2
1		0.301 9*	0.321 9*	0.300 7*	0.319 8*	0.299 6*	0.317 2*	0.299 8*	0.315 9*
7/22	41.98	0.133 4	0.387 0	—	—	—	—	—	—
20		0.149 0	0.382 7	0.138 0	0.341 2	—	—	—	—
18		0.162 6	0.378 8	0.151 5	0.341 0	0.142 7	0.307 6	—	—
16		0.178 8	0.373 9	0.167 5	0.340 1	0.158 4	0.310 1	0.148 9	0.276 8
14		0.193 2	0.369 4	0.183 8	0.339 0	0.175 1	0.312 9	0.167 1	0.283 2
12		0.210 2	0.363 6	0.199 7	0.337 9	0.191 4	0.314 8	0.184 1	0.289 2
10		0.226 4	0.357 6	0.216 3	0.336 1	0.209 4	0.316 5	0.203 5	0.295 6
8		0.243 9	0.350 8	0.235 4	0.333 5	0.229 2	0.317 8	0.223 5	0.301 4
6		0.260 8	0.343 0	0.254 3	0.330 2	0.249 0	0.318 6	0.244 8	0.306 9
4		0.276 4	0.335 4	0.271 2	0.326 9	0.267 1	0.318 9	0.264 2	0.310 9
3		0.284 4*	0.331 3*	0.280 3*	0.324 9*	0.277 2*	0.318 7*	0.275 3*	0.312 7*
2		0.292 7	0.326 9	0.289 8	0.322 5	0.287 8	0.318 2	0.286 9	0.314 3
1		0.301 2*	0.321 9*	0.299 7*	0.319 7*	0.298 8*	0.317 4*	0.298 6*	0.315 5*
6/22	29.30	0.112 0	0.386 0	—	—	—	—	—	—
20		0.126 9	0.382 9	0.116 8	0.334 4	—	—	—	—
18		0.142 8	0.379 0	0.132 5	0.334 5	0.124 8	0.298 1	0.118 1	0.258 1
16		0.160 0	0.374 8	0.149 1	0.334 5	0.140 8	0.301 7	0.133 7	0.265 1
14		0.177 9	0.369 9	0.166 2	0.334 3	0.158 5	0.305 2	0.151 8	0.272 9
12		0.195 4	0.364 5	0.184 4	0.333 7	0.176 2	0.308 1	0.169 8	0.280 2
10		0.214 8	0.358 4	0.203 7	0.332 9	0.196 1	0.311 0	0.190 9	0.288 1
8		0.233 2	0.352 2	0.223 6	0.331 1	0.217 1	0.313 8	0.211 6	0.295 0
6		0.252 6	0.344 8	0.244 1	0.329 0	0.238 4	0.315 5	0.233 5	0.301 5
4		0.270 2	0.336 9	0.264 8	0.326 2	0.260 4	0.316 9	0.257 8	0.307 8
3		0.280 1*	0.332 0*	0.275 9*	0.324 2*	0.272 5*	0.317 2*	0.270 6*	0.310 7*
2		0.290 2	0.326 8	0.287 2	0.321 9	0.284 9	0.317 2	0.283 7	0.313 2
1		0.300 3*	0.321 5*	0.298 7*	0.319 3*	0.297 5*	0.316 9*	0.296 9*	0.315 1*
5/24	19.27	0.073 8	0.385 1	—	—	—	—	—	—
22		0.086 1	0.383 2	0.078 1	0.321 1	—	—	—	—
20		0.100 5	0.381 4	0.090 4	0.323 1	—	—	—	—
18		0.116 5	0.378 5	0.104 6	0.324 4	0.098 2	0.282 8	—	—
16		0.134 8	0.375 0	0.124 3	0.326 1	0.116 7	0.288 0	0.110 8	0.248 9
14		0.155 9	0.370 8	0.144 8	0.327 5	0.136 4	0.293 2	0.130 8	0.258 2
12		0.173 5	0.366 8	0.161 4	0.328 0	0.153 7	0.297 6	0.148 5	0.266 2
10		0.198 0	0.360 6	0.185 0	0.328 0	0.177 6	0.303 2	0.171 6	0.276 0
8		0.220 5	0.353 7	0.210 0	0.328 0	0.203 0	0.308 2	0.197 0	0.286 0
6		0.244 8	0.345 2	0.236 0	0.327 0	0.229 2	0.312 5	0.223 4	0.295 2
4		0.265 9	0.336 9	0.259 1	0.324 6	0.255 0	0.315 0	0.251 2	0.304 0
3		0.276 9*	0.332 1*	0.271 4*	0.322 9*	0.267 9*	0.315 7*	0.265 2*	0.307 8*
2		0.288 0	0.327 0	0.284 1	0.321 0	0.281 2	0.316 1	0.279 6	0.311 1
1		0.299 1*	0.321 7*	0.297 0*	0.318 8*	0.295 2*	0.316 3*	0.294 5*	0.313 9*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	BG							
		2.5 BG		5.0 BG		7.5 BG		10.0 BG	
		x	y	x	y	x	y	x	y
4/24	11.70	0.051 0	0.380 0	—	—	—	—	—	—
22		0.063 6	0.378 8	—	—	—	—	—	—
20		0.076 8	0.377 3	0.067 5	0.307 5	—	—	—	—
18		0.091 5	0.375 4	0.082 8	0.310 8	0.076 8	0.266 7	—	—
16		0.110 2	0.372 0	0.099 2	0.314 1	0.092 2	0.271 8	0.088 8	0.229 8
14		0.128 3	0.368 8	0.117 0	0.317 0	0.109 2	0.277 4	0.103 3	0.237 6
12		0.149 2	0.364 9	0.137 9	0.319 8	0.129 8	0.284 0	0.124 8	0.248 4
10		0.173 8	0.360 0	0.161 8	0.321 9	0.154 0	0.291 0	0.148 0	0.260 0
8		0.200 6	0.354 0	0.189 0	0.323 4	0.181 5	0.298 5	0.176 0	0.273 0
6		0.227 8	0.346 3	0.218 2	0.324 0	0.211 3	0.305 2	0.206 5	0.286 3
4		0.255 2	0.337 5	0.248 0	0.323 2	0.242 9	0.310 8	0.238 4	0.298 4
3		0.269 7*	0.332 4*	0.263 9*	0.322 2*	0.259 5*	0.313 1*	0.255 9*	0.304 1*
2		0.284 0	0.327 0	0.279 9	0.320 8	0.276 4	0.314 8	0.274 0	0.309 1
1		0.297 6*	0.321 6*	0.295 4*	0.318 8*	0.293 3*	0.315 9*	0.292 2*	0.313 3*
3/20	6.391	0.048 2	0.369 5	—	—	—	—	—	—
18		0.064 8	0.368 2	0.058 0	0.294 0	—	—	—	—
16		0.084 3	0.366 7	0.073 5	0.297 9	0.069 1	0.255 9	—	—
14		0.105 1	0.364 8	0.094 0	0.302 7	0.087 4	0.262 7	0.079 8	0.215 1
12		0.128 8	0.362 0	0.115 8	0.307 1	0.108 6	0.270 6	0.101 8	0.228 1
10		0.155 2	0.358 0	0.141 0	0.311 8	0.132 6	0.278 4	0.125 0	0.241 1
8		0.184 5	0.353 1	0.170 3	0.315 9	0.162 0	0.287 2	0.155 1	0.257 1
6		0.213 2	0.346 8	0.202 0	0.318 8	0.192 8	0.295 8	0.186 1	0.272 2
4		0.243 7	0.338 6	0.234 3	0.320 0	0.227 2	0.304 1	0.222 1	0.288 6
3		0.261 8*	0.333 0*	0.254 0*	0.319 9*	0.248 2*	0.308 3*	0.243 5*	0.297 1*
2		0.279 9	0.327 1	0.274 2	0.319 2	0.269 9	0.312 0	0.266 0	0.305 0
1		0.296 5*	0.321 4*	0.293 4*	0.318 0*	0.291 0*	0.314 8*	0.288 5*	0.311 6*
2/14	3.048	0.055 5	0.358 8	—	—	—	—	—	—
12		0.085 1	0.357 6	0.076 9	0.288 0	0.072 4	0.247 8	—	—
10		0.119 0	0.355 1	0.105 0	0.295 6	0.099 1	0.258 2	0.092 9	0.213 3
8		0.155 7	0.351 7	0.140 5	0.303 7	0.132 5	0.271 0	0.125 8	0.233 1
6		0.197 1	0.345 2	0.184 3	0.311 0	0.174 7	0.285 3	0.166 9	0.257 0
4		0.234 3	0.337 8	0.223 4	0.315 0	0.216 2	0.298 1	0.209 6	0.279 0
3		0.255 6*	0.332 7*	0.246 5*	0.316 6*	0.240 4*	0.304 3*	0.234 7*	0.290 4*
2		0.276 5	0.327 1	0.269 7	0.317 5	0.265 1	0.309 8	0.260 6	0.301 0
1		0.295 2*	0.321 5*	0.291 5*	0.317 5*	0.288 8*	0.314 0*	0.286 1*	0.309 9*
1/ 8	1.180	0.047 6	0.345 8	—	—	—	—	—	—
6		0.116 9	0.345 2	0.109 3	0.286 0	0.105 9	0.248 5	0.107 4	0.212 9
4		0.188 3	0.340 6	0.175 3	0.302 1	0.170 2	0.276 8	0.165 8	0.249 6
3		0.225 5*	0.335 3*	0.213 0*	0.309 0*	0.206 4*	0.290 4*	0.200 0*	0.269 4*
2		0.260 0	0.328 9	0.250 0	0.314 1	0.243 0	0.302 3	0.236 2	0.288 2
1		0.289 1*	0.322 3*	0.283 3*	0.316 8*	0.278 2*	0.311 3*	0.273 2*	0.304 3*



Attached Table 2. (continued)

I/C	Y <sub>c</sub> (%)	B							
		2.5 B		5.0 B		7.5 B		10.0 B	
		x	y	x	y	x	y	x	y
9/4	76.69	0.268 0	0.307 3	0.267 5	0.300 5	0.268 8	0.296 1	0.271 2	0.292 4
3		0.279 9*	0.310 1*	0.280 5*	0.305 8*	0.282 3*	0.303 0*	0.284 1*	0.300 8*
2		0.290 9	0.312 5	0.291 9	0.310 2	0.293 7	0.308 7	0.294 9	0.307 6
1		0.301 0*	0.314 6*	0.301 8*	0.313 7*	0.303 0*	0.313 1*	0.303 6*	0.312 8*
8/12	57.62	0.187 7	0.275 2	—	—	—	—	—	—
10		0.206 6	0.283 9	—	—	—	—	—	—
8		0.226 4	0.292 3	0.223 7	0.276 1	0.225 2	0.266 8	0.229 4	0.258 7
6		0.246 2	0.300 0	0.245 7	0.288 8	0.247 2	0.282 1	0.251 2	0.276 0
4		0.266 8	0.306 7	0.267 1	0.299 8	0.268 8	0.295 6	0.271 8	0.291 1
3		0.278 3*	0.309 7*	0.279 1*	0.305 0*	0.280 7*	0.302 0*	0.282 9*	0.299 0*
2		0.289 7	0.312 4	0.290 8	0.309 6	0.292 2	0.307 7	0.293 5	0.306 2
1		0.300 5*	0.314 6*	0.301 4*	0.313 5*	0.302 3*	0.312 6*	0.302 8*	0.312 2*
7/16	41.98	0.143 5	0.247 2	—	—	—	—	—	—
14		0.162 4	0.258 1	0.161 5	0.230 7	—	—	—	—
12		0.179 7	0.267 2	0.177 8	0.243 0	0.181 8	0.230 3	0.188 3	0.220 3
10		0.199 4	0.277 5	0.198 6	0.257 9	0.201 6	0.246 6	0.207 8	0.238 2
8		0.220 8	0.287 1	0.220 4	0.272 9	0.222 5	0.263 1	0.227 7	0.255 9
6		0.241 8	0.296 0	0.241 0	0.285 4	0.243 6	0.278 7	0.247 8	0.272 8
4		0.262 9	0.303 8	0.263 3	0.297 2	0.265 1	0.292 7	0.268 5	0.288 6
3		0.274 7*	0.307 6*	0.275 4*	0.302 7*	0.277 0*	0.299 5*	0.279 7*	0.296 5*
2		0.286 7	0.311 0	0.287 5	0.307 8	0.288 8	0.305 8	0.290 8	0.303 9
1		0.298 6*	0.314 0*	0.299 2*	0.312 4*	0.300 0*	0.311 5*	0.301 1*	0.310 6*
6/16	29.30	0.129 4	0.234 8	0.131 0	0.204 8	0.137 6	0.187 9	0.145 4	0.177 8
14		0.148 0	0.245 9	0.149 6	0.219 3	0.155 6	0.204 3	0.162 9	0.194 7
12		0.166 0	0.256 1	0.168 5	0.233 9	0.173 4	0.220 3	0.180 3	0.211 4
10		0.187 9	0.268 2	0.188 3	0.248 7	0.193 4	0.237 4	0.200 0	0.229 8
8		0.208 0	0.278 9	0.208 8	0.263 5	0.213 2	0.253 7	0.218 9	0.246 8
6		0.231 2	0.289 9	0.232 0	0.278 9	0.235 2	0.270 8	0.239 9	0.265 0
4		0.257 1	0.300 8	0.257 9	0.293 8	0.260 2	0.288 1	0.263 7	0.284 0
3		0.270 3*	0.305 5*	0.271 1*	0.300 4*	0.272 8*	0.296 2*	0.275 5*	0.292 8*
2		0.283 5	0.309 7	0.284 2	0.306 3	0.285 4	0.303 7	0.287 1	0.301 2
1		0.296 8*	0.313 3*	0.297 2*	0.311 6*	0.297 9*	0.310 5*	0.298 7*	0.309 0*
5/18	19.27	—	—	—	—	—	—	0.120 3	0.150 5
16		0.109 0	0.216 6	0.113 2	0.186 3	0.123 0	0.171 1	0.132 6	0.163 2
14		0.128 3	0.229 2	0.132 0	0.202 1	0.140 4	0.187 8	0.149 2	0.179 7
12		0.146 1	0.240 6	0.150 5	0.217 2	0.158 4	0.204 2	0.166 6	0.196 4
10		0.169 7	0.254 9	0.172 9	0.234 7	0.179 2	0.223 0	0.186 0	0.214 9
8		0.194 7	0.268 7	0.195 8	0.251 9	0.200 7	0.241 7	0.206 7	0.234 4
6		0.221 0	0.282 3	0.221 5	0.270 1	0.224 8	0.261 2	0.229 9	0.254 8
4		0.249 2	0.295 4	0.249 3	0.287 9	0.251 1	0.280 8	0.254 7	0.275 7
3		0.264 0*	0.301 5*	0.264 2*	0.295 8*	0.265 5*	0.290 6*	0.268 2*	0.286 2*
2		0.279 1	0.307 1	0.279 4	0.303 2	0.280 3	0.300 0	0.282 1	0.296 6
1		0.294 5*	0.312 1*	0.294 8*	0.310 0*	0.295 3*	0.308 7*	0.296 1*	0.306 7*
4/16	11.70	0.090 0	0.197 3	—	—	—	—	0.115 5	0.141 6
14		0.102 7	0.205 7	0.109 8	0.178 5	0.120 4	0.165 5	0.131 0	0.158 0
12		0.124 7	0.220 9	0.129 9	0.196 3	0.139 3	0.183 7	0.148 7	0.176 0
10		0.146 3	0.235 4	0.151 2	0.214 8	0.160 1	0.202 8	0.168 1	0.195 4
8		0.173 7	0.252 4	0.175 9	0.234 5	0.182 1	0.223 2	0.189 3	0.216 0
6		0.204 8	0.270 8	0.206 0	0.257 2	0.210 2	0.247 0	0.215 7	0.240 7
4		0.236 0	0.287 2	0.236 3	0.278 2	0.238 8	0.270 4	0.242 9	0.264 8
3		0.254 0*	0.295 7*	0.253 8*	0.288 9*	0.255 5*	0.282 7*	0.258 6*	0.277 8*
2		0.272 7	0.303 8	0.272 3	0.299 2	0.273 3	0.294 7	0.275 3	0.291 0
1		0.291 6*	0.310 8*	0.291 2*	0.308 5*	0.291 6*	0.306 1*	0.292 6*	0.304 0*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	B							
		2.5 B		5.0 B		7.5 B		10.0 B	
		x	y	x	y	x	y	x	y
3/14	6.391	—	—	—	—	—	—	0.106 5	0.128 5
12		0.098 9	0.196 3	0.104 2	0.168 1	0.113 1	0.154 2	0.122 8	0.146 0
10		0.122 0	0.213 2	0.125 9	0.187 9	0.134 3	0.175 6	0.143 2	0.167 5
8		0.151 1	0.233 1	0.152 7	0.211 9	0.158 3	0.198 7	0.165 8	0.190 5
6		0.182 6	0.253 6	0.183 5	0.237 5	0.187 5	0.225 8	0.193 3	0.217 3
4		0.218 3	0.274 8	0.217 6	0.263 2	0.220 0	0.253 6	0.224 6	0.246 7
3		0.240 3*	0.286 8*	0.238 8*	0.277 7*	0.239 8*	0.269 5*	0.242 9*	0.263 0*
2		0.263 6	0.298 3	0.261 7	0.292 1	0.261 6	0.285 7	0.263 1	0.280 1
1		0.287 2*	0.308 5*	0.285 7*	0.305 3*	0.285 1*	0.301 6*	0.285 5*	0.297 9*
2/10	3.048	0.091 1	0.182 8	0.096 5	0.155 8	0.105 1	0.142 2	0.115 7	0.134 6
8		0.123 0	0.207 6	0.124 5	0.182 7	0.131 3	0.169 2	0.139 6	0.160 3
6		0.162 1	0.235 8	0.161 7	0.216 2	0.165 8	0.202 6	0.171 6	0.193 7
4		0.206 0	0.264 9	0.204 8	0.251 8	0.206 3	0.240 0	0.210 2	0.231 3
3		0.231 4*	0.279 9*	0.229 7*	0.270 0*	0.229 5*	0.260 0*	0.232 0*	0.251 5*
2		0.257 8	0.294 0	0.255 9	0.287 4	0.254 5	0.279 9	0.255 8	0.272 5
1		0.284 4*	0.306 4*	0.282 9*	0.303 1*	0.281 4*	0.298 9*	0.281 8*	0.294 1*
1/ 8	1.180	—	—	—	—	0.096 8	0.128 0	0.107 7	0.121 8
6		0.111 8	0.190 8	0.121 2	0.174 5	0.130 3	0.163 9	0.139 2	0.156 3
4		0.164 9	0.232 4	0.166 7	0.216 8	0.171 6	0.204 8	0.178 3	0.197 4
3		0.197 0*	0.255 5*	0.195 7*	0.241 9*	0.197 9*	0.230 3*	0.202 1*	0.221 6*
2		0.232 2	0.278 1	0.229 1	0.267 7	0.229 1	0.257 9	0.230 9	0.249 1
1		0.270 1*	0.298 9*	0.267 2*	0.293 0*	0.266 2*	0.286 9*	0.266 4*	0.280 5*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	PB							
		2.5 PB		5.0 PB		7.5 PB		10.0 PB	
		x	y	x	y	x	y	x	y
9/ 4	76.69	—	—	—	—	—	—	0.291 0	0.285 0
3		—	—	—	—	—	—	0.298 2*	0.296 4*
2		0.297 5	0.306 3	0.299 1	0.305 7	0.301 5	0.305 2	0.303 8	0.305 4
1		0.305 0*	0.312 2*	0.305 6*	0.311 9*	0.306 5*	0.311 8*	0.307 8*	0.312 0*
8/ 8	57.62	—	—	—	—	—	—	0.267 7	0.244 3
6		0.256 2	0.270 9	0.261 4	0.267 0	0.270 2	0.264 8	0.279 2	0.264 9
4		0.275 8	0.287 9	0.279 8	0.286 1	0.285 6	0.284 6	0.291 1	0.284 8
3		0.286 1*	0.296 6*	0.289 0*	0.295 4*	0.293 3*	0.294 4*	0.297 2*	0.294 6*
2		0.295 7	0.304 7	0.297 4	0.303 9	0.300 3	0.303 4	0.302 7	0.303 5
1		0.304 0*	0.311 5*	0.304 6*	0.311 0*	0.306 1*	0.310 9*	0.307 2*	0.310 9*
7/12	41.98	—	—	—	—	—	—	0.246 5	0.205 8
10		0.216 2	0.230 9	0.225 4	0.226 7	0.241 0	0.222 4	0.256 3	0.224 0
8		0.235 2	0.249 8	0.242 7	0.245 8	0.254 6	0.241 8	0.267 0	0.242 5
6		0.253 8	0.267 7	0.259 6	0.264 3	0.268 7	0.261 2	0.277 6	0.261 2
4		0.272 9	0.284 8	0.277 3	0.282 8	0.283 3	0.280 9	0.288 6	0.280 1
3		0.283 2*	0.293 9*	0.286 4*	0.292 2*	0.290 9*	0.290 8*	0.294 6*	0.290 2*
2		0.293 2	0.302 5	0.295 2	0.301 1	0.298 2	0.300 3	0.300 5	0.300 0
1		0.302 4*	0.310 2*	0.303 2*	0.309 3*	0.304 7*	0.308 9*	0.305 8*	0.308 9*
6/16	29.30	—	—	—	—	—	—	0.226 5	0.167 1
14		0.175 4	0.186 8	0.187 3	0.182 2	0.211 9	0.179 9	0.235 2	0.183 9
12		0.191 3	0.203 8	0.202 6	0.199 9	0.224 1	0.197 5	0.244 0	0.199 8
10		0.209 5	0.222 5	0.219 7	0.218 8	0.237 8	0.216 8	0.254 0	0.217 6
8		0.227 4	0.240 6	0.236 0	0.236 5	0.250 5	0.234 7	0.263 7	0.235 2
6		0.246 5	0.259 9	0.253 3	0.255 8	0.263 8	0.253 1	0.274 0	0.253 3
4		0.268 4	0.280 4	0.273 4	0.277 8	0.279 8	0.275 2	0.286 3	0.274 7
3		0.279 1*	0.290 0*	0.283 0*	0.288 0*	0.287 7*	0.285 9*	0.292 6*	0.285 5*
2		0.289 7	0.299 1	0.292 3	0.297 8	0.295 5	0.296 3	0.298 8	0.296 1
1		0.300 0*	0.307 9*	0.301 3*	0.307 2*	0.303 0*	0.306 4*	0.304 7*	0.306 4*
5/22	19.27	—	—	—	—	—	—	0.208 2	0.122 5
20		—	—	—	—	0.179 4	0.123 9	0.212 1	0.132 9
18		0.136 3	0.141 0	0.151 8	0.136 5	0.186 2	0.136 5	0.217 4	0.144 4
16		0.149 5	0.155 9	0.163 8	0.152 1	0.194 5	0.151 1	0.222 4	0.155 5
14		0.164 2	0.172 8	0.177 3	0.168 9	0.204 2	0.166 1	0.229 9	0.169 8
12		0.179 3	0.189 4	0.191 8	0.185 8	0.215 7	0.183 0	0.238 4	0.185 7
10		0.196 8	0.207 8	0.208 0	0.204 1	0.228 5	0.202 0	0.247 8	0.203 0
8		0.215 7	0.227 8	0.225 5	0.223 9	0.241 7	0.220 4	0.257 2	0.221 1
6		0.236 5	0.248 8	0.244 7	0.244 9	0.256 3	0.241 7	0.268 6	0.241 2
4		0.260 0	0.272 0	0.266 2	0.268 7	0.273 9	0.266 6	0.282 1	0.265 9
3		0.272 2*	0.283 2*	0.277 2*	0.280 5*	0.282 8*	0.278 7*	0.289 0*	0.278 1*
2		0.284 7	0.294 2	0.288 2	0.292 3	0.291 8	0.290 8	0.295 9	0.290 5
1		0.297 3*	0.305 2*	0.299 2*	0.304 2*	0.300 9*	0.303 3*	0.302 9*	0.303 2*
4/30	11.70	—	—	—	—	—	—	0.195 2	0.077 8
28		—	—	—	—	—	—	0.197 1	0.084 0
26		—	—	—	—	0.165 9	0.082 5	0.199 4	0.090 4
24		—	—	—	—	0.168 4	0.089 9	0.202 0	0.098 5
22		—	—	—	—	0.171 3	0.098 0	0.204 8	0.106 4
20		—	—	0.128 8	0.102 7	0.174 2	0.105 8	0.207 5	0.114 0
18		0.121 8	0.120 8	0.139 2	0.116 7	0.179 8	0.118 5	0.212 0	0.125 6
16		0.133 6	0.134 9	0.150 4	0.131 7	0.186 1	0.131 6	0.217 0	0.137 3
14		0.147 3	0.151 3	0.162 7	0.147 9	0.194 1	0.146 8	0.222 0	0.150 3
12		0.163 4	0.169 8	0.177 3	0.165 9	0.203 7	0.162 9	0.229 8	0.165 9
10		0.180 5	0.188 8	0.192 5	0.184 3	0.215 8	0.181 1	0.238 8	0.183 7
8		0.199 5	0.209 4	0.210 3	0.205 0	0.230 4	0.202 3	0.249 7	0.203 8
6		0.223 5	0.234 3	0.232 5	0.230 0	0.247 1	0.226 6	0.261 8	0.226 3
4		0.248 7	0.259 7	0.256 2	0.256 0	0.265 7	0.252 8	0.275 9	0.252 2
3		0.263 0*	0.273 4*	0.268 6*	0.269 7*	0.275 6*	0.266 8*	0.283 2*	0.265 7*
2		0.278 2	0.287 6	0.281 6	0.284 2	0.286 1	0.281 9	0.291 1	0.280 4
1		0.294 0*	0.302 0*	0.295 4*	0.299 7*	0.297 5*	0.298 3*	0.300 0*	0.297 1*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	PB							
		2.5 PB		5.0 PB		7.5 PB		10.0 PB	
		x	y	x	y	x	y	x	y
3/34	6.391	—	—	—	—	0.160 8	0.048 0	0.191 8	0.050 3
32		—	—	—	—	0.161 2	0.051 1	0.192 6	0.054 2
30		—	—	—	—	0.162 1	0.055 6	0.193 8	0.059 9
28		—	—	—	—	0.163 2	0.060 9	0.195 0	0.065 0
26		—	—	—	—	0.164 2	0.065 5	0.196 3	0.070 8
24		—	—	—	—	0.165 8	0.071 1	0.198 2	0.077 2
22		—	—	—	—	0.167 7	0.078 2	0.200 4	0.084 7
20		—	—	—	—	0.170 2	0.086 7	0.203 0	0.093 0
18		—	—	0.122 8	0.089 5	0.173 0	0.094 8	0.206 0	0.102 0
16		—	—	0.131 8	0.102 4	0.176 5	0.104 8	0.209 2	0.111 8
14		0.125 1	0.121 8	0.143 1	0.118 4	0.182 4	0.118 8	0.214 2	0.125 0
12		0.139 8	0.139 5	0.155 7	0.135 6	0.190 3	0.135 3	0.220 6	0.140 7
10		0.157 6	0.160 0	0.171 8	0.156 2	0.200 5	0.153 6	0.227 8	0.156 5
8		0.178 0	0.183 3	0.190 8	0.179 9	0.214 9	0.176 1	0.238 7	0.178 6
6		0.202 2	0.210 1	0.212 2	0.205 2	0.231 1	0.201 0	0.251 1	0.203 1
4		0.231 2	0.240 5	0.239 3	0.236 1	0.252 0	0.231 9	0.266 0	0.231 9
3		0.247 8*	0.257 4*	0.254 3*	0.253 2*	0.264 1*	0.249 3*	0.274 7*	0.248 2*
2		0.266 3	0.275 6	0.270 8	0.271 9	0.277 7	0.268 7	0.284 7	0.267 0
1		0.287 0*	0.295 2*	0.289 3*	0.292 8*	0.292 9*	0.290 8*	0.296 4*	0.289 4*
2/38	3.048	—	—	—	—	0.162 3	0.028 0	—	—
36		—	—	—	—	0.162 8	0.031 0	—	—
34		—	—	—	—	0.163 0	0.034 0	0.191 1	0.034 4
32		—	—	—	—	0.163 5	0.037 3	0.191 8	0.037 9
30		—	—	—	—	0.164 0	0.040 9	0.192 5	0.042 0
28		—	—	—	—	0.164 7	0.045 1	0.193 7	0.047 1
26		—	—	—	—	0.165 3	0.049 2	0.194 9	0.052 0
24		—	—	—	—	0.166 0	0.053 8	0.196 2	0.057 8
22		—	—	—	—	0.167 0	0.059 4	0.197 8	0.064 3
20		—	—	—	—	0.168 5	0.066 6	0.199 8	0.071 8
18		—	—	—	—	0.170 1	0.074 2	0.202 1	0.080 8
16		—	—	—	—	0.172 8	0.083 9	0.205 2	0.091 0
14		—	—	0.125 3	0.087 3	0.176 2	0.095 5	0.208 7	0.102 6
12		0.116 6	0.107 6	0.136 3	0.104 8	0.181 3	0.109 4	0.213 9	0.117 0
10		0.133 2	0.127 8	0.150 0	0.124 0	0.188 2	0.125 8	0.220 0	0.133 0
8		0.154 0	0.153 0	0.168 5	0.149 1	0.200 5	0.149 5	0.229 4	0.155 1
6		0.182 5	0.185 7	0.194 2	0.181 1	0.218 9	0.179 0	0.244 0	0.184 0
4		0.217 5	0.224 5	0.226 3	0.219 2	0.242 0	0.214 8	0.260 0	0.216 2
3		0.237 4*	0.245 4*	0.244 2*	0.239 8*	0.255 6*	0.235 1*	0.269 3*	0.234 7*
2		0.259 2	0.267 5	0.263 8	0.262 4	0.271 2	0.258 2	0.280 3	0.256 7
1		0.283 3*	0.291 1*	0.285 6*	0.287 7*	0.289 2*	0.285 0*	0.293 7*	0.283 4*
1/38	1.180	—	—	—	—	0.168 0	0.014 0	—	—
36		—	—	—	—	0.168 1	0.016 0	—	—
34		—	—	—	—	0.168 2	0.018 0	—	—
32		—	—	—	—	0.168 2	0.020 2	—	—
30		—	—	—	—	0.168 4	0.023 4	0.192 8	0.024 0
28		—	—	—	—	0.168 6	0.027 0	0.193 6	0.028 1
26		—	—	—	—	0.168 9	0.030 9	0.194 2	0.032 6
24		—	—	—	—	0.169 1	0.035 2	0.195 2	0.038 0
22		—	—	—	—	0.169 6	0.040 2	0.196 5	0.043 6
20		—	—	—	—	0.170 1	0.045 4	0.197 6	0.049 3
18		—	—	—	—	0.170 9	0.051 8	0.199 1	0.056 4
16		—	—	—	—	0.172 0	0.058 3	0.200 8	0.063 8
14		—	—	—	—	0.173 8	0.068 8	0.203 8	0.074 5
12		—	—	—	—	0.176 3	0.080 4	0.207 0	0.086 9
10		—	—	0.128 5	0.087 0	0.180 4	0.095 0	0.212 0	0.102 9
8		0.127 3	0.115 7	0.144 7	0.112 4	0.187 2	0.114 1	0.219 0	0.122 8
6		0.153 9	0.149 1	0.167 8	0.144 7	0.200 0	0.142 2	0.229 0	0.147 0
4		0.189 5	0.191 1	0.201 2	0.186 7	0.223 2	0.182 1	0.245 9	0.182 8
3		0.210 3*	0.214 5*	0.219 8*	0.209 4*	0.236 9*	0.203 7*	0.255 2*	0.202 1*
2		0.236 0	0.242 0	0.242 7	0.236 8	0.254 7	0.231 0	0.267 7	0.228 0
1		0.268 6*	0.275 3*	0.272 1*	0.271 5*	0.278 4*	0.267 4*	0.285 3*	0.264 7*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	P							
		2.5 P		5.0 P		7.5 P		10.0 P	
		x	y	x	y	x	y	x	y
9/6	76.69	—	—	—	—	0.312 0	0.278 8	0.321 8	0.284 5
4		0.296 3	0.286 5	0.300 3	0.287 0	0.311 7	0.292 8	0.317 6	0.296 6
3		0.301 1*	0.296 7*	0.303 9*	0.297 6*	0.311 2*	0.300 8*	0.315 1*	0.303 3*
2		0.305 0	0.305 1	0.306 7	0.306 0	0.310 7	0.308 1	0.312 8	0.309 4
1		0.308 0*	0.311 6*	0.308 8*	0.312 2*	0.310 3*	0.313 6*	0.311 0*	0.314 0*
8/14	57.62	—	—	—	—	—	—	0.334 2	0.234 9
12		—	—	—	—	0.311 7	0.237 0	0.331 2	0.247 0
10		—	—	0.287 0	0.238 0	0.311 6	0.249 7	0.328 2	0.258 2
8		0.280 0	0.248 8	0.291 4	0.253 4	0.311 6	0.262 6	0.325 0	0.270 0
6		0.288 1	0.267 1	0.296 3	0.270 4	0.311 4	0.278 5	0.321 3	0.282 9
4		0.296 2	0.285 0	0.301 2	0.286 8	0.311 4	0.291 5	0.317 5	0.295 5
3		0.300 7*	0.294 9*	0.303 9*	0.296 1*	0.311 1*	0.299 5*	0.315 2*	0.302 2*
2		0.304 8	0.304 0	0.306 5	0.304 7	0.310 7	0.307 0	0.313 1	0.308 4
1		0.308 1*	0.311 5*	0.308 6*	0.311 8*	0.310 3*	0.313 0*	0.311 3*	0.313 3*
7/22	41.98	—	—	—	—	—	—	0.343 0	0.188 3
20		—	—	—	—	—	—	0.341 0	0.198 8
18		—	—	—	—	0.309 3	0.196 2	0.339 1	0.208 8
16		—	—	—	—	0.309 9	0.207 4	0.336 8	0.219 2
14		—	—	0.280 1	0.206 8	0.310 1	0.219 2	0.334 1	0.230 8
12		0.266 4	0.212 7	0.283 3	0.219 7	0.310 4	0.232 0	0.331 4	0.242 3
10		0.272 9	0.228 9	0.287 2	0.234 3	0.310 8	0.244 2	0.328 8	0.253 1
8		0.279 9	0.245 9	0.291 8	0.250 4	0.310 9	0.258 4	0.325 6	0.265 4
6		0.287 3	0.263 3	0.296 1	0.266 3	0.311 1	0.273 0	0.322 1	0.278 6
4		0.295 0	0.281 0	0.300 9	0.283 1	0.311 1	0.288 0	0.318 1	0.292 0
3		0.299 1*	0.290 6*	0.303 4*	0.292 1*	0.311 1*	0.296 0*	0.315 9*	0.298 9*
2		0.303 1	0.300 0	0.305 9	0.301 0	0.310 9	0.303 7	0.313 8	0.305 4
1		0.306 8*	0.308 7*	0.308 2*	0.309 2*	0.310 6*	0.310 6*	0.311 8*	0.311 3*
6/26	29.30	—	—	—	—	—	—	0.345 7	0.160 4
24		—	—	—	—	0.305 8	0.154 7	0.344 1	0.169 8
22		—	—	—	—	0.306 2	0.163 8	0.342 6	0.178 5
20		—	—	0.270 2	0.162 1	0.306 9	0.174 5	0.340 9	0.188 2
18		0.250 4	0.165 8	0.273 1	0.173 8	0.307 5	0.187 0	0.338 8	0.199 5
16		0.254 8	0.176 8	0.276 1	0.185 2	0.308 0	0.197 6	0.337 0	0.209 5
14		0.259 3	0.190 9	0.279 4	0.197 9	0.308 4	0.209 5	0.334 9	0.220 3
12		0.264 7	0.205 2	0.282 9	0.212 1	0.309 0	0.222 2	0.332 1	0.232 9
10		0.270 3	0.220 4	0.286 2	0.226 0	0.309 2	0.235 0	0.329 3	0.245 0
8		0.277 0	0.237 2	0.290 5	0.242 1	0.309 9	0.250 2	0.325 9	0.258 4
6		0.284 2	0.255 0	0.295 0	0.258 5	0.310 1	0.265 0	0.322 6	0.271 6
4		0.293 2	0.275 9	0.300 1	0.277 8	0.310 7	0.283 1	0.318 1	0.287 1
3		0.297 4*	0.286 0*	0.302 5*	0.287 2*	0.310 8*	0.291 3*	0.316 4*	0.294 5*
2		0.301 6	0.296 0	0.305 0	0.296 7	0.310 7	0.299 3	0.314 6	0.301 8
1		0.305 8*	0.306 1*	0.307 5*	0.306 3*	0.310 5*	0.307 5*	0.312 6*	0.309 0*
5/30	19.27	—	—	—	—	0.301 0	0.117 0	0.349 0	0.130 8
28		—	—	0.261 8	0.113 5	0.301 8	0.125 3	0.347 8	0.138 8
26		0.234 8	0.114 0	0.263 5	0.122 4	0.302 2	0.133 1	0.346 8	0.146 0
24		0.237 2	0.122 3	0.265 2	0.130 4	0.303 0	0.142 3	0.345 0	0.155 5
22		0.240 2	0.131 5	0.267 3	0.139 8	0.303 8	0.150 0	0.343 7	0.164 4
20		0.243 8	0.141 9	0.269 4	0.149 9	0.304 2	0.160 6	0.342 2	0.173 5
18		0.247 6	0.153 2	0.271 8	0.160 4	0.305 2	0.171 1	0.340 1	0.184 0
16		0.251 5	0.164 4	0.274 4	0.171 8	0.306 0	0.183 0	0.338 2	0.195 1
14		0.256 0	0.177 4	0.277 5	0.184 7	0.306 8	0.195 1	0.336 0	0.206 6
12		0.260 8	0.191 3	0.280 6	0.197 7	0.307 1	0.208 0	0.333 5	0.218 7
10		0.266 5	0.207 5	0.284 5	0.213 7	0.308 0	0.223 0	0.330 8	0.232 8
8		0.272 8	0.224 0	0.288 5	0.229 6	0.308 7	0.237 5	0.328 0	0.246 4
6		0.280 6	0.244 4	0.293 2	0.248 7	0.309 3	0.255 5	0.324 3	0.263 0
4		0.289 8	0.266 7	0.298 6	0.269 9	0.310 0	0.275 0	0.319 8	0.280 7
3		0.294 8*	0.278 8*	0.301 5*	0.281 2*	0.310 2*	0.285 4*	0.317 3*	0.289 7*
2		0.300 0	0.291 2	0.304 5	0.292 8	0.310 3	0.295 9	0.314 8	0.298 6
1		0.305 1*	0.303 8*	0.307 4*	0.304 5*	0.310 3*	0.306 3*	0.312 4*	0.307 5*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	P							
		2.5 P		5.0 P		7.5 P		10.0 P	
		x	y	x	y	x	y	x	y
4/32	11.70	0.226 5	0.077 4	0.257 4	0.083 3	0.296 2	0.090 6	—	—
30		0.228 5	0.084 7	0.258 8	0.090 7	0.296 9	0.097 9	0.344 0	0.108 0
28		0.230 2	0.090 9	0.260 0	0.097 1	0.297 9	0.106 2	0.343 2	0.117 2
26		0.232 2	0.097 8	0.261 8	0.105 2	0.298 6	0.113 5	0.342 8	0.124 8
24		0.234 8	0.106 2	0.263 5	0.113 2	0.299 3	0.122 5	0.342 1	0.133 7
22		0.237 1	0.114 3	0.265 2	0.121 8	0.300 1	0.130 6	0.341 1	0.142 4
20		0.239 4	0.122 1	0.267 0	0.130 0	0.301 0	0.139 6	0.340 0	0.150 0
18		0.243 0	0.133 2	0.269 3	0.140 8	0.301 6	0.150 0	0.338 6	0.162 6
16		0.246 7	0.145 2	0.271 8	0.152 0	0.302 8	0.162 1	0.337 0	0.175 6
14		0.250 9	0.158 5	0.274 7	0.166 0	0.303 5	0.175 5	0.335 1	0.187 5
12		0.255 9	0.173 0	0.277 8	0.180 8	0.304 5	0.190 5	0.333 1	0.201 4
10		0.261 9	0.190 3	0.281 4	0.196 7	0.305 6	0.206 0	0.330 6	0.216 2
8		0.268 5	0.208 9	0.285 5	0.215 0	0.306 6	0.222 8	0.328 0	0.231 8
6		0.276 3	0.230 0	0.290 3	0.234 7	0.307 6	0.241 6	0.324 8	0.249 3
4		0.285 5	0.253 1	0.295 8	0.256 5	0.308 4	0.262 2	0.321 0	0.268 6
3		0.290 6*	0.266 1*	0.298 9*	0.268 8*	0.308 9*	0.273 4*	0.318 7*	0.279 0*
2		0.296 2	0.280 7	0.302 2	0.282 5	0.309 3	0.285 9	0.316 2	0.290 2
1		0.302 6*	0.297 3*	0.305 9*	0.298 2*	0.309 7*	0.300 0*	0.313 3*	0.302 6*
3/34	6.391	0.223 0	0.054 3	—	—	—	—	—	—
32		0.224 2	0.058 7	0.255 7	0.063 0	—	—	—	—
30		0.225 2	0.063 8	0.256 8	0.069 0	0.292 2	0.075 0	—	—
28		0.226 8	0.069 8	0.257 9	0.075 0	0.293 0	0.081 2	—	—
26		0.228 6	0.076 5	0.259 0	0.082 2	0.293 8	0.089 2	0.334 3	0.097 8
24		0.230 5	0.083 2	0.260 2	0.089 1	0.294 4	0.096 7	0.334 1	0.105 5
22		0.232 9	0.091 1	0.262 0	0.097 8	0.295 3	0.105 7	0.334 0	0.114 6
20		0.235 4	0.100 3	0.263 9	0.107 4	0.296 1	0.115 1	0.333 2	0.124 0
18		0.238 0	0.109 4	0.265 7	0.116 3	0.296 9	0.123 9	0.332 9	0.133 2
16		0.241 0	0.119 8	0.268 0	0.127 2	0.298 1	0.135 6	0.332 0	0.145 6
14		0.244 9	0.132 5	0.270 7	0.139 7	0.299 2	0.147 5	0.330 9	0.157 2
12		0.249 8	0.148 0	0.273 9	0.153 9	0.300 3	0.161 8	0.330 1	0.171 5
10		0.254 8	0.163 8	0.277 2	0.170 7	0.302 0	0.179 4	0.328 6	0.188 9
8		0.261 5	0.184 5	0.281 9	0.191 0	0.303 7	0.198 1	0.326 9	0.207 5
6		0.269 1	0.207 2	0.287 0	0.213 5	0.305 7	0.220 8	0.324 3	0.229 3
4		0.279 2	0.234 2	0.292 8	0.238 6	0.307 2	0.244 8	0.321 4	0.251 7
3		0.285 2*	0.249 8*	0.296 0*	0.253 0*	0.308 0*	0.258 3*	0.319 5*	0.264 4*
2		0.292 2	0.268 0	0.299 7	0.270 0	0.308 8	0.274 0	0.317 0	0.279 0
1		0.300 4*	0.289 9*	0.304 3*	0.290 8*	0.309 5*	0.293 0*	0.313 9*	0.296 1*
2/30	3.048	0.223 1	0.043 2	—	—	—	—	—	—
28		0.224 5	0.049 1	0.255 9	0.052 5	—	—	—	—
26		0.226 0	0.055 5	0.256 9	0.059 4	—	—	—	—
24		0.227 7	0.062 1	0.258 2	0.066 9	0.288 2	0.071 9	—	—
22		0.229 8	0.069 6	0.259 7	0.075 0	0.289 0	0.079 9	0.323 0	0.086 1
20		0.232 0	0.077 9	0.261 2	0.083 8	0.290 2	0.090 1	0.323 1	0.096 2
18		0.234 5	0.087 3	0.263 2	0.093 5	0.291 2	0.099 5	0.323 3	0.106 3
16		0.237 2	0.098 0	0.265 2	0.104 5	0.292 2	0.110 6	0.323 5	0.118 1
14		0.240 6	0.110 0	0.267 6	0.116 3	0.293 8	0.123 5	0.323 5	0.131 7
12		0.244 9	0.124 5	0.270 9	0.132 0	0.295 6	0.139 2	0.323 3	0.147 7
10		0.250 1	0.142 2	0.274 8	0.150 0	0.297 9	0.156 9	0.323 0	0.165 9
8		0.257 0	0.163 5	0.279 1	0.170 7	0.300 0	0.178 1	0.321 9	0.186 2
6		0.266 1	0.192 1	0.285 0	0.199 2	0.302 5	0.205 8	0.320 7	0.213 2
4		0.275 8	0.220 8	0.290 8	0.226 1	0.304 8	0.232 1	0.318 9	0.239 0
3		0.281 8*	0.237 7*	0.294 2*	0.241 9*	0.305 9*	0.246 8*	0.317 8*	0.252 7*
2		0.289 2	0.258 3	0.298 4	0.261 2	0.307 1	0.264 7	0.316 1	0.269 1
1		0.298 5*	0.284 0*	0.303 6*	0.285 5*	0.308 5*	0.287 3*	0.313 6*	0.289 8*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	P							
		2.5 P		5.0 P		7.5 P		10.0 P	
		x	y	x	y	x	y	x	y
1/26	1.180	0.225 1	0.035 5	—	—	—	—	—	—
24		0.226 6	0.041 8	—	—	—	—	—	—
22		0.227 9	0.047 3	0.259 0	0.050 9	—	—	—	—
20		0.229 5	0.054 2	0.260 1	0.058 6	0.283 1	0.062 5	—	—
18		0.231 2	0.061 8	0.261 2	0.066 7	0.284 1	0.070 6	0.306 9	0.074 8
16		0.233 1	0.069 6	0.262 5	0.074 6	0.285 2	0.079 0	0.307 8	0.083 9
14		0.236 1	0.081 0	0.264 5	0.086 3	0.286 8	0.090 3	0.308 4	0.095 2
12		0.239 4	0.094 0	0.267 0	0.100 6	0.288 4	0.105 9	0.309 4	0.111 0
10		0.244 1	0.111 2	0.270 1	0.117 8	0.290 5	0.122 9	0.310 2	0.128 2
8		0.249 6	0.130 3	0.274 2	0.137 5	0.293 2	0.142 9	0.311 4	0.148 1
6		0.257 0	0.155 9	0.279 4	0.162 8	0.296 0	0.168 2	0.312 6	0.173 7
4		0.266 8	0.187 4	0.285 4	0.192 7	0.299 1	0.197 4	0.313 2	0.203 2
3		0.272 6*	0.205 1*	0.288 8*	0.209 5*	0.300 8*	0.213 6*	0.313 4*	0.218 9*
2		0.280 8	0.229 6	0.293 6	0.233 0	0.303 0	0.236 1	0.313 2	0.240 4
1		0.292 8*	0.265 3*	0.300 4*	0.267 2*	0.306 0*	0.269 0*	0.312 2*	0.271 6*

Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	RP							
		2.5 RP		5.0 RP		7.5 RP		10.0 RP	
		x	y	x	y	x	y	x	y
9/6	76.69	0.332 2	0.291 0	0.343 1	0.298 8	0.351 2	0.305 2	0.359 0	0.311 8
4		0.323 4	0.301 0	0.330 1	0.306 0	0.335 0	0.309 9	0.340 0	0.314 0
3		0.318 9*	0.306 2*	0.323 3*	0.309 5*	0.326 5*	0.312 2*	0.329 7*	0.314 8*
2		0.314 9	0.310 8	0.317 2	0.312 6	0.319 0	0.314 1	0.320 5	0.315 5
1		0.311 8*	0.314 3*	0.312 6*	0.315 0*	0.313 2*	0.315 5*	0.313 6*	0.316 0*
8/14	57.62	0.362 1	0.249 6	—	—	—	—	—	—
12		0.355 2	0.259 4	0.381 8	0.274 2	0.400 2	0.285 9	—	—
10		0.347 9	0.269 9	0.368 5	0.282 8	0.383 0	0.293 0	0.398 3	0.304 9
8		0.340 6	0.279 3	0.357 0	0.290 0	0.368 2	0.298 3	0.380 0	0.308 2
6		0.332 7	0.289 8	0.344 0	0.297 8	0.352 1	0.304 2	0.360 0	0.311 2
4		0.323 9	0.300 0	0.330 8	0.305 2	0.336 0	0.309 2	0.341 2	0.313 5
3		0.319 4*	0.305 2*	0.324 1*	0.308 8*	0.327 6*	0.311 5*	0.331 1*	0.314 4*
2		0.315 4	0.310 0	0.318 0	0.312 0	0.320 0	0.313 6	0.321 8	0.315 2
1		0.312 2*	0.313 8*	0.313 2*	0.314 6*	0.313 9*	0.315 2*	0.314 5*	0.315 8*
7/20	41.98	0.381 1	0.214 3	—	—	—	—	—	—
18		0.375 1	0.224 1	0.418 6	0.245 9	—	—	—	—
16		0.368 8	0.234 2	0.407 6	0.254 0	0.434 6	0.268 9	0.464 8	0.287 8
14		0.362 0	0.244 8	0.395 8	0.262 8	0.419 5	0.276 2	0.445 6	0.293 1
12		0.355 5	0.254 5	0.384 1	0.271 0	0.404 0	0.283 4	0.426 0	0.298 0
10		0.348 7	0.264 8	0.371 3	0.279 8	0.387 1	0.290 6	0.404 0	0.303 0
8		0.341 7	0.274 5	0.360 3	0.286 9	0.372 2	0.296 3	0.385 1	0.306 7
6		0.333 8	0.285 4	0.347 0	0.294 9	0.356 2	0.302 2	0.364 8	0.309 8
4		0.325 4	0.297 1	0.333 2	0.303 2	0.338 9	0.307 9	0.344 6	0.312 5
3		0.321 1*	0.302 5*	0.326 7*	0.307 0*	0.330 8*	0.310 3*	0.334 9*	0.313 7*
2		0.317 0	0.307 6	0.320 6	0.310 4	0.323 2	0.312 5	0.325 8	0.314 8
1		0.313 3*	0.312 2*	0.315 0*	0.313 5*	0.316 3*	0.314 5*	0.317 5*	0.315 7*
6/24	29.30	0.392 7	0.189 2	—	—	—	—	—	—
22		0.387 7	0.197 8	0.444 9	0.221 9	—	—	—	—
20		0.383 3	0.205 6	0.436 8	0.228 3	0.473 5	0.246 4	—	—
18		0.377 3	0.215 8	0.424 5	0.238 2	0.458 1	0.254 9	0.496 1	0.275 1
16		0.371 8	0.225 1	0.413 6	0.246 7	0.444 8	0.262 2	0.478 1	0.281 2
14		0.365 2	0.235 5	0.402 3	0.255 2	0.428 5	0.270 5	0.455 2	0.288 1
12		0.358 2	0.246 2	0.390 0	0.264 6	0.412 5	0.278 4	0.436 0	0.293 6
10		0.350 9	0.257 8	0.376 9	0.273 8	0.396 0	0.286 0	0.415 0	0.298 9
8		0.343 7	0.268 8	0.364 8	0.282 0	0.379 1	0.292 9	0.393 0	0.303 8
6		0.336 2	0.279 9	0.352 0	0.290 4	0.363 5	0.298 7	0.374 0	0.307 4
4		0.327 2	0.292 9	0.337 1	0.300 1	0.343 9	0.305 6	0.350 8	0.311 2
3		0.323 0*	0.298 9*	0.330 0*	0.304 4*	0.334 8*	0.308 6*	0.339 7*	0.312 7*
2		0.318 8	0.304 8	0.323 2	0.308 5	0.326 1	0.311 3	0.329 2	0.311 1
1		0.314 5*	0.310 6*	0.316 6*	0.312 4*	0.317 9*	0.313 9*	0.319 3*	0.315 3*
5/26	19.27	0.401 1	0.165 2	—	—	—	—	—	—
24		0.396 5	0.173 8	0.468 3	0.197 8	—	—	—	—
22		0.392 4	0.181 4	0.458 1	0.206 8	0.504 5	0.224 8	—	—
20		0.387 3	0.190 9	0.448 4	0.215 0	0.491 5	0.233 0	0.539 6	0.253 5
18		0.382 1	0.200 7	0.437 2	0.224 2	0.476 1	0.242 1	0.518 5	0.262 0
16		0.376 3	0.210 8	0.426 1	0.233 1	0.461 7	0.250 6	0.498 6	0.269 5
14		0.370 3	0.221 1	0.414 2	0.242 8	0.445 4	0.259 6	0.476 7	0.277 6
12		0.363 5	0.232 5	0.402 2	0.252 3	0.430 3	0.267 5	0.457 9	0.284 1
10		0.356 1	0.245 2	0.388 0	0.263 0	0.410 8	0.277 3	0.433 2	0.291 8
8		0.349 0	0.257 0	0.374 8	0.272 9	0.393 2	0.285 2	0.410 5	0.298 0
6		0.339 6	0.271 8	0.358 5	0.284 2	0.372 6	0.294 1	0.385 1	0.303 9
4		0.329 8	0.286 9	0.342 1	0.295 4	0.351 5	0.302 4	0.359 4	0.309 0
3		0.324 8*	0.294 4*	0.333 8*	0.301 0*	0.340 4*	0.306 2*	0.346 1*	0.311 2*
2		0.319 9	0.301 9	0.325 6	0.306 5	0.329 6	0.309 8	0.333 2	0.313 1
1		0.315 0*	0.309 2*	0.317 7*	0.311 6*	0.319 4*	0.313 2*	0.321 0*	0.314 8*



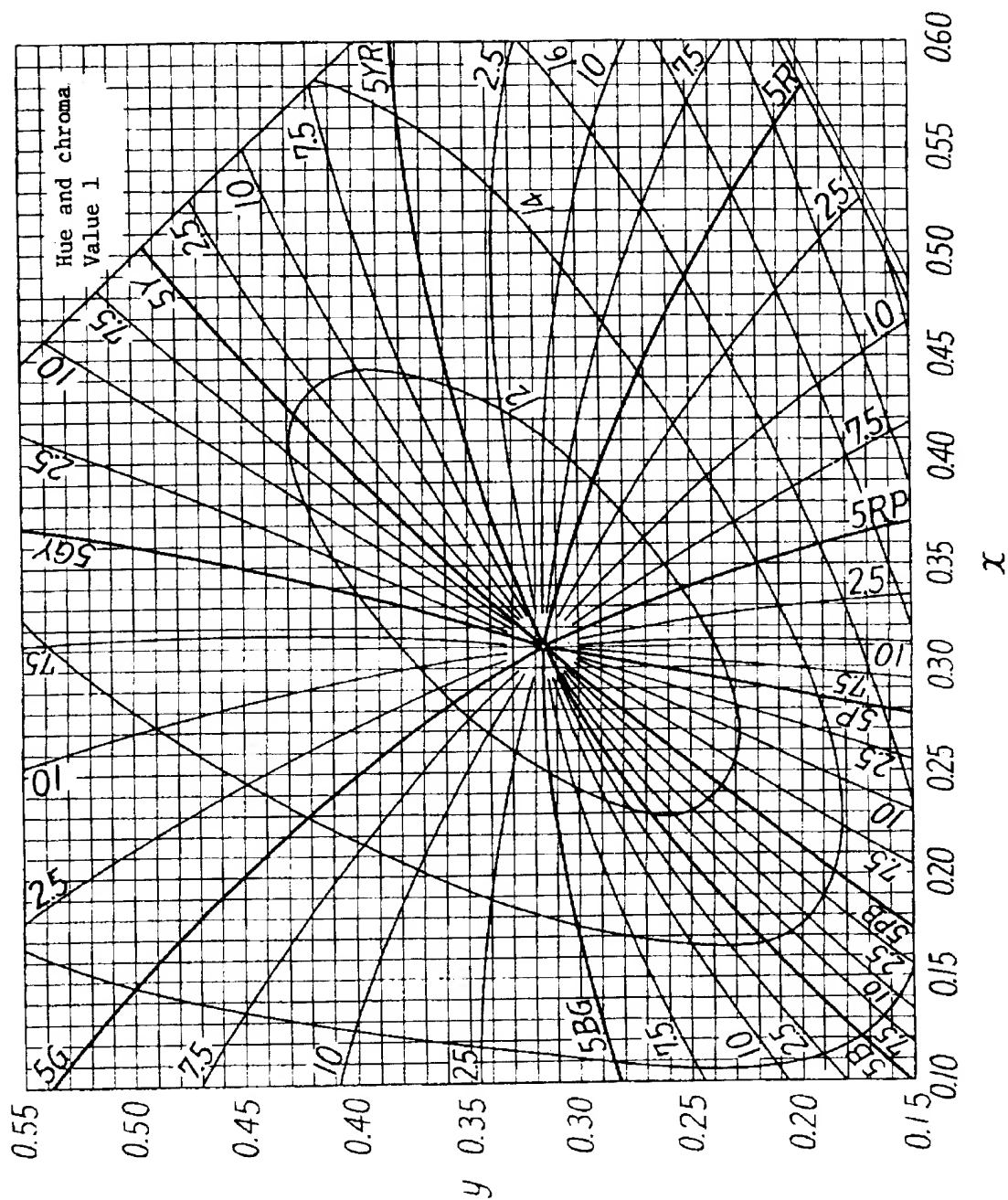
Attached Table 2. (continued)

V/C	Y <sub>c</sub> (%)	RP							
		2.5 RP		5.0 RP		7.5 RP		10.0 RP	
		x	y	x	y	x	y	x	y
4/26	11.70	0.404 8	0.142 8	—	—	—	—	—	—
24		0.401 1	0.150 4	—	—	—	—	—	—
22		0.396 7	0.159 3	0.465 6	0.182 1	—	—	—	—
20		0.392 6	0.167 9	0.457 1	0.190 6	0.513 0	0.210 1	0.567 4	0.231 9
18		0.386 5	0.180 2	0.445 5	0.202 3	0.496 5	0.221 7	0.546 6	0.242 4
16		0.380 7	0.192 3	0.433 9	0.213 9	0.479 9	0.232 9	0.523 4	0.253 0
14		0.374 8	0.203 9	0.422 5	0.224 9	0.462 9	0.243 7	0.502 0	0.262 3
12		0.368 3	0.216 2	0.410 4	0.236 1	0.445 0	0.254 1	0.478 9	0.271 7
10		0.360 8	0.230 1	0.396 0	0.248 9	0.425 9	0.265 1	0.452 8	0.281 1
8		0.353 3	0.243 8	0.383 3	0.260 0	0.407 2	0.275 0	0.428 2	0.289 0
6		0.344 2	0.259 5	0.367 1	0.273 3	0.385 0	0.285 9	0.399 9	0.297 2
4		0.334 0	0.277 0	0.349 1	0.287 2	0.361 2	0.296 3	0.371 5	0.304 2
3		0.328 7*	0.285 8*	0.340 2*	0.294 0*	0.349 4*	0.301 2*	0.356 8*	0.307 5*
2		0.323 1	0.295 1	0.331 0	0.301 0	0.337 1	0.306 1	0.341 7	0.310 6
1		0.317 0*	0.305 2*	0.321 1*	0.308 4*	0.324 1*	0.311 1*	0.326 1*	0.313 5*
3/22	6.391	0.401 8	0.130 4	—	—	—	—	—	—
20		0.396 9	0.141 3	0.457 7	0.159 3	—	—	—	—
18		0.392 9	0.150 6	0.450 3	0.169 5	0.513 0	0.189 3	—	—
16		0.387 6	0.162 9	0.441 8	0.180 9	0.499 1	0.201 1	0.562 8	0.224 1
14		0.381 8	0.175 8	0.431 3	0.194 4	0.483 1	0.214 0	0.538 0	0.236 9
12		0.375 4	0.189 8	0.419 9	0.208 9	0.465 4	0.227 3	0.513 9	0.248 9
10		0.368 1	0.205 4	0.407 3	0.223 5	0.444 5	0.241 9	0.485 1	0.261 8
8		0.359 8	0.223 3	0.393 0	0.239 5	0.423 4	0.255 6	0.455 2	0.274 1
6		0.350 1	0.242 5	0.376 5	0.256 9	0.399 0	0.270 8	0.421 8	0.286 4
4		0.340 0	0.262 4	0.358 6	0.274 2	0.373 9	0.285 1	0.388 9	0.296 9
3		0.334 0*	0.273 6*	0.348 4*	0.283 8*	0.360 1*	0.292 5*	0.371 4*	0.301 9*
2		0.327 2	0.286 1	0.337 0	0.294 0	0.345 0	0.300 1	0.352 6	0.306 8
1		0.319 3*	0.300 2*	0.324 3*	0.304 8*	0.328 4*	0.308 0*	0.332 3*	0.311 6*
2/20	3.048	0.380 2	0.108 0	—	—	—	—	—	—
18		0.377 8	0.118 8	0.433 8	0.134 0	—	—	—	—
16		0.374 8	0.131 0	0.426 9	0.145 4	0.474 4	0.159 5	—	—
14		0.371 1	0.144 9	0.418 0	0.159 8	0.462 4	0.173 7	0.512 9	0.188 8
12		0.366 8	0.161 8	0.408 0	0.176 4	0.448 1	0.190 3	0.491 1	0.206 0
10		0.361 7	0.180 0	0.397 1	0.193 9	0.432 1	0.208 2	0.467 8	0.223 7
8		0.355 5	0.200 3	0.385 8	0.214 0	0.413 7	0.227 6	0.442 8	0.241 9
6		0.347 0	0.225 9	0.370 8	0.238 0	0.391 8	0.249 0	0.413 9	0.260 8
4		0.338 2	0.249 6	0.355 8	0.259 7	0.370 2	0.268 3	0.385 0	0.277 8
3		0.333 6*	0.261 4*	0.347 9	0.270 6*	0.358 9*	0.278 3*	0.370 0*	0.286 5*
2		0.327 9	0.275 4	0.338 3	0.282 9	0.345 9	0.289 2	0.353 2	0.295 7
1		0.320 3*	0.293 2*	0.326 0*	0.297 8*	0.330 0*	0.301 7*	0.333 6*	0.305 6*
1/16	1.180	0.336 8	0.090 2	—	—	—	—	—	—
14		0.336 8	0.102 0	0.381 1	0.113 8	—	—	—	—
12		0.336 1	0.118 1	0.377 2	0.128 3	0.424 0	0.140 0	0.466 8	0.151 4
10		0.335 4	0.135 1	0.372 7	0.145 8	0.413 2	0.158 0	0.452 1	0.171 0
8		0.334 2	0.155 1	0.366 0	0.166 2	0.400 5	0.179 3	0.435 7	0.192 1
6		0.332 1	0.181 1	0.358 8	0.192 0	0.386 5	0.203 6	0.415 1	0.216 9
4		0.329 0	0.209 5	0.350 3	0.219 6	0.370 5	0.230 0	0.392 0	0.242 3
3		0.327 2*	0.225 1*	0.345 3*	0.234 7*	0.361 6*	0.244 1*	0.379 3*	0.255 4*
2		0.324 0	0.245 9	0.337 8	0.254 2	0.349 8	0.261 7	0.362 9	0.271 0
1		0.318 6*	0.275 2*	0.326 6*	0.280 5*	0.333 2*	0.285 0*	0.340 6*	0.290 7*

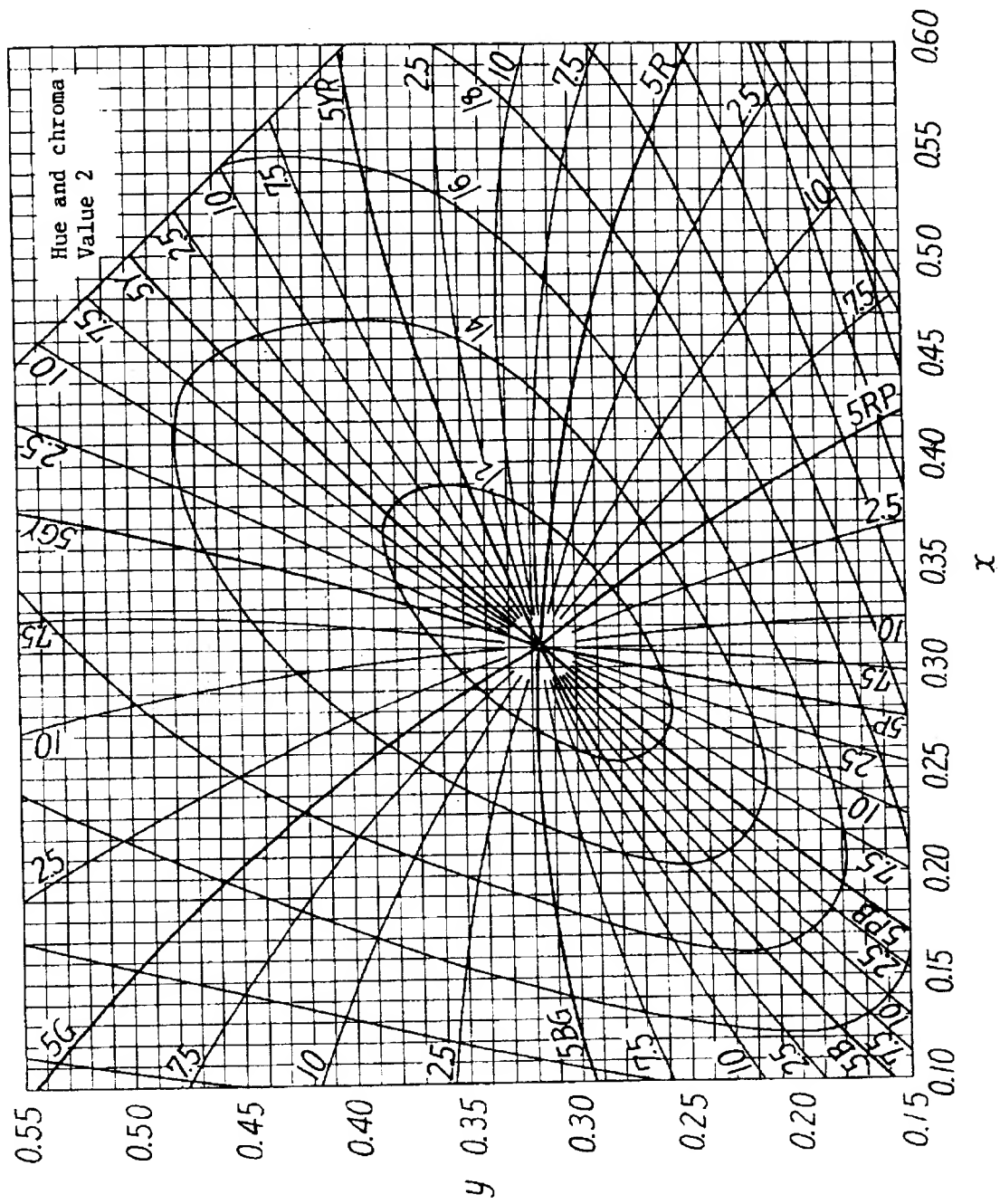
Note \*: These values have been obtained by the cubic interpolation from the values given in the original text.

Remarks: This table has been reprinted from "Journal of the Optical Society of America, Vol. 33 (1943), pp. 397 to 405, Table 1" with permission of the author. However, Y<sub>c</sub>(%) was calculated by the formula shown in Remarks of Attached Table 1.

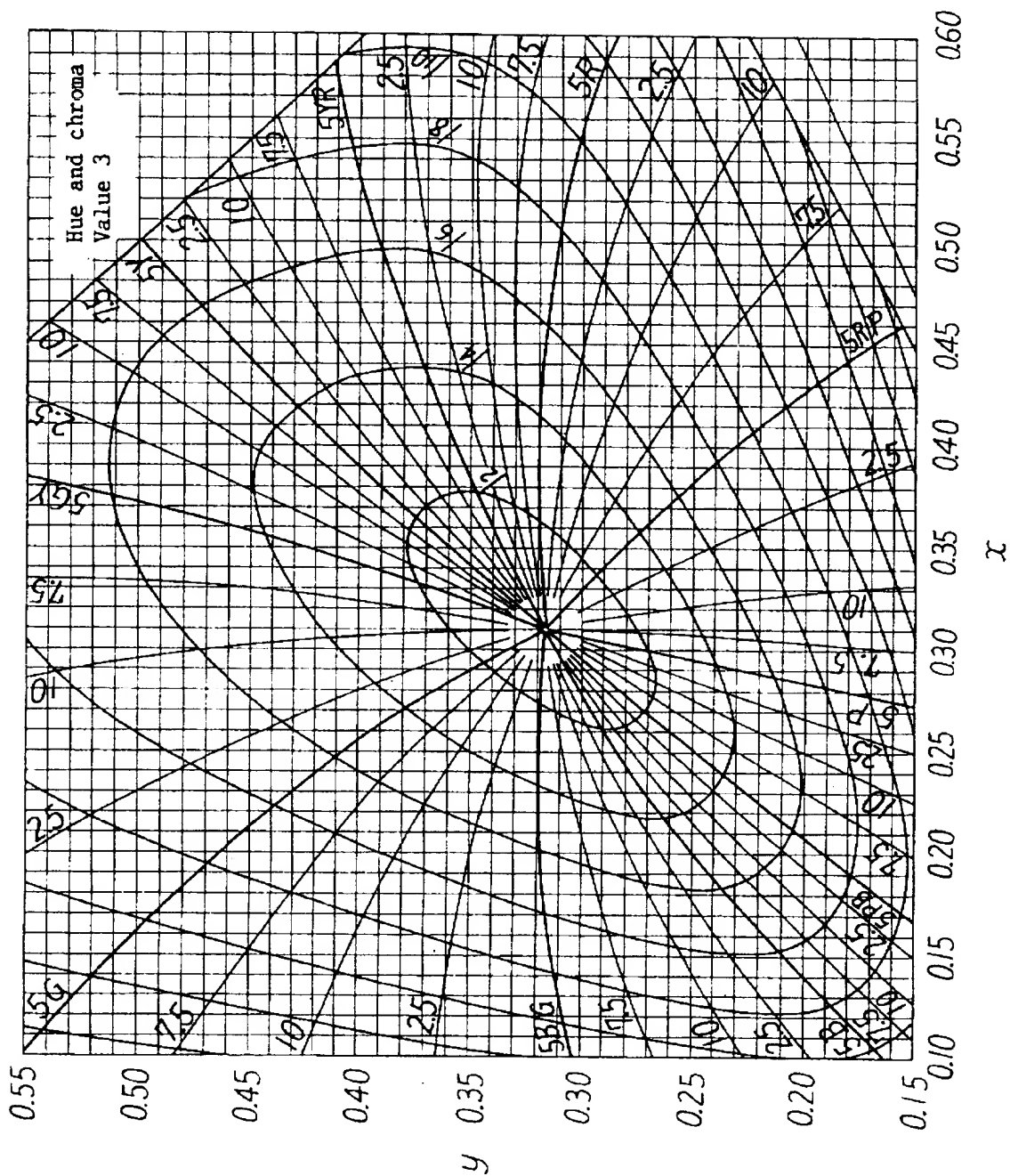
Attached Fig. 1



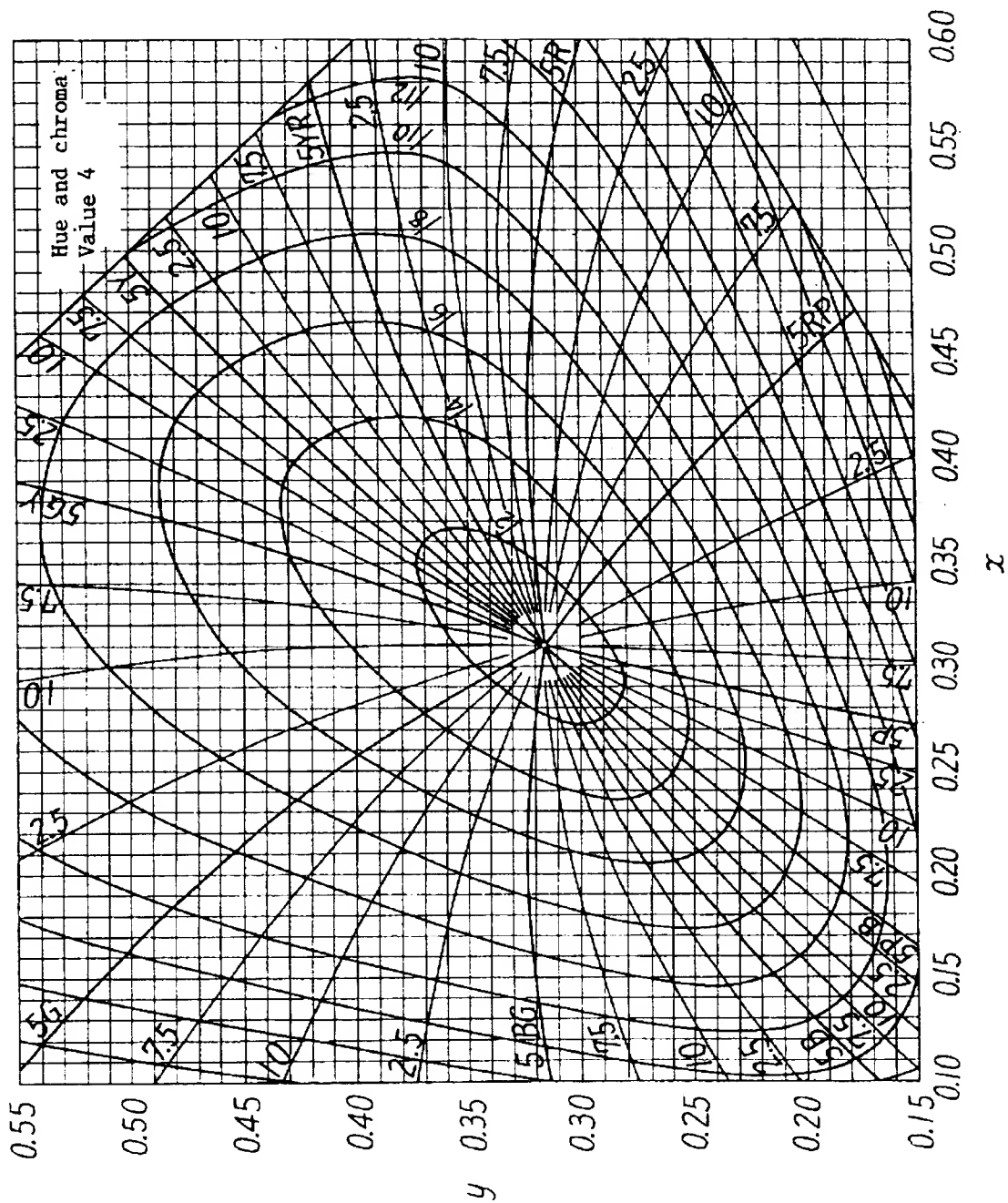
Attached Fig. 2



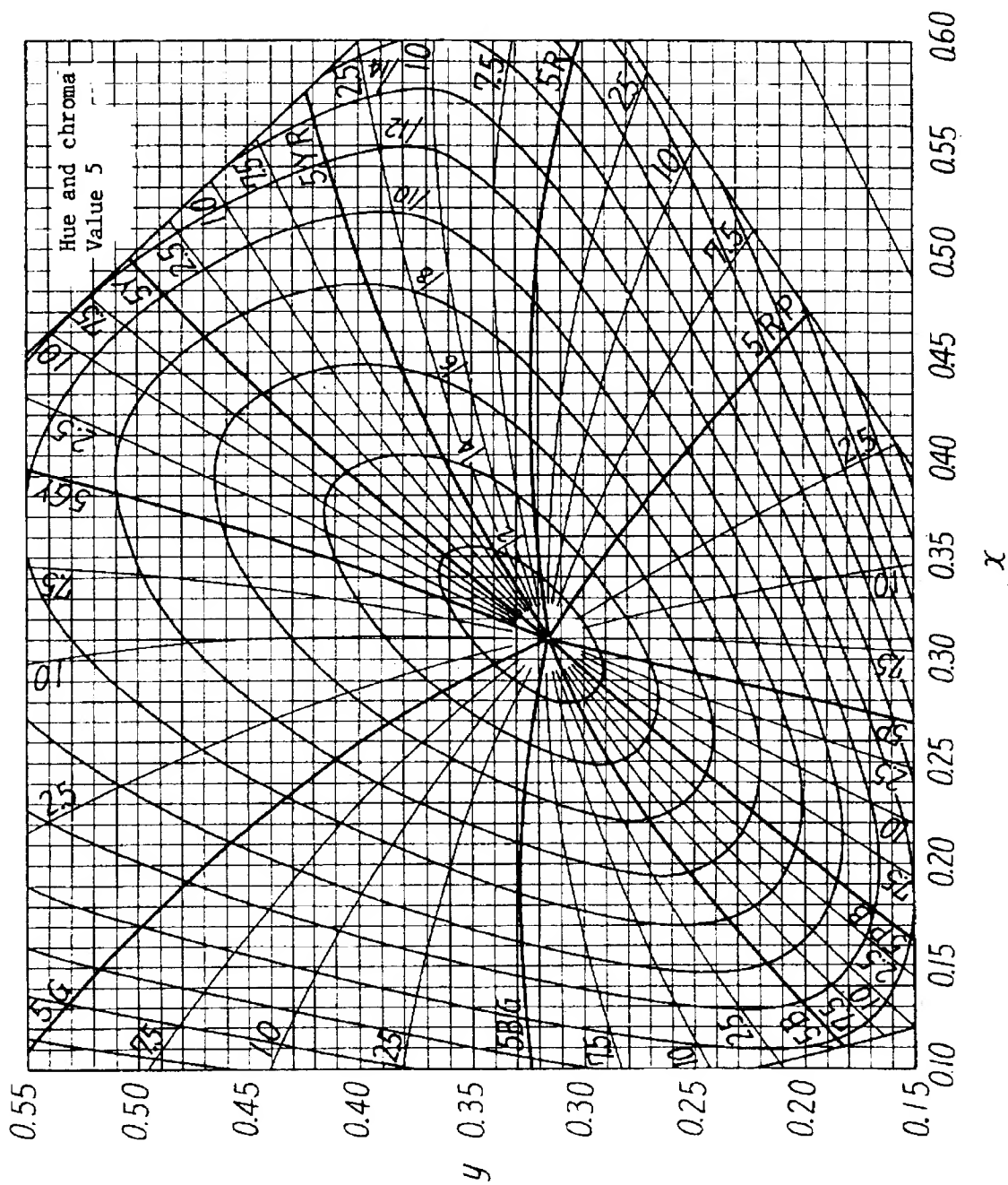
Attached Fig. 3



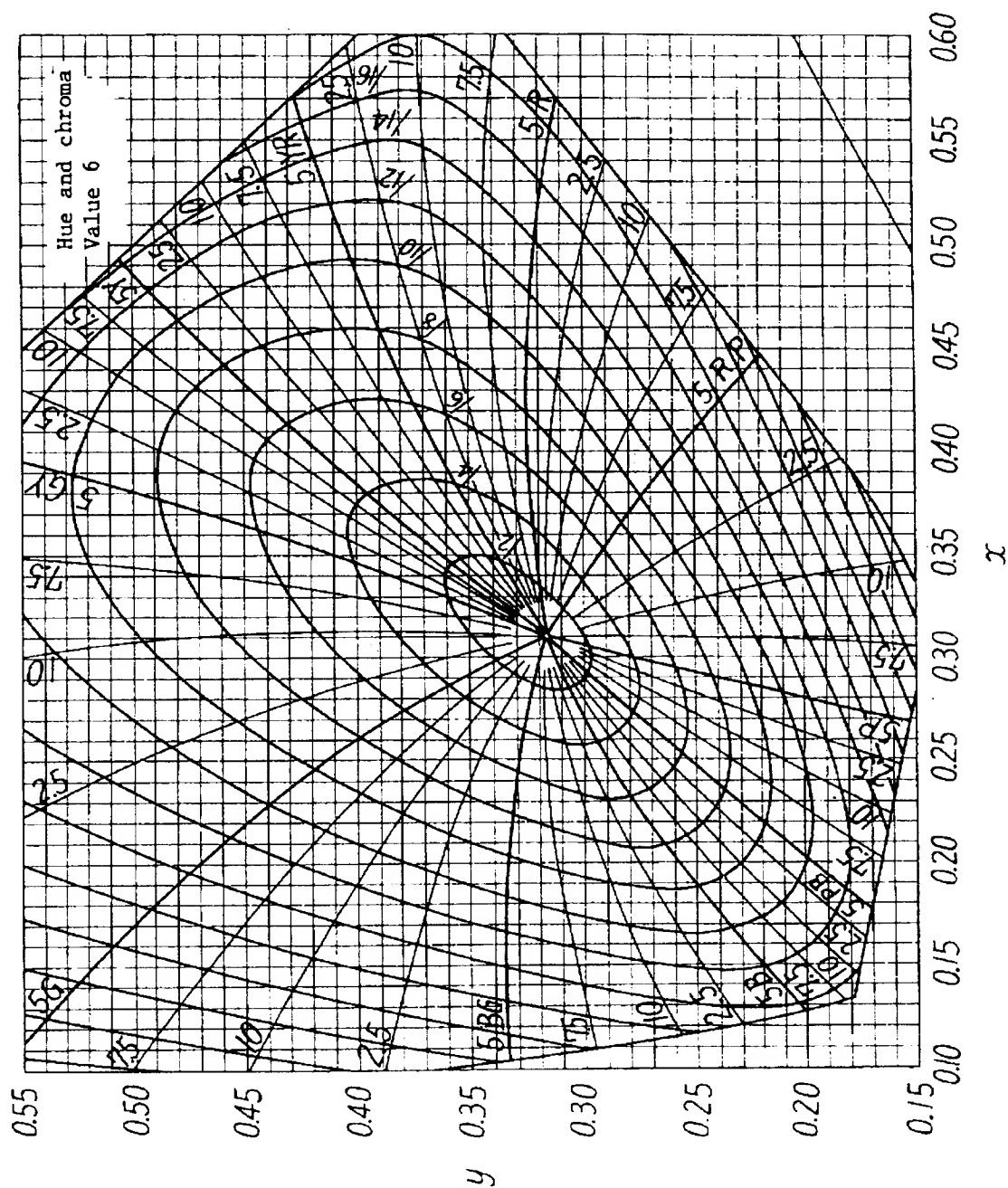
Attached Fig. 4



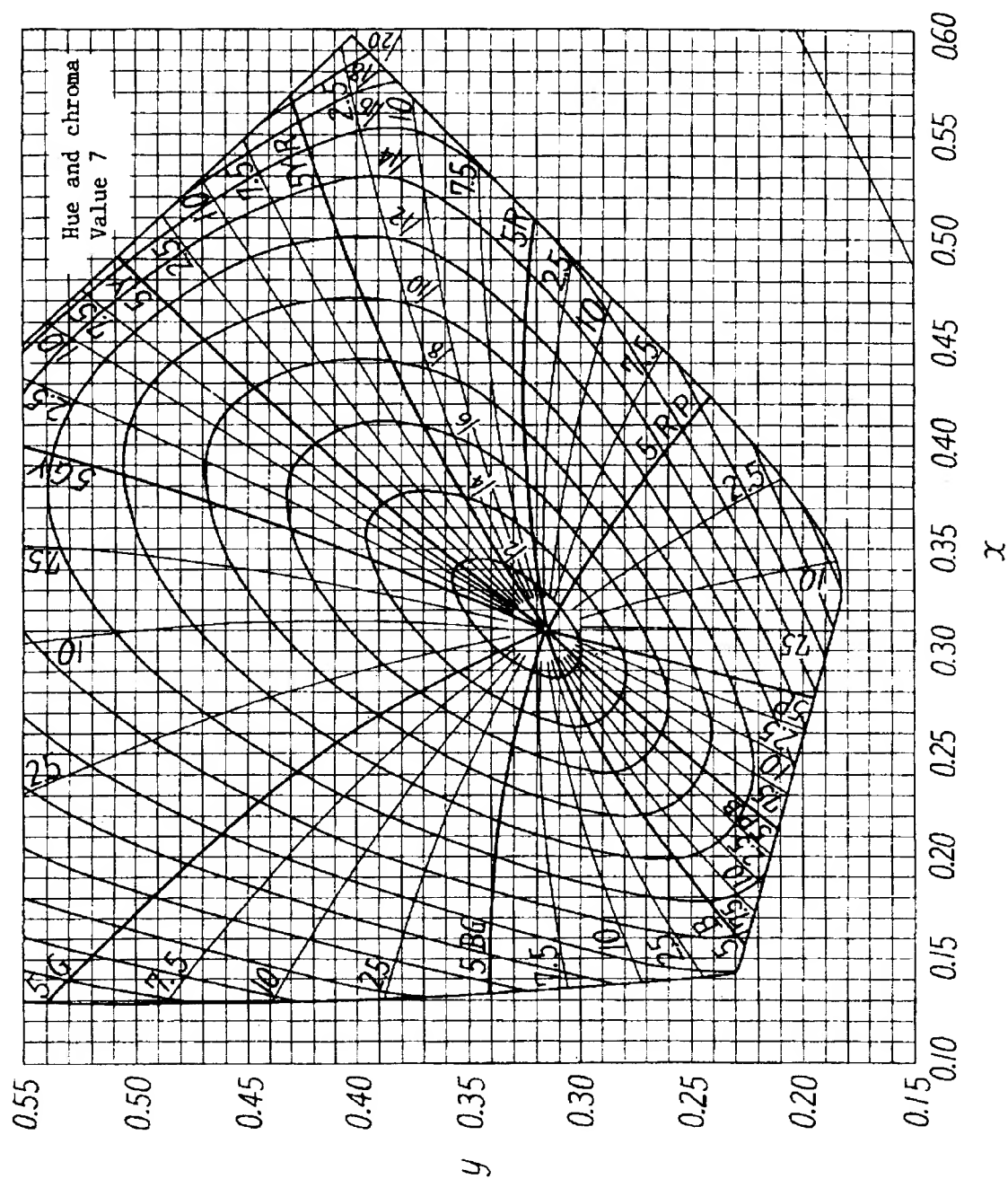
Attached Fig. 5



Attached Fig. 6

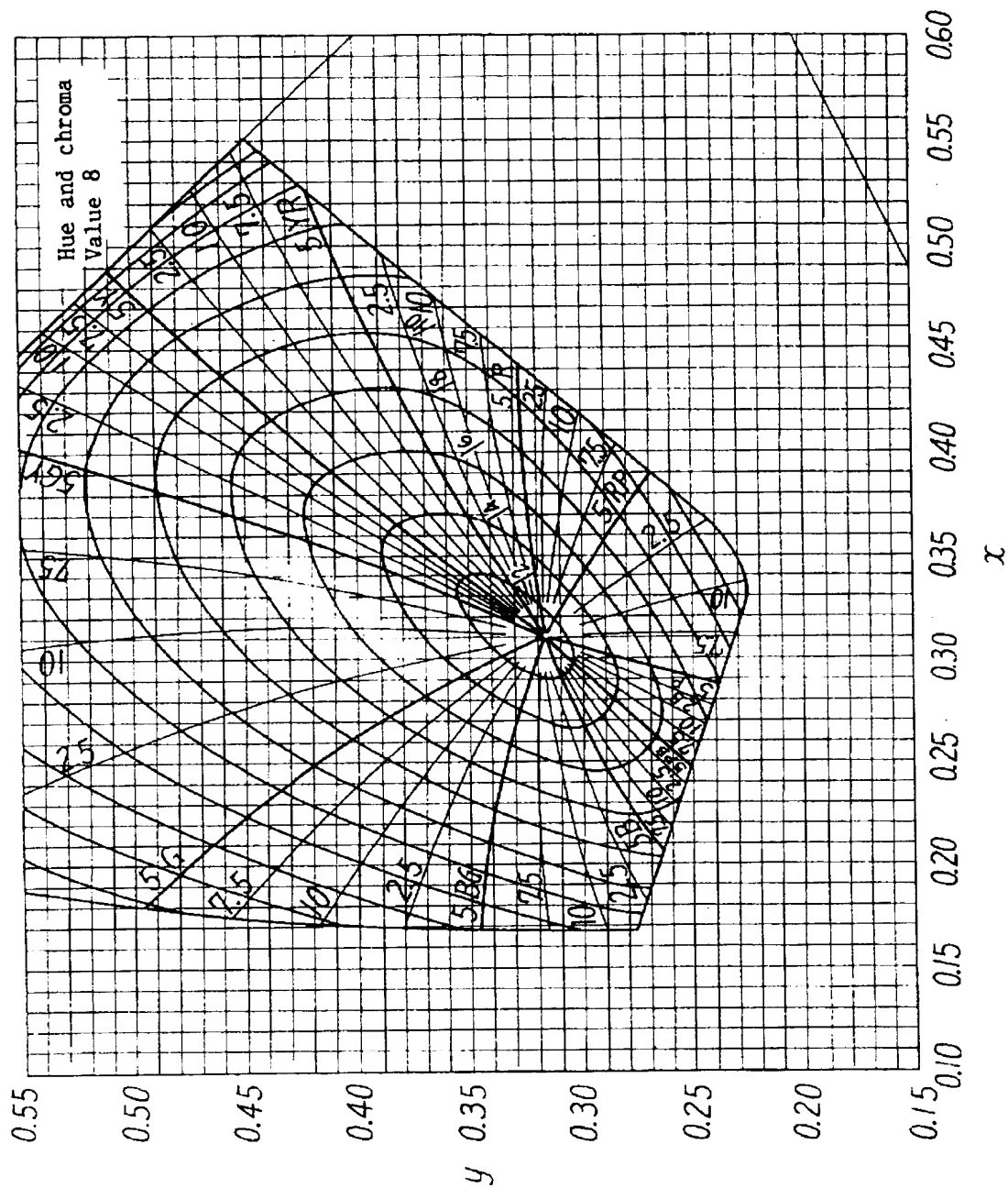


Attached Fig. 7

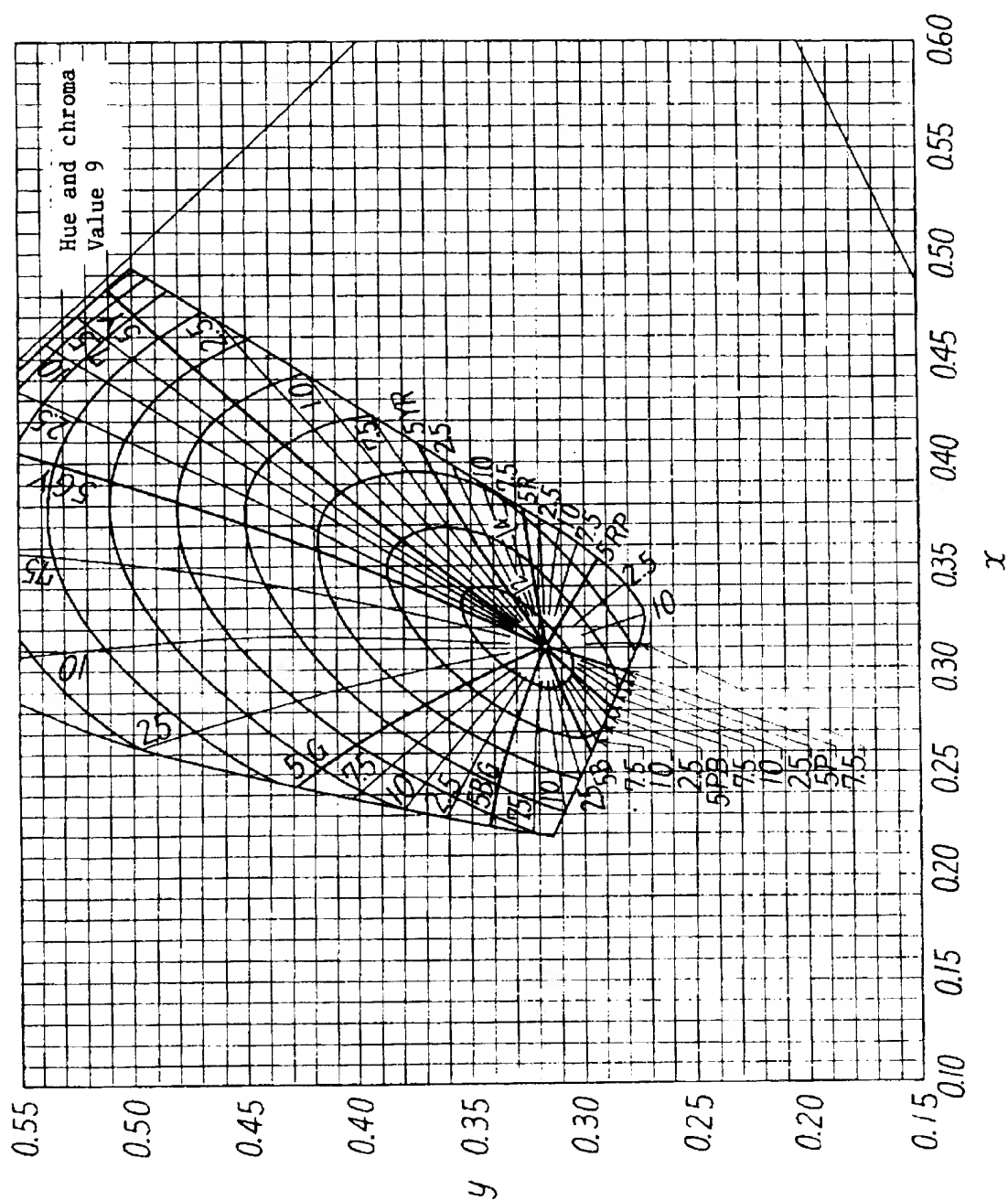




Attached Fig. 8



Attached Fig. 9



Annex Basis of colour system according to three attributes  
under illumination by standard illuminant D<sub>65</sub>

1. Scope This Annex specifies the basis on which the basis  $Y_c, x_c, y_c$  of the colour system according to three attributes under the lighting by the standard illuminant C is converted to the basis  $Y_D, x_D, y_D$  of the colour system under the lighting by the standard illuminant D<sub>65</sub>.

2. Basis of colour system according to three attributes under the illumination by standard illuminant D<sub>65</sub> The basis of colour system according to three attributes under the illumination by standard illuminant D<sub>65</sub> shall be  $Y_D$  of luminance factor and the values of chromaticity coordinates  $x_D, y_D$  shown in Annex Attached Table 1.

The relation between the hue and chroma of the equal lightness and the values of chromaticity coordinates  $x_D, y_D$  is shown in Annex Attached Figs. 1 to 9.

3. Determination of notation to specify colours The notation to specify colours shall be, in the method to obtain from the values of  $Y_D, x_D$  and  $y_D$ , determined by means of interpolation or extrapolation<sup>(5)</sup> using Annex Attached Table 1.

Note (5) Example of calculation by interpolation is shown in Informative reference 2.

4. Recording of notation to specify colours The notation to specify colours shall be recorded as shown in the following examples as to hue  $H_D$ , value  $V_D$  and chroma  $C_D$  for chromatic colours and as to value  $V_D$  for achromatic colours:

Example 1. When  $H_D = 5R$ ,  $V_D = 4$  and  $C_D = 10$  in chromatic colour,

5R 4/10 [D]

Example 2. When  $H_D = 7.5P$ ,  $V_D = 2.5$  and  $C_D = 2.5$  in chromatic colour,

7.5P 2.5/2.5 [D]

Example 3. When  $V_D = 8$  in achromatic colour,

N8 [D]

Example 4. When  $H_D = 7.5R$ ,  $V_D = 5.5$  and  $C_D = 0.3$  in chromatic colour,

N5.5 (R0.3) [D]

Annex Attached Table 1. Basis of colour system according to three attributes (chromatic colour).

2.5R				5R			7.5R			10R		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/6	75.93	0.3710	0.3286	75.96	0.3778	0.3360	76.00	0.3855	0.3454	76.06	0.3923	0.3548
4	76.42	0.3478	0.3294	76.41	0.3528	0.3339	76.37	0.3584	0.3394	76.40	0.3631	0.3458
3	76.55	0.3357	0.3295	76.54	0.3391	0.3327	76.52	0.3431	0.3363	76.51	0.3465	0.3406
2	76.60	0.3239	0.3293	76.59	0.3269	0.3312	76.58	0.3292	0.3333	76.58	0.3313	0.3356
1	76.64	0.3168	0.3292	76.64	0.3176	0.3300	76.63	0.3185	0.3308	76.63	0.3193	0.3315
8/10	56.52	0.4182	0.3236	56.50	0.4308	0.3348	56.46	0.4444	0.3489	56.56	0.4537	0.3654
8	57.06	0.3942	0.3264	57.01	0.4043	0.3352	57.01	0.4156	0.3470	57.16	0.4241	0.3610
6	57.38	0.3705	0.3283	57.36	0.3776	0.3353	57.35	0.3861	0.3437	57.34	0.3938	0.3541
4	57.45	0.3492	0.3293	57.44	0.3542	0.3338	57.43	0.3595	0.3391	57.42	0.3650	0.3459
3	57.50	0.3374	0.3294	57.49	0.3408	0.3324	57.48	0.3445	0.3363	57.47	0.3484	0.3408
2	57.54	0.3266	0.3293	57.53	0.3283	0.3309	57.53	0.3306	0.3334	57.52	0.3330	0.3359
1	57.57	0.3180	0.3292	57.57	0.3185	0.3298	57.56	0.3195	0.3310	57.56	0.3205	0.3318
7/16	41.03	0.4975	0.3115	—	—	—	41.02	0.5403	0.3499	41.11	0.5551	0.3757
14	41.21	0.4723	0.3148	41.18	0.4906	0.3295	41.19	0.5106	0.3496	41.28	0.5262	0.3736
12	41.50	0.4481	0.3195	41.47	0.4637	0.3322	41.51	0.4809	0.3498	41.55	0.4949	0.3716
10	41.66	0.4222	0.3233	41.65	0.4355	0.3344	41.64	0.4500	0.3491	41.64	0.4622	0.3667
8	41.73	0.3998	0.3257	41.72	0.4102	0.3349	41.70	0.4227	0.3470	41.70	0.4334	0.3616
6	41.79	0.3763	0.3276	41.78	0.3839	0.3347	41.77	0.3919	0.3436	41.76	0.4012	0.3548
4	41.86	0.3532	0.3285	41.85	0.3584	0.3334	41.84	0.3642	0.3392	41.83	0.3700	0.3468
3	41.89	0.3421	0.3289	41.88	0.3457	0.3323	41.87	0.3500	0.3366	41.87	0.3542	0.3420
2	41.91	0.3314	0.3292	41.91	0.3336	0.3311	41.91	0.3365	0.3340	41.90	0.3389	0.3372
1	41.94	0.3216	0.3293	41.94	0.3225	0.3300	41.94	0.3239	0.3315	41.93	0.3250	0.3328
6/18	28.87	0.5332	0.2990	28.87	0.5606	0.3187	28.88	0.5858	0.3426	28.85	0.6009	0.3735
16	28.90	0.5092	0.3041	28.88	0.5336	0.3227	28.87	0.5583	0.3457	28.88	0.5746	0.3739
14	28.94	0.4834	0.3108	28.93	0.5056	0.3270	28.92	0.5290	0.3479	28.92	0.5478	0.3734
12	28.99	0.4610	0.3157	28.98	0.4796	0.3302	28.97	0.4988	0.3487	28.97	0.5165	0.3716
10	29.04	0.4360	0.3202	29.03	0.4516	0.3328	29.02	0.4684	0.3483	29.02	0.4832	0.3682
8	29.10	0.4103	0.3237	29.08	0.4222	0.3340	29.08	0.4349	0.3466	29.07	0.4474	0.3627
6	29.14	0.3868	0.3260	29.13	0.3955	0.3342	29.13	0.4032	0.3435	29.12	0.4131	0.3564
4	29.19	0.3600	0.3274	29.18	0.3661	0.3330	29.18	0.3724	0.3398	29.17	0.3797	0.3485
3	29.22	0.3472	0.3281	29.21	0.3514	0.3321	29.20	0.3566	0.3374	29.20	0.3621	0.3436
2	29.24	0.3349	0.3286	29.24	0.3374	0.3310	29.23	0.3411	0.3346	29.23	0.3447	0.3385
1	29.26	0.3235	0.3291	29.26	0.3243	0.3299	29.26	0.3264	0.3319	29.25	0.3280	0.3336
5/20	19.05	0.5848	0.2771	19.05	0.6180	0.3005	19.05	0.6402	0.3234	—	—	—
18	18.99	0.5598	0.2849	18.99	0.5958	0.3070	19.00	0.6182	0.3296	19.10	0.6301	0.3642
16	18.94	0.5351	0.2928	18.93	0.5675	0.3138	18.93	0.5924	0.3356	18.95	0.6040	0.3672
14	18.99	0.5095	0.3007	18.98	0.5378	0.3204	18.97	0.5615	0.3406	18.98	0.5778	0.3689
12	19.02	0.4866	0.3067	19.01	0.5108	0.3250	19.01	0.5307	0.3436	19.01	0.5493	0.3696
10	19.07	0.4576	0.3133	19.06	0.4784	0.3295	19.05	0.4956	0.3459	19.05	0.5131	0.3680
8	19.11	0.4293	0.3187	19.10	0.4449	0.3320	19.09	0.4594	0.3461	19.09	0.4736	0.3641
6	19.15	0.3998	0.3226	19.14	0.4114	0.3330	19.13	0.4212	0.3436	19.13	0.4326	0.3582
4	19.18	0.3695	0.3255	19.18	0.3774	0.3325	19.17	0.3838	0.3396	19.17	0.3909	0.3497
3	19.20	0.3541	0.3267	19.20	0.3596	0.3318	19.20	0.3644	0.3371	19.19	0.3699	0.3446
2	19.22	0.3392	0.3276	19.22	0.3423	0.3309	19.22	0.3456	0.3345	19.21	0.3495	0.3393
1	19.24	0.3253	0.3284	19.24	0.3265	0.3300	19.24	0.3282	0.3318	19.23	0.3303	0.3340
4/20	—	—	—	—	—	—	11.49	0.6810	0.3001	—	—	—
18	11.52	0.5957	0.2665	11.55	0.6360	0.2908	11.60	0.6552	0.3115	—	—	—
16	11.55	0.5679	0.2767	11.55	0.6076	0.3006	11.56	0.6281	0.3209	11.63	0.6412	0.3534
14	11.49	0.5423	0.2854	11.48	0.5774	0.3089	11.49	0.5985	0.3291	11.54	0.6162	0.3578
12	11.52	0.5123	0.2952	11.51	0.5424	0.3173	11.51	0.5630	0.3356	11.52	0.5812	0.3612
10	11.55	0.4822	0.3035	11.54	0.5081	0.3232	11.54	0.5264	0.3399	11.54	0.5435	0.3619
8	11.58	0.4517	0.3108	11.57	0.4728	0.3278	11.57	0.4881	0.3421	11.57	0.5017	0.3612
6	11.61	0.4182	0.3174	11.60	0.4336	0.3309	11.60	0.4448	0.3418	11.60	0.4562	0.3573
4	11.63	0.3844	0.3226	11.63	0.3952	0.3320	11.63	0.4024	0.3394	11.62	0.4108	0.3503
3	11.65	0.3671	0.3246	11.64	0.3749	0.3318	11.64	0.3798	0.3373	11.64	0.3863	0.3456
2	11.66	0.3495	0.3264	11.66	0.3541	0.3312	11.66	0.3570	0.3347	11.65	0.3613	0.3403
1	11.67	0.3314	0.3278	11.67	0.3334	0.3302	11.67	0.3346	0.3319	11.67	0.3366	0.3347

Annex Attached Table 1. (continued)

	2.5R			5R			7.5R			10R		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
3/16	6.151	0.616 8	0.248 9	6.152	0.655 1	0.268 1	6.182	0.682 5	0.288 2	—	—	—
14	6.249	0.588 1	0.261 7	6.252	0.623 8	0.281 5	6.274	0.650 9	0.302 7	6.362	0.670 0	0.325 6
12	6.288	0.559 4	0.273 4	6.289	0.592 6	0.293 5	6.298	0.618 4	0.314 9	6.310	0.633 3	0.337 1
10	6.280	0.524 6	0.285 9	6.276	0.554 4	0.306 2	6.276	0.576 1	0.326 9	6.279	0.588 9	0.346 1
8	6.301	0.487 2	0.298 0	6.298	0.510 6	0.316 7	6.297	0.528 3	0.334 3	6.298	0.541 6	0.351 5
6	6.322	0.445 5	0.308 6	6.319	0.463 2	0.323 8	6.318	0.477 2	0.338 0	6.318	0.488 2	0.352 6
4	6.341	0.406 3	0.316 7	6.338	0.418 7	0.327 6	6.337	0.427 5	0.338 5	6.337	0.433 9	0.349 2
3	6.350	0.385 1	0.320 4	6.348	0.394 0	0.328 8	6.347	0.400 6	0.337 2	6.347	0.405 5	0.346 0
2	6.360	0.362 7	0.323 7	6.359	0.368 0	0.329 5	6.358	0.372 4	0.335 1	6.358	0.376 1	0.341 6
1	6.370	0.338 8	0.326 5	6.369	0.341 0	0.329 5	6.369	0.343 2	0.332 3	6.369	0.345 3	0.335 9
2/14	2.867	0.579 9	0.211 8	2.854	0.632 4	0.229 8	2.854	0.680 3	0.252 6	2.861	0.716 7	0.273 7
12	2.940	0.549 8	0.229 6	2.930	0.597 3	0.249 7	2.930	0.641 5	0.272 4	2.955	0.673 8	0.294 8
10	2.986	0.518 9	0.248 0	2.983	0.561 0	0.267 4	2.982	0.598 7	0.290 3	2.992	0.626 5	0.313 9
8	2.995	0.484 1	0.265 0	2.992	0.520 0	0.284 6	2.991	0.547 8	0.306 3	2.990	0.574 4	0.328 3
6	3.008	0.444 6	0.283 2	3.005	0.469 3	0.299 8	3.004	0.491 9	0.317 8	3.003	0.512 9	0.337 7
4	3.018	0.407 0	0.298 5	3.016	0.423 0	0.311 2	3.015	0.437 7	0.324 4	3.014	0.451 7	0.339 8
3	3.023	0.387 2	0.306 0	3.021	0.398 9	0.316 3	3.021	0.409 0	0.326 4	3.020	0.418 9	0.339 0
2	3.028	0.365 5	0.313 4	3.027	0.373 2	0.320 9	3.026	0.379 0	0.327 7	3.026	0.384 7	0.336 8
1	3.033	0.341 2	0.320 7	3.033	0.344 9	0.324 9	3.033	0.347 2	0.328 3	3.032	0.349 5	0.333 2
1/10	1.119	0.512 5	0.194 3	1.113	0.565 9	0.213 4	1.104	0.614 9	0.231 4	1.096	0.668 0	0.251 2
8	1.146	0.488 7	0.216 1	1.141	0.534 5	0.234 6	1.137	0.576 8	0.252 5	1.135	0.620 3	0.273 8
6	1.156	0.458 8	0.239 1	1.155	0.495 0	0.256 9	1.154	0.528 9	0.274 3	1.156	0.562 6	0.295 6
4	1.160	0.423 2	0.263 4	1.159	0.448 3	0.278 6	1.158	0.471 8	0.293 7	1.157	0.498 4	0.310 7
3	1.163	0.404 7	0.275 8	1.162	0.424 3	0.289 3	1.161	0.441 6	0.302 5	1.161	0.460 3	0.317 2
2	1.165	0.382 2	0.289 6	1.165	0.396 0	0.300 5	1.164	0.407 0	0.310 6	1.164	0.417 5	0.322 1
1	1.168	0.352 9	0.306 2	1.168	0.360 3	0.312 7	1.168	0.365 4	0.318 5	1.168	0.369 1	0.325 3

Annex Attached Table 1. (continued)

2.5YR				5YR			7.5YR			10YR		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/ 8	—	—	—	—	—	—	76.14	0.424 7	0.402 5	76.34	0.421 1	0.415 5
6	76.12	0.396 5	0.365 6	76.21	0.397 9	0.376 0	76.35	0.397 2	0.386 0	76.51	0.395 3	0.397 4
4	76.45	0.366 8	0.353 1	76.47	0.369 2	0.361 7	76.51	0.370 1	0.369 3	76.58	0.369 5	0.377 7
3	76.51	0.350 4	0.346 2	76.53	0.353 5	0.353 3	76.56	0.355 4	0.359 7	76.61	0.355 7	0.366 8
2	76.58	0.334 8	0.339 4	76.59	0.338 0	0.344 5	76.61	0.340 5	0.349 7	76.65	0.341 5	0.355 0
1	76.63	0.321 7	0.333 5	76.64	0.324 0	0.336 3	76.66	0.326 1	0.339 4	76.68	0.327 1	0.342 5
8/20	—	—	—	—	—	—	56.32	0.540 0	0.451 3	56.54	0.524 8	0.470 5
18	—	—	—	—	—	—	56.44	0.532 3	0.448 3	57.12	0.515 4	0.469 3
16	—	—	—	—	—	—	56.67	0.519 7	0.444 1	57.25	0.505 2	0.464 7
14	—	—	—	56.42	0.511 3	0.417 6	57.06	0.501 8	0.437 7	57.28	0.491 9	0.457 3
12	56.38	0.489 9	0.390 2	56.69	0.487 0	0.409 2	57.20	0.481 2	0.428 5	57.32	0.474 0	0.446 8
10	56.74	0.458 5	0.382 1	57.20	0.458 6	0.400 6	57.26	0.457 1	0.416 7	57.36	0.452 2	0.433 5
8	57.24	0.429 6	0.374 5	57.27	0.432 6	0.390 0	57.32	0.431 6	0.403 2	57.41	0.428 4	0.418 2
6	57.33	0.398 5	0.364 3	57.35	0.400 9	0.375 8	57.39	0.401 7	0.386 4	57.46	0.400 6	0.399 1
4	57.42	0.369 4	0.353 7	57.43	0.371 5	0.361 7	57.47	0.372 1	0.369 3	57.52	0.371 9	0.378 2
3	57.47	0.352 5	0.346 7	57.48	0.355 6	0.353 5	57.50	0.357 1	0.359 8	57.55	0.357 6	0.367 1
2	57.52	0.336 2	0.339 7	57.53	0.340 0	0.344 9	57.54	0.342 0	0.349 8	57.57	0.343 0	0.355 3
1	57.57	0.322 4	0.333 6	57.57	0.325 4	0.336 7	57.58	0.327 2	0.339 5	57.60	0.328 1	0.342 7
7/20	41.09	0.583 4	0.404 3	41.27	0.565 5	0.429 9	—	—	—	—	—	—
18	41.17	0.570 5	0.403 0	41.49	0.554 8	0.428 7	41.50	0.539 8	0.450 8	40.96	0.528 8	0.468 8
16	41.32	0.552 9	0.400 9	41.51	0.542 5	0.425 4	41.60	0.529 8	0.447 5	41.70	0.515 8	0.467 8
14	41.50	0.530 0	0.397 6	41.55	0.524 6	0.420 3	41.62	0.515 9	0.441 5	41.72	0.504 9	0.461 6
12	41.56	0.501 1	0.391 2	41.59	0.500 8	0.412 8	41.65	0.496 2	0.432 8	41.74	0.488 2	0.452 6
10	41.63	0.468 7	0.383 4	41.65	0.471 9	0.403 4	41.70	0.470 4	0.421 1	41.77	0.465 8	0.439 4
8	41.69	0.439 2	0.375 8	41.71	0.441 7	0.391 8	41.75	0.442 3	0.407 1	41.81	0.440 0	0.423 8
6	41.76	0.407 8	0.366 2	41.77	0.411 1	0.379 1	41.80	0.412 3	0.390 9	41.85	0.411 1	0.404 9
4	41.83	0.374 2	0.354 5	41.84	0.377 5	0.363 5	41.86	0.379 4	0.371 7	41.90	0.379 5	0.382 4
3	41.87	0.357 9	0.348 1	41.87	0.361 0	0.355 1	41.89	0.362 9	0.361 8	41.92	0.363 3	0.370 1
2	41.90	0.342 0	0.341 6	41.91	0.344 8	0.346 7	41.92	0.346 2	0.351 4	41.95	0.346 6	0.357 2
1	41.94	0.326 9	0.335 3	41.94	0.328 7	0.337 9	41.96	0.329 5	0.340 6	41.97	0.329 8	0.343 6
6/18	28.87	0.587 2	0.403 1	28.73	0.572 5	0.426 0	—	—	—	—	—	—
16	28.90	0.569 3	0.401 1	28.94	0.558 2	0.425 8	28.81	0.546 1	0.448 3	—	—	—
14	28.93	0.548 8	0.397 7	28.96	0.541 3	0.421 5	29.02	0.530 1	0.443 9	29.09	0.517 1	0.465 1
12	28.96	0.522 2	0.392 9	28.99	0.519 6	0.415 7	29.04	0.513 2	0.436 8	29.10	0.502 8	0.457 3
10	29.01	0.490 4	0.386 2	29.03	0.492 5	0.407 4	29.07	0.489 9	0.427 0	29.13	0.482 9	0.446 6
8	29.06	0.455 2	0.378 0	29.07	0.460 4	0.396 7	29.10	0.460 1	0.412 9	29.15	0.456 6	0.431 4
6	29.11	0.420 4	0.368 7	29.12	0.424 8	0.383 4	29.15	0.425 5	0.395 9	29.19	0.424 7	0.411 3
4	29.17	0.383 3	0.356 9	29.18	0.386 4	0.366 5	29.19	0.388 1	0.375 2	29.23	0.387 7	0.386 8
3	29.20	0.365 6	0.350 5	29.21	0.368 2	0.357 8	29.22	0.369 7	0.364 7	29.24	0.369 7	0.373 8
2	29.23	0.348 1	0.343 7	29.23	0.350 1	0.348 8	29.24	0.351 2	0.353 6	29.26	0.351 4	0.359 9
1	29.26	0.330 6	0.336 5	29.26	0.331 7	0.339 3	29.27	0.332 3	0.341 9	29.28	0.332 5	0.345 1
5/16	18.99	0.593 4	0.399 1	—	—	—	—	—	—	—	—	—
14	18.99	0.572 7	0.397 2	19.02	0.562 9	0.421 8	18.91	0.550 6	0.444 9	—	—	—
12	19.02	0.548 4	0.393 9	19.04	0.541 5	0.416 9	19.08	0.531 8	0.440 5	19.13	0.518 3	0.462 8
10	19.05	0.518 4	0.388 8	19.06	0.516 1	0.410 4	19.09	0.509 9	0.431 5	19.14	0.500 6	0.452 8
8	19.08	0.481 1	0.381 8	19.10	0.483 8	0.401 6	19.12	0.482 0	0.419 5	19.16	0.476 0	0.439 2
6	19.13	0.438 7	0.371 9	19.13	0.443 6	0.388 3	19.15	0.445 0	0.402 7	19.18	0.443 0	0.420 1
4	19.17	0.395 2	0.359 1	19.18	0.399 1	0.370 9	19.19	0.401 0	0.380 8	19.21	0.400 9	0.393 5
3	19.19	0.374 1	0.352 2	19.20	0.377 3	0.361 1	19.21	0.378 8	0.368 6	19.22	0.379 0	0.378 6
2	19.21	0.353 5	0.345 0	19.22	0.355 7	0.350 8	19.23	0.356 5	0.355 8	19.24	0.356 8	0.362 8
1	19.24	0.333 1	0.337 3	19.24	0.334 3	0.340 1	19.25	0.334 5	0.342 6	19.26	0.334 7	0.346 3
4/12	11.52	0.580 6	0.392 6	11.51	0.572 9	0.417 2	—	—	—	—	—	—
10	11.54	0.548 0	0.388 7	11.56	0.542 7	0.412 4	11.58	0.534 0	0.436 8	11.61	0.522 3	0.460 0
8	11.57	0.508 5	0.382 5	11.58	0.507 5	0.403 9	11.59	0.503 3	0.424 7	11.62	0.495 0	0.445 7
6	11.59	0.463 3	0.374 2	11.60	0.466 5	0.392 3	11.61	0.466 1	0.409 2	11.63	0.461 5	0.427 6
4	11.62	0.416 7	0.362 6	11.63	0.420 9	0.376 4	11.64	0.422 4	0.389 3	11.65	0.419 9	0.403 3
3	11.64	0.391 4	0.355 5	11.64	0.394 9	0.366 3	11.65	0.396 3	0.376 0	11.66	0.394 9	0.387 6
2	11.66	0.365 3	0.347 5	11.66	0.367 8	0.354 9	11.67	0.368 6	0.361 2	11.68	0.368 1	0.369 9
1	11.67	0.339 0	0.338 7	11.68	0.340 2	0.342 5	11.68	0.340 5	0.345 4	11.69	0.340 4	0.350 4

Annex Attached Table 1. (continued)

	2.5YR			5YR			7.5YR			10YR		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
3/10	6.283	0.594 7	0.382 5	—	—	—	—	—	—	—	—	—
8	6.299	0.548 5	0.380 1	6.307	0.545 4	0.406 6	6.321	0.537 6	0.433 0	6.321	0.528 8	0.457 6
6	6.317	0.497 3	0.374 4	6.323	0.497 6	0.395 7	6.333	0.493 0	0.416 4	6.348	0.486 2	0.437 5
4	6.338	0.438 6	0.364 0	6.342	0.439 7	0.379 0	6.349	0.439 2	0.394 0	6.361	0.434 8	0.409 5
3	6.348	0.409 1	0.357 2	6.352	0.410 3	0.369 1	6.358	0.410 2	0.380 4	6.368	0.406 5	0.392 5
2	6.359	0.378 7	0.349 2	6.362	0.379 8	0.357 7	6.367	0.379 5	0.365 1	6.376	0.376 7	0.373 5
1	6.371	0.346 8	0.339 8	6.374	0.347 6	0.344 5	6.378	0.347 1	0.348 0	6.384	0.345 5	0.352 3
2/ 8	2.987	0.600 7	0.360 0	—	—	—	—	—	—	—	—	—
6	3.001	0.530 3	0.361 7	3.004	0.543 2	0.395 0	3.005	0.546 7	0.428 8	—	—	—
4	3.014	0.462 8	0.357 1	3.017	0.469 4	0.379 7	3.022	0.469 9	0.402 2	3.029	0.467 5	0.422 6
3	3.021	0.426 1	0.352 3	3.023	0.430 4	0.369 1	3.028	0.430 8	0.386 2	3.034	0.428 0	0.401 3
2	3.027	0.388 5	0.345 8	3.030	0.390 9	0.356 9	3.034	0.391 3	0.368 5	3.039	0.389 1	0.378 6
1	3.034	0.350 6	0.337 9	3.037	0.351 5	0.343 3	3.040	0.352 0	0.349 3	3.044	0.350 7	0.354 5
1/ 8	1.145	0.671 8	0.307 1	—	—	—	—	—	—	—	—	—
6	1.151	0.606 1	0.328 9	—	—	—	—	—	—	—	—	—
4	1.157	0.534 4	0.339 8	1.157	0.566 4	0.381 4	—	—	—	—	—	—
3	1.161	0.485 0	0.341 8	1.163	0.504 0	0.374 7	—	—	—	—	—	—
2	1.165	0.429 8	0.340 8	1.167	0.440 7	0.364 2	1.170	0.444 9	0.383 8	1.174	0.445 3	0.404 8
1	1.170	0.371 8	0.336 1	1.172	0.373 0	0.347 1	1.175	0.369 5	0.353 7	1.178	0.365 0	0.359 4

Annex Attached Table 1. (continued)

	2.5Y			5Y			7.5Y			10Y		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/20	—	—	—	76.45	0.480 0	0.511 9	—	—	—	—	—	—
18	—	—	—	76.49	0.475 1	0.508 1	76.68	0.463 1	0.522 0	76.85	0.450 5	0.535 3
16	—	—	—	76.55	0.467 8	0.501 6	76.69	0.456 1	0.514 3	76.84	0.444 1	0.526 5
14	—	—	—	76.61	0.456 9	0.491 8	76.71	0.446 7	0.504 2	76.82	0.435 6	0.515 1
12	76.31	0.456 1	0.458 7	76.62	0.443 0	0.477 9	76.72	0.434 0	0.489 0	76.81	0.424 0	0.498 2
10	76.50	0.436 2	0.444 1	76.64	0.426 0	0.460 2	76.72	0.418 3	0.469 6	76.80	0.410 0	0.477 0
8	76.54	0.415 4	0.427 1	76.65	0.407 5	0.440 5	76.73	0.401 1	0.448 0	76.79	0.394 7	0.454 0
6	76.59	0.391 8	0.407 0	76.67	0.386 3	0.417 1	76.73	0.381 4	0.422 4	76.78	0.376 3	0.425 8
4	76.63	0.367 1	0.384 8	76.69	0.363 4	0.391 1	76.73	0.360 3	0.394 5	76.76	0.356 9	0.396 6
3	76.65	0.354 4	0.372 6	76.70	0.351 9	0.377 3	76.73	0.349 7	0.380 2	76.75	0.347 2	0.381 8
2	76.67	0.341 2	0.359 3	76.70	0.339 9	0.362 5	76.73	0.338 5	0.364 9	76.74	0.336 8	0.366 0
1	76.70	0.327 3	0.344 9	76.71	0.327 0	0.346 7	76.72	0.326 3	0.347 6	76.73	0.325 5	0.348 6
8/20	56.48	0.510 5	0.488 5	—	—	—	—	—	—	—	—	—
18	56.77	0.502 7	0.486 1	56.68	0.484 5	0.507 2	56.71	0.470 3	0.522 6	56.80	0.455 8	0.537 7
16	57.20	0.493 2	0.482 8	56.95	0.477 7	0.502 8	56.93	0.464 4	0.517 5	56.99	0.450 7	0.531 5
14	57.39	0.481 3	0.475 4	57.39	0.466 8	0.495 8	57.29	0.454 8	0.509 6	57.30	0.442 3	0.521 6
12	57.42	0.465 7	0.464 2	57.54	0.453 3	0.484 1	57.62	0.442 1	0.497 1	57.70	0.430 5	0.507 5
10	57.45	0.445 8	0.449 0	57.55	0.435 7	0.466 8	57.63	0.426 0	0.478 0	57.69	0.416 5	0.486 1
8	57.48	0.422 9	0.431 2	57.57	0.415 0	0.446 0	57.63	0.407 7	0.454 9	57.69	0.399 5	0.460 6
6	57.52	0.397 6	0.410 4	57.59	0.391 6	0.421 4	57.64	0.386 3	0.427 3	57.68	0.380 2	0.431 6
4	57.56	0.370 0	0.386 0	57.61	0.366 3	0.393 6	57.64	0.363 3	0.397 2	57.67	0.359 1	0.399 6
3	57.58	0.356 5	0.373 6	57.61	0.354 1	0.379 2	57.64	0.351 9	0.382 1	57.66	0.348 7	0.383 9
2	57.60	0.342 8	0.360 4	57.62	0.341 4	0.363 9	57.64	0.339 9	0.366 2	57.65	0.337 8	0.367 5
1	57.61	0.328 3	0.345 8	57.62	0.327 9	0.347 3	57.64	0.326 9	0.348 8	57.64	0.326 0	0.349 5
7/16	41.20	0.504 4	0.484 8	41.03	0.487 6	0.504 6	40.99	0.472 9	0.521 4	41.03	0.458 0	0.537 6
14	41.80	0.491 7	0.480 8	41.48	0.477 3	0.498 6	41.35	0.463 8	0.514 4	41.33	0.450 2	0.529 3
12	41.82	0.478 0	0.471 1	41.91	0.464 3	0.490 2	41.85	0.451 5	0.504 7	41.77	0.439 1	0.517 0
10	41.85	0.458 9	0.457 4	41.92	0.448 5	0.475 4	41.99	0.437 1	0.488 9	42.05	0.425 7	0.499 8
8	41.87	0.434 7	0.438 6	41.94	0.425 9	0.453 7	41.99	0.416 8	0.464 4	42.04	0.407 2	0.472 0
6	41.90	0.407 8	0.416 3	41.96	0.400 9	0.428 9	42.00	0.394 1	0.435 7	42.04	0.386 0	0.440 1
4	41.93	0.377 5	0.390 5	41.97	0.372 9	0.399 2	42.00	0.368 6	0.403 4	42.03	0.363 2	0.406 2
3	41.95	0.361 8	0.377 0	41.98	0.358 6	0.383 1	42.00	0.355 3	0.386 0	42.02	0.351 2	0.388 0
2	41.97	0.345 7	0.362 6	41.99	0.343 9	0.366 0	42.00	0.341 5	0.367 9	42.02	0.338 8	0.369 1
1	41.99	0.329 4	0.346 7	41.99	0.328 7	0.348 1	42.00	0.327 3	0.348 9	42.01	0.326 0	0.349 5
6/14	28.76	0.505 4	0.483 5	28.56	0.491 0	0.503 3	28.45	0.476 3	0.521 1	28.23	0.459 8	0.538 7
12	29.17	0.489 7	0.476 8	29.07	0.475 4	0.495 0	28.93	0.461 9	0.510 9	28.91	0.447 1	0.525 8
10	29.18	0.473 7	0.465 6	29.24	0.460 9	0.483 9	29.30	0.447 6	0.499 3	29.31	0.433 5	0.511 8
8	29.20	0.450 5	0.448 5	29.25	0.440 7	0.465 3	29.30	0.429 8	0.478 5	29.34	0.417 5	0.488 1
6	29.23	0.420 4	0.425 9	29.27	0.413 5	0.438 9	29.30	0.405 2	0.448 6	29.33	0.395 0	0.454 1
4	29.25	0.385 2	0.396 8	29.28	0.380 3	0.405 8	29.31	0.375 2	0.410 9	29.33	0.368 5	0.414 1
3	29.27	0.367 8	0.381 8	29.29	0.364 0	0.388 3	29.31	0.360 2	0.391 8	29.32	0.355 2	0.393 9
2	29.28	0.350 1	0.365 7	29.30	0.347 6	0.369 8	29.31	0.344 9	0.372 0	29.32	0.341 6	0.373 2
1	29.29	0.331 8	0.348 3	29.30	0.330 6	0.350 2	29.31	0.329 2	0.351 3	29.31	0.327 5	0.351 8
5/12	18.94	0.507 4	0.481 8	18.83	0.493 8	0.501 3	18.68	0.477 6	0.519 9	18.58	0.459 4	0.538 6
10	19.18	0.487 7	0.472 3	19.22	0.474 1	0.491 6	19.12	0.460 7	0.508 5	19.14	0.444 3	0.523 9
8	19.19	0.466 7	0.457 8	19.23	0.455 4	0.474 7	19.27	0.442 0	0.490 6	19.30	0.427 3	0.502 5
6	19.21	0.437 5	0.436 5	19.24	0.429 1	0.450 8	19.27	0.418 4	0.462 7	19.29	0.405 5	0.470 1
4	19.23	0.397 7	0.404 9	19.25	0.392 0	0.415 4	19.27	0.385 3	0.421 9	19.29	0.376 4	0.426 1
3	19.24	0.376 7	0.387 1	19.26	0.372 0	0.395 0	19.27	0.367 2	0.399 2	19.29	0.360 3	0.401 6
2	19.25	0.355 4	0.368 5	19.27	0.351 8	0.373 6	19.27	0.348 8	0.375 8	19.28	0.343 9	0.376 8
1	19.26	0.334 0	0.349 1	19.27	0.331 9	0.351 6	19.27	0.330 5	0.352 2	19.28	0.327 8	0.352 3
4/10	11.53	0.511 3	0.480 5	—	—	—	—	—	—	—	—	—
8	11.65	0.484 0	0.466 8	11.67	0.471 2	0.485 3	11.70	0.455 6	0.503 3	11.70	0.439 3	0.519 6
6	11.66	0.453 1	0.445 4	11.68	0.443 4	0.461 4	11.70	0.430 9	0.475 4	11.72	0.416 5	0.486 4
4	11.67	0.414 3	0.416 2	11.69	0.406 9	0.427 6	11.70	0.397 9	0.436 3	11.71	0.386 6	0.441 6
3	11.68	0.390 6	0.397 5	11.69	0.384 5	0.405 7	11.70	0.377 5	0.411 3	11.71	0.368 3	0.413 9
2	11.69	0.365 2	0.376 4	11.69	0.360 7	0.381 3	11.70	0.355 7	0.384 2	11.71	0.349 1	0.385 0
1	11.69	0.338 9	0.353 6	11.70	0.336 3	0.355 6	11.70	0.333 8	0.356 4	11.71	0.330 2	0.356 2



Annex Attached Table 1. (continued)

2.5Y				5Y			7.5Y			10Y		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
3/ 6	6.362	0.476 4	0.457 9	6.375	0.464 3	0.475 9	6.388	0.449 2	0.493 8	6.401	0.430 8	0.507 9
4	6.372	0.427 8	0.424 4	6.381	0.418 7	0.436 3	6.390	0.407 8	0.446 2	6.399	0.395 1	0.453 9
3	6.377	0.400 6	0.403 7	6.384	0.393 0	0.412 1	6.391	0.384 5	0.418 4	6.398	0.374 2	0.422 7
2	6.382	0.372 1	0.380 7	6.388	0.366 1	0.385 7	6.392	0.360 3	0.389 0	6.397	0.352 6	0.390 4
1	6.388	0.342 6	0.355 8	6.391	0.339 1	0.357 8	6.393	0.336 2	0.358 9	6.396	0.331 7	0.358 8
2/ 4	3.036	0.461 5	0.444 8	3.041	0.452 3	0.462 9	3.047	0.437 6	0.478 1	3.053	0.416 3	0.485 4
3	3.039	0.422 0	0.417 0	3.044	0.413 3	0.428 1	3.048	0.400 5	0.435 6	3.052	0.384 7	0.438 1
2	3.043	0.384 0	0.388 5	3.046	0.377 0	0.394 2	3.049	0.367 2	0.396 5	3.052	0.356 8	0.396 0
1	3.046	0.347 6	0.359 2	3.048	0.343 5	0.361 2	3.050	0.337 9	0.360 9	3.051	0.332 7	0.359 6
1/ 2	1.177	0.436 1	0.424 4	1.179	0.422 6	0.433 6	1.181	0.403 8	0.436 6	1.182	0.380 2	0.430 3
1	1.179	0.357 6	0.363 8	1.180	0.350 1	0.364 4	1.181	0.342 8	0.363 8	1.182	0.335 4	0.362 0

Annex Attached Table 1. (continued)

	2.5GY			5GY			7.5GY			10GY		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/18	77.04	0.431 1	0.554 4	77.25	0.405 9	0.574 0	77.35	0.354 6	0.597 5	77.19	0.299 2	0.582 8
16	77.02	0.424 7	0.542 8	77.17	0.401 2	0.559 1	77.25	0.353 8	0.572 0	77.23	0.304 6	0.553 2
14	76.99	0.417 2	0.529 1	77.14	0.395 2	0.539 0	77.21	0.351 7	0.541 9	77.23	0.309 0	0.523 1
12	76.95	0.407 4	0.509 4	77.10	0.387 7	0.515 5	77.22	0.349 2	0.513 5	77.23	0.312 2	0.494 0
10	76.92	0.395 1	0.484 2	77.04	0.378 8	0.487 9	77.22	0.345 3	0.483 9	77.22	0.314 4	0.467 6
8	76.89	0.382 3	0.458 5	76.99	0.368 7	0.459 7	77.15	0.340 6	0.452 9	77.25	0.315 3	0.438 6
6	76.85	0.367 1	0.428 5	76.92	0.357 2	0.429 0	77.05	0.335 3	0.423 3	77.15	0.315 6	0.413 9
4	76.81	0.351 0	0.398 3	76.85	0.344 7	0.398 1	76.93	0.328 5	0.392 0	76.98	0.315 6	0.384 3
3	76.78	0.342 8	0.382 8	76.81	0.337 9	0.382 4	76.87	0.325 2	0.377 6	76.91	0.315 1	0.371 4
2	76.75	0.334 0	0.366 3	76.77	0.330 3	0.365 9	76.81	0.321 7	0.362 9	76.83	0.314 3	0.358 5
1	76.73	0.324 1	0.348 6	76.73	0.322 0	0.348 3	76.74	0.317 7	0.347 0	76.74	0.313 5	0.344 7
8/24	—	—	—	—	—	—	—	—	—	58.65	0.271 3	0.689 2
22	—	—	—	—	—	—	—	—	—	58.51	0.278 7	0.662 4
20	—	—	—	56.96	0.409 7	0.588 0	57.78	0.354 0	0.628 1	58.39	0.286 7	0.632 5
18	57.03	0.435 0	0.557 6	57.32	0.407 1	0.581 5	57.90	0.353 5	0.611 2	58.33	0.294 4	0.599 8
16	57.18	0.430 1	0.550 2	57.48	0.402 6	0.568 0	57.97	0.352 3	0.585 7	58.32	0.300 6	0.566 7
14	57.43	0.423 0	0.538 3	57.65	0.397 4	0.551 8	58.07	0.350 6	0.556 2	58.36	0.305 9	0.534 6
12	57.82	0.411 5	0.519 3	57.95	0.388 5	0.526 7	58.13	0.347 8	0.523 1	58.27	0.310 1	0.503 7
10	57.80	0.399 4	0.494 5	57.90	0.379 0	0.496 4	58.05	0.344 3	0.489 4	58.17	0.312 6	0.472 2
8	57.77	0.384 5	0.464 2	57.85	0.368 4	0.464 2	57.97	0.339 9	0.456 6	58.06	0.314 4	0.441 1
6	57.74	0.368 9	0.433 5	57.80	0.357 2	0.432 5	57.89	0.334 0	0.425 1	57.96	0.315 3	0.414 5
4	57.71	0.351 4	0.400 4	57.74	0.344 3	0.399 2	57.81	0.327 6	0.393 6	57.85	0.315 1	0.385 9
3	57.69	0.343 2	0.384 5	57.71	0.337 6	0.383 2	57.76	0.324 6	0.378 5	57.79	0.314 6	0.372 6
2	57.67	0.334 6	0.367 9	57.68	0.330 3	0.366 8	57.71	0.321 3	0.363 1	57.73	0.314 0	0.359 0
1	57.64	0.324 7	0.349 8	57.64	0.322 1	0.348 9	57.65	0.317 5	0.346 8	57.65	0.313 4	0.344 7
7/22	—	—	—	—	—	—	—	—	—	42.83	0.267 6	0.694 2
20	—	—	—	—	—	—	—	—	—	42.74	0.276 5	0.662 3
18	—	—	—	—	—	—	41.97	0.351 3	0.628 2	42.68	0.285 8	0.625 9
16	41.13	0.435 8	0.558 5	41.60	0.404 8	0.580 9	42.23	0.350 3	0.605 2	42.63	0.294 0	0.591 9
14	41.47	0.428 9	0.548 2	41.75	0.399 7	0.565 2	42.27	0.349 1	0.576 4	42.58	0.301 2	0.555 3
12	41.88	0.418 0	0.531 5	42.05	0.391 2	0.542 3	42.37	0.346 5	0.540 8	42.50	0.306 5	0.520 1
10	42.13	0.405 7	0.509 7	42.22	0.382 0	0.512 8	42.34	0.343 5	0.504 7	42.42	0.310 5	0.485 0
8	42.11	0.390 1	0.477 0	42.18	0.370 5	0.476 4	42.27	0.339 3	0.466 9	42.34	0.313 2	0.451 3
6	42.09	0.372 4	0.441 9	42.14	0.357 8	0.440 0	42.21	0.334 0	0.431 2	42.26	0.314 4	0.418 9
4	42.06	0.354 2	0.406 8	42.09	0.344 5	0.404 8	42.14	0.327 6	0.397 5	42.17	0.314 3	0.389 6
3	42.05	0.344 6	0.388 4	42.07	0.337 6	0.386 9	42.10	0.324 3	0.381 1	42.12	0.314 0	0.374 9
2	42.03	0.334 6	0.369 3	42.04	0.330 2	0.368 5	42.06	0.320 8	0.364 5	42.07	0.313 6	0.360 0
1	42.01	0.324 1	0.349 6	42.01	0.322 1	0.349 2	42.02	0.317 1	0.347 3	42.02	0.313 2	0.344 8
6/20	—	—	—	—	—	—	—	—	—	29.98	0.260 4	0.704 8
18	—	—	—	—	—	—	—	—	—	29.95	0.271 1	0.668 0
16	—	—	—	—	—	—	29.35	0.345 6	0.632 3	29.90	0.282 2	0.627 8
14	28.58	0.435 1	0.559 7	29.12	0.401 4	0.581 6	29.63	0.345 0	0.604 4	29.86	0.291 8	0.589 2
12	29.03	0.424 6	0.544 2	29.26	0.394 7	0.560 8	29.60	0.344 6	0.566 9	29.72	0.300 3	0.545 7
10	29.37	0.412 1	0.524 6	29.47	0.385 1	0.533 0	29.58	0.342 9	0.528 3	29.64	0.306 3	0.506 1
8	29.40	0.397 9	0.496 1	29.46	0.374 7	0.496 6	29.53	0.339 8	0.487 3	29.58	0.310 3	0.468 6
6	29.38	0.378 9	0.456 6	29.42	0.361 3	0.454 3	29.47	0.334 6	0.444 0	29.51	0.312 6	0.430 5
4	29.36	0.357 7	0.415 1	29.38	0.346 7	0.412 6	29.42	0.328 2	0.404 8	29.44	0.313 2	0.395 5
3	29.34	0.347 0	0.394 2	29.36	0.338 8	0.392 2	29.39	0.324 7	0.386 3	29.41	0.313 1	0.379 1
2	29.33	0.335 9	0.373 0	29.34	0.330 5	0.371 8	29.36	0.321 0	0.367 9	29.37	0.313 0	0.362 8
1	29.32	0.324 5	0.351 5	29.32	0.321 8	0.350 9	29.32	0.317 1	0.349 0	29.33	0.312 9	0.346 2
5/18	—	—	—	—	—	—	—	—	—	19.80	0.251 4	0.721 4
16	—	—	—	—	—	—	—	—	—	19.77	0.264 7	0.676 7
14	—	—	—	—	—	—	19.34	0.338 5	0.637 9	19.74	0.278 2	0.629 4
12	18.84	0.432 7	0.560 8	19.24	0.397 9	0.583 5	19.60	0.339 6	0.601 7	19.66	0.289 4	0.584 6
10	19.25	0.419 1	0.541 0	19.36	0.388 9	0.554 0	19.52	0.340 8	0.557 0	19.53	0.299 7	0.533 9
8	19.34	0.405 3	0.513 3	19.39	0.378 1	0.517 0	19.44	0.338 6	0.507 4	19.48	0.306 2	0.487 8
6	19.33	0.386 2	0.473 4	19.36	0.364 8	0.471 3	19.40	0.334 4	0.459 8	19.43	0.310 3	0.443 0
4	19.31	0.362 3	0.425 3	19.33	0.348 5	0.421 3	19.36	0.327 9	0.412 0	19.38	0.311 8	0.401 4
3	19.30	0.349 6	0.400 5	19.32	0.339 6	0.397 2	19.34	0.324 2	0.390 0	19.35	0.312 3	0.382 3
2	19.29	0.336 9	0.375 9	19.30	0.330 6	0.373 8	19.31	0.320 5	0.369 0	19.32	0.312 7	0.364 0
1	19.28	0.324 4	0.352 0	19.28	0.321 5	0.351 1	19.29	0.316 6	0.348 7	19.29	0.312 9	0.346 3

Annex Attached Table 1. (continued)

	2.5GY			5GY			7.5GY			10GY		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
4/16	—	—	—	—	—	—	—	—	—	12.10	0.240 2	0.738 0
14	—	—	—	—	—	—	—	—	—	12.06	0.253 4	0.692 4
12	—	—	—	—	—	—	11.70	0.331 1	0.650 4	12.01	0.270 0	0.637 0
10	—	—	—	11.64	0.395 3	0.588 0	11.92	0.333 8	0.598 7	11.93	0.286 3	0.577 0
8	11.76	0.413 1	0.535 3	11.80	0.382 3	0.544 9	11.83	0.336 2	0.543 0	11.86	0.298 1	0.520 4
6	11.74	0.394 2	0.493 5	11.77	0.369 4	0.494 1	11.80	0.333 7	0.484 8	11.82	0.305 6	0.467 5
4	11.73	0.370 3	0.443 2	11.75	0.353 4	0.439 5	11.77	0.328 1	0.428 1	11.78	0.310 2	0.415 1
3	11.73	0.355 2	0.413 2	11.74	0.343 3	0.409 8	11.75	0.324 2	0.400 0	11.76	0.311 6	0.390 9
2	11.72	0.339 7	0.382 8	11.72	0.332 7	0.380 3	11.73	0.320 1	0.373 4	11.74	0.312 5	0.368 3
1	11.71	0.325 1	0.354 1	11.71	0.322 3	0.352 9	11.71	0.316 1	0.349 4	11.72	0.312 9	0.347 6
3/14	—	—	—	—	—	—	—	—	—	6.677	0.225 8	0.745 0
12	—	—	—	—	—	—	—	—	—	6.585	0.247 3	0.677 6
10	—	—	—	—	—	—	6.463	0.321 4	0.650 1	6.539	0.267 2	0.611 9
8	—	—	—	6.419	0.388 0	0.587 6	6.492	0.329 0	0.577 8	6.491	0.285 5	0.546 2
6	6.418	0.403 2	0.517 3	6.436	0.371 6	0.518 7	6.455	0.330 7	0.506 8	6.469	0.297 5	0.484 1
4	6.412	0.376 1	0.458 0	6.423	0.354 5	0.453 7	6.436	0.326 5	0.441 1	6.445	0.305 2	0.425 7
3	6.408	0.359 5	0.423 5	6.416	0.344 1	0.419 0	6.425	0.323 1	0.408 2	6.431	0.308 1	0.397 5
2	6.403	0.342 5	0.388 8	6.408	0.333 2	0.385 4	6.413	0.319 4	0.377 5	6.417	0.310 3	0.371 2
1	6.398	0.326 4	0.356 5	6.400	0.322 5	0.354 8	6.402	0.315 8	0.350 5	6.403	0.311 8	0.348 1
2/12	—	—	—	—	—	—	—	—	—	3.266	0.190 0	0.780 5
10	—	—	—	—	—	—	—	—	—	3.162	0.225 6	0.689 1
8	—	—	—	—	—	—	3.095	0.310 6	0.656 4	3.115	0.258 4	0.593 4
6	—	—	—	3.084	0.378 5	0.580 1	3.088	0.322 2	0.546 4	3.095	0.282 8	0.509 3
4	3.061	0.386 0	0.483 4	3.068	0.356 5	0.475 0	3.075	0.323 7	0.457 7	3.081	0.298 0	0.437 6
3	3.058	0.363 2	0.434 5	3.063	0.344 2	0.428 0	3.069	0.321 2	0.415 5	3.073	0.303 8	0.402 8
2	3.055	0.343 3	0.392 2	3.058	0.332 1	0.386 8	3.062	0.317 8	0.378 2	3.064	0.308 2	0.371 6
1	3.053	0.326 5	0.356 9	3.054	0.321 3	0.353 2	3.055	0.314 6	0.348 5	3.057	0.311 2	0.346 3
1/ 6	—	—	—	—	—	—	—	—	—	1.223	0.218 6	0.649 6
4	—	—	—	1.188	0.371 5	0.599 6	1.202	0.308 8	0.548 9	1.201	0.269 7	0.503 7
3	—	—	—	1.195	0.352 0	0.492 0	1.195	0.313 9	0.462 7	1.197	0.288 1	0.439 5
2	1.186	0.354 2	0.419 9	1.188	0.336 3	0.410 3	1.190	0.316 0	0.397 3	1.192	0.301 2	0.386 3
1	1.183	0.329 1	0.359 3	1.185	0.323 2	0.356 6	1.186	0.315 6	0.352 7	1.188	0.310 0	0.350 7

Annex Attached Table 1. (continued)

	2.5G			5G			7.5G			10G		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/16	77.11	0.261 1	0.507 1	—	—	—	—	—	—	—	—	—
14	77.15	0.269 5	0.483 9	—	—	—	—	—	—	—	—	—
12	77.19	0.277 5	0.461 5	77.13	0.252 3	0.429 8	77.10	0.241 7	0.413 0	77.08	0.232 5	0.394 6
10	77.22	0.284 6	0.440 7	77.18	0.263 9	0.414 5	77.15	0.254 7	0.400 4	77.13	0.246 0	0.385 5
8	77.24	0.291 3	0.419 1	77.22	0.273 9	0.399 9	77.19	0.265 8	0.388 6	77.17	0.258 1	0.376 9
6	77.20	0.297 2	0.398 5	77.23	0.284 1	0.384 2	77.24	0.277 3	0.375 4	77.21	0.271 4	0.366 2
4	77.02	0.303 1	0.374 3	77.04	0.294 7	0.365 9	77.05	0.289 7	0.360 2	77.05	0.285 6	0.354 4
3	76.94	0.305 5	0.363 8	76.95	0.299 3	0.357 6	76.96	0.295 3	0.353 1	76.96	0.292 1	0.348 8
2	76.85	0.307 8	0.353 3	76.86	0.303 7	0.349 1	76.86	0.300 8	0.345 8	76.86	0.298 6	0.342 8
1	76.75	0.310 1	0.342 0	76.76	0.308 2	0.339 8	76.76	0.306 5	0.337 9	76.75	0.305 4	0.336 4
8/24	58.68	0.206 6	0.613 7	—	—	—	—	—	—	—	—	—
22	58.67	0.219 4	0.591 0	58.65	0.181 2	0.507 8	—	—	—	—	—	—
20	58.64	0.231 2	0.567 9	58.64	0.194 5	0.495 2	58.64	0.183 8	0.464 5	58.64	0.173 0	0.431 8
18	58.61	0.242 7	0.543 2	58.61	0.209 1	0.480 7	58.61	0.197 2	0.453 8	58.61	0.186 1	0.426 0
16	58.55	0.254 2	0.517 4	58.57	0.223 0	0.465 9	58.57	0.211 3	0.442 1	58.57	0.200 7	0.416 9
14	58.45	0.264 5	0.491 5	58.49	0.236 0	0.450 6	58.50	0.224 9	0.429 1	58.50	0.214 5	0.407 6
12	58.35	0.273 1	0.469 2	58.39	0.248 4	0.434 7	58.39	0.237 8	0.416 4	58.39	0.228 2	0.397 8
10	58.24	0.282 3	0.444 1	58.27	0.261 2	0.417 9	58.27	0.251 6	0.402 5	58.27	0.243 3	0.387 1
8	58.12	0.289 6	0.420 6	58.15	0.272 6	0.401 4	58.15	0.264 4	0.388 6	58.15	0.257 1	0.376 6
6	58.01	0.295 8	0.399 1	58.03	0.283 0	0.384 7	58.03	0.276 4	0.375 5	58.03	0.270 4	0.366 1
4	57.87	0.302 2	0.375 1	57.89	0.293 8	0.366 3	57.89	0.288 9	0.360 5	57.89	0.284 4	0.354 6
3	57.81	0.304 8	0.364 4	57.82	0.298 4	0.357 9	57.82	0.294 6	0.353 4	57.82	0.291 0	0.348 8
2	57.74	0.307 3	0.353 7	57.75	0.302 9	0.349 4	57.75	0.300 1	0.346 1	57.75	0.297 8	0.342 9
1	57.66	0.309 8	0.342 2	57.67	0.307 6	0.339 9	57.67	0.306 2	0.338 2	57.66	0.305 0	0.336 4
7/26	43.64	0.167 6	0.665 1	43.55	0.140 1	0.548 0	43.55	0.131 1	0.503 8	—	—	—
24	43.49	0.185 5	0.638 1	43.51	0.152 0	0.536 7	43.50	0.141 8	0.495 7	43.52	0.131 6	0.456 1
22	43.32	0.200 6	0.614 0	43.42	0.165 3	0.524 3	43.45	0.153 7	0.486 6	43.46	0.143 6	0.449 7
20	43.12	0.215 7	0.587 2	43.30	0.179 6	0.510 5	43.33	0.168 3	0.475 6	43.36	0.158 6	0.442 0
18	42.92	0.230 4	0.559 7	43.12	0.195 6	0.494 3	43.17	0.183 4	0.463 5	43.22	0.172 9	0.433 4
16	42.76	0.242 6	0.533 3	42.93	0.210 0	0.478 4	42.99	0.197 5	0.451 3	43.03	0.187 6	0.424 2
14	42.65	0.254 9	0.506 4	42.72	0.225 2	0.461 2	42.76	0.213 3	0.437 3	42.81	0.202 9	0.413 8
12	42.57	0.265 8	0.480 5	42.59	0.240 9	0.442 5	42.60	0.229 1	0.422 4	42.60	0.219 3	0.402 5
10	42.48	0.276 7	0.453 6	42.50	0.255 1	0.424 2	42.51	0.244 5	0.407 4	42.51	0.235 4	0.391 3
8	42.39	0.285 9	0.427 0	42.40	0.268 9	0.405 2	42.41	0.259 9	0.391 9	42.41	0.251 9	0.379 3
6	42.29	0.293 8	0.401 3	42.30	0.280 8	0.386 7	42.31	0.273 7	0.377 1	42.31	0.267 2	0.367 7
4	42.19	0.300 4	0.378 2	42.20	0.291 5	0.368 9	42.21	0.286 4	0.362 5	42.21	0.281 8	0.355 9
3	42.14	0.303 5	0.366 6	42.15	0.296 8	0.359 7	42.15	0.292 8	0.354 8	42.15	0.289 1	0.349 7
2	42.09	0.306 6	0.354 7	42.09	0.302 1	0.350 1	42.09	0.299 2	0.346 9	42.09	0.296 5	0.343 3
1	42.02	0.309 7	0.342 2	42.03	0.307 4	0.339 9	42.03	0.305 9	0.338 3	42.03	0.304 4	0.336 5
6/28	31.09	0.115 0	0.720 2	30.81	0.092 2	0.588 2	30.74	0.087 1	0.533 5	—	—	—
26	31.00	0.133 5	0.697 4	30.80	0.108 4	0.574 8	30.73	0.101 7	0.522 3	30.69	0.094 8	0.473 4
24	30.87	0.152 2	0.672 5	30.76	0.125 0	0.559 8	30.72	0.116 0	0.511 4	30.67	0.107 3	0.466 8
22	30.68	0.172 0	0.645 0	30.68	0.142 4	0.544 4	30.66	0.132 0	0.500 0	30.64	0.122 7	0.459 0
20	30.47	0.190 0	0.617 3	30.55	0.159 7	0.528 1	30.57	0.147 7	0.488 2	30.57	0.137 6	0.451 5
18	30.25	0.207 8	0.587 7	30.39	0.177 2	0.511 1	30.42	0.164 4	0.475 3	30.45	0.154 3	0.442 2
16	30.03	0.225 4	0.556 8	30.19	0.194 7	0.493 1	30.24	0.182 2	0.461 0	30.28	0.171 4	0.432 0
14	29.85	0.240 5	0.526 8	29.98	0.211 8	0.474 2	30.03	0.199 2	0.446 3	30.07	0.188 8	0.421 1
12	29.75	0.255 7	0.495 1	29.77	0.228 4	0.455 1	29.81	0.216 5	0.431 0	29.86	0.205 6	0.409 5
10	29.69	0.267 9	0.467 1	29.70	0.246 1	0.433 8	29.70	0.234 8	0.414 3	29.71	0.224 7	0.396 5
8	29.61	0.279 4	0.438 2	29.63	0.261 2	0.414 3	29.63	0.251 2	0.398 7	29.63	0.242 4	0.384 1
6	29.54	0.289 4	0.410 5	29.55	0.275 3	0.394 3	29.56	0.266 9	0.382 4	29.55	0.259 9	0.371 2
4	29.46	0.297 7	0.383 4	29.47	0.287 9	0.373 8	29.48	0.281 9	0.366 7	29.48	0.276 2	0.358 9
3	29.42	0.301 8	0.370 3	29.43	0.294 3	0.363 0	29.43	0.289 9	0.357 6	29.43	0.285 4	0.351 7
2	29.38	0.305 7	0.357 1	29.38	0.300 7	0.351 8	29.38	0.297 7	0.348 1	29.38	0.294 9	0.344 0
1	29.33	0.309 5	0.343 5	29.33	0.306 9	0.340 5	29.33	0.305 4	0.338 4	29.33	0.304 2	0.336 3

Annex Attached Table 1. (continued)

	2.5G			5G			7.5G			10G		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
5/28	20.69	0.080 3	0.745 1	20.20	0.061 4	0.606 7	20.01	0.058 6	0.541 3	19.87	0.056 9	0.478 0
26	20.65	0.099 1	0.724 9	20.25	0.078 3	0.594 1	20.08	0.072 7	0.532 5	19.92	0.068 5	0.473 7
24	20.56	0.117 9	0.703 1	20.27	0.094 7	0.581 7	20.14	0.087 2	0.523 9	19.99	0.080 4	0.468 8
22	20.46	0.136 2	0.680 3	20.26	0.113 3	0.566 0	20.15	0.104 0	0.513 1	20.04	0.094 9	0.462 9
20	20.33	0.155 8	0.653 3	20.21	0.130 4	0.551 9	20.15	0.120 0	0.502 3	20.07	0.110 9	0.456 6
18	20.15	0.175 9	0.624 1	20.15	0.147 3	0.536 9	20.11	0.135 8	0.491 1	20.06	0.126 3	0.449 7
16	19.96	0.198 0	0.590 6	20.04	0.167 8	0.517 3	20.02	0.155 7	0.476 4	20.01	0.145 6	0.440 2
14	19.78	0.218 7	0.555 5	19.88	0.189 6	0.495 6	19.90	0.176 3	0.461 0	19.90	0.166 0	0.429 3
12	19.64	0.236 4	0.521 1	19.73	0.209 1	0.475 1	19.76	0.195 4	0.445 7	19.77	0.184 4	0.418 6
10	19.56	0.255 0	0.484 6	19.57	0.232 1	0.449 1	19.58	0.219 5	0.425 2	19.59	0.209 2	0.403 0
8	19.51	0.270 2	0.452 4	19.52	0.250 8	0.426 3	19.52	0.239 4	0.407 8	19.52	0.229 8	0.389 7
6	19.45	0.284 1	0.418 8	19.46	0.269 3	0.401 1	19.46	0.260 3	0.387 9	19.46	0.252 6	0.374 4
4	19.39	0.295 2	0.387 5	19.40	0.285 1	0.377 2	19.40	0.278 6	0.369 1	19.40	0.272 3	0.360 3
3	19.36	0.300 1	0.372 6	19.36	0.292 5	0.365 1	19.37	0.287 6	0.359 3	19.37	0.282 7	0.352 6
2	19.33	0.304 8	0.358 0	19.33	0.299 6	0.352 8	19.33	0.296 4	0.349 2	19.33	0.292 9	0.344 8
1	19.29	0.309 0	0.343 6	19.29	0.306 4	0.340 8	19.29	0.304 8	0.339 2	19.29	0.303 0	0.336 9
4/26	12.53	0.053 0	0.754 8	12.11	0.040 3	0.613 8	11.93	0.038 5	0.539 6	11.75	0.039 0	0.467 8
24	12.53	0.075 6	0.733 1	12.17	0.060 5	0.600 6	12.02	0.057 0	0.530 9	11.85	0.054 2	0.463 8
22	12.50	0.099 8	0.708 3	12.21	0.082 8	0.585 4	12.08	0.075 7	0.521 4	11.94	0.068 9	0.460 1
20	12.44	0.121 4	0.683 3	12.24	0.100 3	0.572 6	12.12	0.091 3	0.512 7	12.00	0.083 6	0.456 1
18	12.37	0.142 5	0.657 2	12.23	0.117 2	0.559 0	12.14	0.107 1	0.503 4	12.05	0.099 2	0.451 4
16	12.25	0.165 8	0.625 7	12.21	0.138 5	0.540 8	12.15	0.127 8	0.490 1	12.08	0.119 8	0.443 6
14	12.14	0.188 4	0.592 7	12.15	0.161 0	0.520 6	12.12	0.148 5	0.475 9	12.09	0.138 5	0.436 4
12	12.03	0.210 4	0.557 1	12.07	0.182 7	0.499 0	12.07	0.169 3	0.461 1	12.05	0.159 1	0.426 4
10	11.93	0.233 6	0.515 0	11.96	0.210 3	0.470 2	11.97	0.198 0	0.439 9	11.97	0.186 9	0.411 9
8	11.87	0.254 8	0.474 2	11.88	0.235 2	0.442 6	11.88	0.222 8	0.419 1	11.88	0.212 2	0.397 3
6	11.83	0.273 0	0.436 1	11.84	0.258 0	0.414 7	11.84	0.246 9	0.398 2	11.84	0.237 7	0.381 9
4	11.79	0.289 7	0.396 4	11.79	0.278 8	0.385 1	11.79	0.271 1	0.375 2	11.80	0.263 8	0.365 0
3	11.77	0.296 7	0.378 0	11.77	0.288 6	0.370 1	11.77	0.282 7	0.363 1	11.77	0.277 0	0.355 9
2	11.74	0.302 9	0.360 6	11.74	0.297 6	0.355 5	11.74	0.293 7	0.351 0	11.75	0.289 8	0.346 7
1	11.72	0.308 2	0.344 3	11.72	0.305 7	0.341 7	11.72	0.303 8	0.339 5	11.72	0.301 9	0.337 7
3/22	6.813	0.038 8	0.750 5	6.562	0.033 3	0.610 7	6.421	0.032 4	0.530 4	6.263	0.032 5	0.452 0
20	6.812	0.071 0	0.720 9	6.605	0.060 9	0.593 9	6.493	0.055 7	0.521 7	6.372	0.051 8	0.450 5
18	6.802	0.103 3	0.688 5	6.640	0.086 9	0.577 0	6.544	0.078 5	0.511 5	6.452	0.070 6	0.448 2
16	6.756	0.132 1	0.655 7	6.647	0.110 5	0.559 2	6.582	0.101 0	0.499 8	6.500	0.091 3	0.443 8
14	6.695	0.160 3	0.620 2	6.644	0.136 8	0.538 4	6.595	0.125 0	0.485 7	6.546	0.115 0	0.437 2
12	6.614	0.188 0	0.579 2	6.610	0.164 6	0.513 3	6.597	0.150 5	0.469 8	6.567	0.140 1	0.428 4
10	6.549	0.215 0	0.536 0	6.561	0.192 3	0.485 9	6.559	0.179 1	0.449 6	6.551	0.168 1	0.416 1
8	6.499	0.242 0	0.489 7	6.509	0.221 9	0.454 6	6.513	0.208 2	0.427 6	6.514	0.196 6	0.402 0
6	6.477	0.263 4	0.449 0	6.480	0.246 7	0.425 8	6.481	0.234 5	0.406 6	6.481	0.224 1	0.386 9
4	6.450	0.283 9	0.406 0	6.453	0.271 6	0.393 1	6.454	0.262 4	0.382 1	6.455	0.253 2	0.369 4
3	6.435	0.293 2	0.384 4	6.437	0.283 8	0.375 2	6.438	0.276 9	0.367 7	6.439	0.269 8	0.358 8
2	6.419	0.301 4	0.363 8	6.420	0.295 1	0.357 9	6.421	0.290 7	0.353 2	6.422	0.286 1	0.347 9
1	6.404	0.308 0	0.345 1	6.405	0.305 0	0.342 2	6.405	0.302 9	0.339 9	6.405	0.300 8	0.337 8
2/16	3.235	0.032 4	0.739 0	3.106	0.027 1	0.605 3	3.024	0.027 0	0.522 0	2.928	0.028 1	0.436 7
14	3.236	0.080 7	0.696 1	3.142	0.067 6	0.583 3	3.090	0.062 0	0.511 4	3.029	0.059 0	0.438 2
12	3.219	0.128 8	0.645 2	3.165	0.110 7	0.553 9	3.129	0.101 0	0.493 7	3.091	0.092 4	0.434 5
10	3.165	0.175 3	0.585 1	3.161	0.154 7	0.517 2	3.145	0.143 2	0.470 1	3.124	0.131 2	0.424 5
8	3.121	0.217 5	0.519 5	3.126	0.196 8	0.476 0	3.128	0.183 4	0.443 1	3.124	0.169 9	0.409 9
6	3.099	0.248 1	0.467 2	3.100	0.231 1	0.439 5	3.101	0.219 6	0.415 5	3.101	0.209 1	0.391 5
4	3.083	0.276 3	0.414 6	3.084	0.264 2	0.399 9	3.084	0.254 4	0.386 4	3.085	0.244 7	0.372 1
3	3.074	0.288 7	0.388 6	3.075	0.279 6	0.378 9	3.076	0.272 0	0.370 1	3.076	0.264 5	0.360 3
2	3.065	0.299 2	0.364 7	3.066	0.293 3	0.359 2	3.066	0.288 4	0.354 3	3.067	0.283 6	0.348 5
1	3.057	0.307 4	0.344 4	3.058	0.304 6	0.342 1	3.058	0.302 4	0.340 3	3.058	0.300 1	0.337 8
1/ 8	1.247	0.060 9	0.698 0	1.210	0.054 9	0.583 3	1.187	0.052 1	0.507 0	1.155	0.050 5	0.424 8
6	1.230	0.169 4	0.578 7	1.226	0.145 6	0.519 0	1.218	0.133 4	0.469 9	1.209	0.124 0	0.420 4
4	1.203	0.244 4	0.464 7	1.206	0.228 3	0.439 0	1.206	0.215 5	0.414 3	1.206	0.203 7	0.390 1
3	1.197	0.271 5	0.417 2	1.198	0.259 6	0.402 6	1.198	0.249 0	0.387 5	1.199	0.239 2	0.372 7
2	1.192	0.291 8	0.378 0	1.193	0.284 2	0.371 3	1.193	0.276 8	0.363 6	1.193	0.270 0	0.356 1
1	1.188	0.305 4	0.348 3	1.188	0.301 9	0.346 0	1.188	0.298 2	0.343 1	1.188	0.294 9	0.340 2

Annex Attached Table 1. (continued)

	2.5BG			5BG			7.5BG			10BG		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/10	77.11	0.238 6	0.372 4	77.08	0.230 6	0.356 4	77.05	0.222 1	0.338 7	—	—	—
8	77.14	0.251 7	0.366 0	77.12	0.244 6	0.353 3	77.08	0.237 1	0.338 2	—	—	—
6	77.19	0.266 4	0.358 2	77.15	0.261 2	0.348 8	77.10	0.255 7	0.337 1	77.06	0.251 6	0.327 0
4	77.05	0.282 2	0.349 2	77.05	0.278 5	0.343 1	77.05	0.274 6	0.335 3	77.06	0.271 9	0.328 5
3	76.96	0.289 5	0.344 9	76.96	0.286 8	0.340 2	76.96	0.283 9	0.334 0	76.97	0.282 5	0.329 3
2	76.87	0.296 8	0.340 3	76.87	0.295 2	0.336 9	76.87	0.293 3	0.332 6	76.87	0.293 0	0.329 7
1	76.76	0.304 5	0.335 2	76.77	0.303 8	0.333 3	76.78	0.303 0	0.331 0	76.78	0.303 2	0.329 9
8/18	58.62	0.175 6	0.396 1	—	—	—	—	—	—	—	—	—
16	58.56	0.191 2	0.391 3	58.57	0.181 2	0.363 6	58.60	0.172 0	0.335 7	—	—	—
14	58.48	0.205 6	0.385 6	58.48	0.195 8	0.361 0	58.49	0.186 9	0.336 0	58.52	0.178 9	0.311 9
12	58.38	0.219 8	0.379 9	58.37	0.210 4	0.358 3	58.38	0.201 4	0.336 1	58.40	0.194 1	0.315 3
10	58.26	0.235 7	0.372 9	58.26	0.227 0	0.354 7	58.26	0.219 1	0.336 1	58.27	0.212 7	0.319 0
8	58.15	0.250 8	0.365 6	58.14	0.242 8	0.351 0	58.14	0.236 2	0.335 6	58.15	0.231 3	0.322 1
6	58.02	0.265 9	0.357 9	58.02	0.260 1	0.346 9	58.02	0.253 9	0.335 0	58.02	0.250 4	0.325 1
4	57.89	0.280 7	0.349 5	57.89	0.276 9	0.342 2	57.89	0.273 6	0.334 5	57.89	0.270 5	0.327 6
3	57.83	0.288 3	0.345 1	57.82	0.285 3	0.339 6	57.82	0.282 9	0.333 5	57.83	0.281 0	0.328 4
2	57.75	0.296 1	0.340 4	57.75	0.294 1	0.336 5	57.75	0.292 2	0.332 1	57.76	0.291 7	0.329 1
1	57.67	0.304 3	0.335 2	57.68	0.303 1	0.333 2	57.68	0.302 1	0.330 6	57.69	0.302 3	0.329 4
7/22	43.49	0.133 8	0.406 1	—	—	—	—	—	—	—	—	—
20	43.40	0.148 9	0.403 6	43.45	0.138 0	0.362 1	—	—	—	—	—	—
18	43.28	0.162 3	0.399 7	43.34	0.151 3	0.362 5	43.40	0.142 4	0.329 1	—	—	—
16	43.07	0.178 5	0.393 9	43.13	0.167 3	0.360 6	43.19	0.158 2	0.330 8	43.26	0.148 5	0.297 5
14	42.85	0.193 0	0.388 2	42.86	0.183 7	0.358 0	42.88	0.175 1	0.332 0	42.82	0.167 0	0.301 7
12	42.59	0.210 2	0.380 9	42.59	0.199 8	0.355 4	42.58	0.191 6	0.332 2	42.59	0.184 3	0.306 4
10	42.50	0.226 7	0.374 2	42.50	0.216 8	0.352 9	42.50	0.209 9	0.333 2	42.49	0.204 1	0.312 2
8	42.41	0.244 6	0.366 7	42.40	0.236 2	0.349 5	42.40	0.230 1	0.333 8	42.40	0.224 5	0.317 4
6	42.30	0.261 9	0.358 2	42.30	0.255 5	0.345 5	42.30	0.250 4	0.333 9	42.30	0.246 2	0.322 2
4	42.20	0.278 0	0.349 9	42.21	0.272 8	0.341 5	42.21	0.268 8	0.333 6	42.21	0.266 0	0.325 6
3	42.15	0.286 2	0.345 4	42.15	0.282 2	0.339 1	42.15	0.279 2	0.333 0	42.15	0.277 3	0.327 0
2	42.09	0.294 8	0.340 6	42.10	0.291 9	0.336 3	42.10	0.290 0	0.332 1	42.10	0.289 2	0.328 2
1	42.03	0.303 6	0.335 2	42.04	0.302 1	0.333 1	42.04	0.301 3	0.330 9	42.04	0.301 1	0.329 0
6/22	30.61	0.111 9	0.407 3	—	—	—	—	—	—	—	—	—
20	30.57	0.126 4	0.404 9	30.55	0.116 3	0.356 0	—	—	—	—	—	—
18	30.49	0.142 1	0.401 4	30.50	0.131 7	0.357 1	30.50	0.123 9	0.320 3	30.49	0.117 1	0.278 4
16	30.33	0.159 3	0.396 5	30.37	0.148 4	0.356 6	30.39	0.140 0	0.323 7	30.40	0.132 7	0.286 4
14	30.12	0.177 4	0.390 2	30.16	0.165 7	0.355 0	30.16	0.158 0	0.325 8	30.13	0.151 2	0.292 8
12	29.89	0.195 2	0.383 1	29.91	0.184 3	0.352 6	29.90	0.176 1	0.326 8	29.82	0.169 7	0.298 0
10	29.70	0.215 0	0.375 5	29.69	0.204 0	0.350 1	29.69	0.196 4	0.328 1	29.69	0.191 3	0.305 0
8	29.63	0.233 7	0.368 5	29.62	0.224 3	0.347 5	29.62	0.217 8	0.330 2	29.62	0.212 4	0.311 3
6	29.55	0.253 5	0.360 3	29.55	0.245 2	0.344 6	29.55	0.239 6	0.331 1	29.55	0.234 8	0.317 1
4	29.48	0.271 6	0.351 6	29.47	0.266 3	0.341 0	29.47	0.262 0	0.331 8	29.47	0.259 5	0.322 6
3	29.43	0.281 8	0.346 3	29.43	0.277 7	0.338 6	29.43	0.274 4	0.331 6	29.43	0.272 6	0.325 1
2	29.38	0.292 2	0.340 6	29.38	0.289 3	0.335 8	29.38	0.287 1	0.331 2	29.38	0.285 9	0.327 2
1	29.33	0.302 7	0.334 8	29.34	0.301 1	0.332 7	29.34	0.299 9	0.330 4	29.34	0.299 4	0.328 7
5/24	19.81	0.073 0	0.403 4	—	—	—	—	—	—	—	—	—
22	19.87	0.085 2	0.401 7	19.69	0.077 0	0.337 6	—	—	—	—	—	—
20	19.94	0.099 4	0.400 7	19.76	0.089 4	0.339 7	—	—	—	—	—	—
18	19.98	0.115 3	0.399 0	19.84	0.103 4	0.342 6	19.70	0.097 0	0.298 5	—	—	—
16	19.97	0.133 6	0.396 1	19.91	0.122 9	0.346 5	19.83	0.115 2	0.306 9	19.70	0.109 2	0.265 4
14	19.89	0.154 9	0.391 6	19.87	0.143 7	0.348 2	19.84	0.135 2	0.313 2	19.80	0.129 4	0.277 1
12	19.79	0.172 8	0.386 7	19.78	0.160 7	0.347 9	19.76	0.153 0	0.317 1	19.73	0.147 7	0.284 8
10	19.62	0.197 8	0.378 7	19.62	0.184 9	0.346 3	19.61	0.177 5	0.321 2	19.57	0.171 5	0.293 3
8	19.52	0.220 8	0.370 5	19.51	0.210 4	0.344 9	19.51	0.203 5	0.325 0	19.51	0.197 5	0.302 6
6	19.45	0.245 6	0.361 0	19.45	0.237 0	0.342 9	19.45	0.230 2	0.328 4	19.45	0.224 5	0.311 0
4	19.40	0.267 2	0.351 8	19.39	0.260 6	0.339 6	19.39	0.256 5	0.330 0	19.39	0.252 8	0.319 0
3	19.36	0.278 6	0.346 5	19.36	0.273 1	0.337 4	19.36	0.269 7	0.330 2	19.36	0.267 1	0.322 4
2	19.33	0.290 0	0.340 9	19.33	0.286 2	0.335 0	19.33	0.283 3	0.330 2	19.33	0.281 8	0.325 2
1	19.30	0.301 4	0.335 1	19.30	0.299 4	0.332 3	19.30	0.297 6	0.329 8	19.30	0.296 9	0.327 6

Annex Attached Table 1. (continued)

	2.5BG			5BG			7.5BG			10BG		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
4/24	11.64	0.049 8	0.392 0	—	—	—	—	—	—	—	—	—
22	11.73	0.062 4	0.391 9	—	—	—	—	—	—	—	—	—
20	11.82	0.075 6	0.391 7	11.57	0.066 4	0.317 5	—	—	—	—	—	—
18	11.91	0.090 2	0.391 2	11.69	0.081 7	0.322 3	11.52	0.075 8	0.275 1	—	—	—
16	11.98	0.108 9	0.389 4	11.82	0.098 0	0.328 0	11.66	0.091 2	0.282 2	11.51	0.088 0	0.236 9
14	12.02	0.127 1	0.387 3	11.92	0.115 8	0.333 5	11.81	0.108 0	0.291 3	11.66	0.102 2	0.248 1
12	12.02	0.148 2	0.384 1	11.97	0.136 9	0.338 1	11.91	0.128 7	0.300 9	11.85	0.123 6	0.263 5
10	11.97	0.173 3	0.378 7	11.95	0.161 3	0.340 3	11.93	0.153 5	0.308 9	11.91	0.147 4	0.277 1
8	11.89	0.200 6	0.371 7	11.88	0.189 1	0.341 0	11.88	0.181 6	0.315 9	11.87	0.176 1	0.290 0
6	11.84	0.228 3	0.362 8	11.83	0.218 8	0.340 5	11.83	0.212 0	0.321 6	11.83	0.207 3	0.302 5
4	11.79	0.256 3	0.352 8	11.79	0.249 3	0.338 6	11.79	0.244 2	0.326 2	11.79	0.239 8	0.313 7
3	11.77	0.271 2	0.347 1	11.77	0.265 5	0.337 0	11.77	0.261 2	0.327 9	11.77	0.257 6	0.318 9
2	11.74	0.285 9	0.341 1	11.74	0.281 9	0.334 9	11.74	0.278 4	0.329 0	11.74	0.276 1	0.323 3
1	11.72	0.299 9	0.335 0	11.72	0.297 8	0.332 3	11.72	0.295 7	0.329 5	11.72	0.294 6	0.326 9
3/20	6.200	0.047 5	0.376 3	—	—	—	—	—	—	—	—	—
18	6.302	0.064 0	0.378 0	6.086	0.057 6	0.297 7	—	—	—	—	—	—
16	6.400	0.083 3	0.379 7	6.204	0.073 0	0.304 6	6.071	0.068 8	0.258 9	—	—	—
14	6.475	0.104 1	0.380 3	6.345	0.093 3	0.313 4	6.225	0.087 0	0.269 4	6.048	0.079 7	0.217 0
12	6.517	0.128 0	0.379 1	6.443	0.115 0	0.321 1	6.370	0.108 0	0.281 8	6.262	0.101 4	0.235 3
10	6.534	0.154 7	0.376 1	6.498	0.140 5	0.328 3	6.463	0.132 0	0.293 3	6.418	0.124 3	0.254 0
8	6.510	0.184 3	0.371 0	6.502	0.170 2	0.333 4	6.493	0.161 9	0.304 2	6.487	0.154 8	0.273 5
6	6.478	0.213 5	0.363 9	6.475	0.202 4	0.335 8	6.475	0.193 2	0.312 7	6.474	0.186 5	0.288 8
4	6.453	0.244 6	0.354 4	6.450	0.235 3	0.335 8	6.449	0.228 3	0.319 9	6.448	0.223 3	0.304 2
3	6.437	0.263 1	0.348 0	6.435	0.255 4	0.335 0	6.434	0.249 7	0.323 4	6.433	0.245 1	0.312 1
2	6.420	0.281 7	0.341 3	6.419	0.276 1	0.333 5	6.418	0.271 8	0.326 3	6.418	0.268 0	0.319 3
1	6.404	0.298 8	0.334 9	6.403	0.295 7	0.331 5	6.403	0.293 3	0.328 4	6.403	0.290 9	0.325 2
2/14	2.945	0.055 1	0.365 1	—	—	—	—	—	—	—	—	—
12	3.036	0.084 3	0.370 1	2.946	0.076 6	0.294 3	2.873	0.072 5	0.250 0	—	—	—
10	3.095	0.118 2	0.371 5	3.040	0.104 4	0.307 6	2.999	0.098 7	0.266 9	2.925	0.092 9	0.217 4
8	3.115	0.155 2	0.369 6	3.095	0.140 1	0.319 6	3.076	0.132 1	0.285 0	3.054	0.125 3	0.244 9
6	3.099	0.197 2	0.362 6	3.096	0.184 5	0.328 1	3.094	0.174 9	0.301 9	3.091	0.166 9	0.273 1
4	3.082	0.235 0	0.354 0	3.080	0.224 3	0.331 1	3.079	0.217 2	0.314 0	3.077	0.210 6	0.294 6
3	3.074	0.256 8	0.348 0	3.072	0.247 8	0.331 8	3.070	0.241 8	0.319 4	3.069	0.236 2	0.305 3
2	3.065	0.278 2	0.341 5	3.063	0.271 5	0.331 8	3.062	0.267 0	0.324 1	3.060	0.262 6	0.315 2
1	3.057	0.297 4	0.335 1	3.055	0.293 8	0.331 0	3.054	0.291 1	0.327 4	3.052	0.288 6	0.323 3
1/ 8	1.117	0.047 4	0.349 4	—	—	—	—	—	—	—	—	—
6	1.194	0.116 2	0.360 9	1.178	0.108 7	0.298 0	1.162	0.105 6	0.257 2	1.153	0.107 2	0.219 6
4	1.205	0.188 3	0.357 8	1.201	0.175 4	0.318 4	1.199	0.170 4	0.292 3	1.195	0.166 0	0.264 2
3	1.197	0.226 1	0.351 6	1.195	0.213 8	0.324 9	1.193	0.207 3	0.305 8	1.191	0.201 0	0.284 3
2	1.191	0.261 3	0.344 0	1.189	0.251 5	0.328 9	1.188	0.244 6	0.316 7	1.186	0.237 9	0.302 2
1	1.187	0.291 0	0.336 2	1.185	0.285 4	0.330 3	1.183	0.280 4	0.324 5	1.181	0.275 5	0.317 2

Annex Attached Table 1. (continued)

2.5B				5B			7.5B			10B		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/ 4	77.04	0.270 0	0.321 8	76.99	0.269 6	0.314 9	76.94	0.270 9	0.310 4	76.91	0.273 5	0.306 5
3	76.94	0.282 1	0.324 2	76.91	0.282 8	0.319 9	76.88	0.284 7	0.316 9	76.85	0.286 6	0.314 6
2	76.85	0.293 3	0.326 3	76.83	0.294 4	0.323 9	76.80	0.296 2	0.322 3	76.79	0.297 5	0.321 2
1	76.77	0.303 6	0.328 0	76.76	0.304 4	0.327 1	76.74	0.305 7	0.326 5	76.73	0.306 3	0.326 1
8/12	58.46	0.188 0	0.292 9	—	—	—	—	—	—	—	—	—
10	58.28	0.207 4	0.300 6	—	—	—	—	—	—	—	—	—
8	58.13	0.227 6	0.308 0	58.12	0.225 0	0.291 7	58.14	0.226 6	0.282 4	58.19	0.230 9	0.274 3
6	58.01	0.247 8	0.315 2	57.97	0.247 4	0.303 8	57.94	0.249 1	0.296 9	57.88	0.253 3	0.290 5
4	57.88	0.268 7	0.321 2	57.85	0.269 2	0.314 2	57.82	0.271 0	0.309 9	57.78	0.274 2	0.305 2
3	57.81	0.280 5	0.323 9	57.79	0.281 4	0.319 1	57.76	0.283 1	0.316 0	57.73	0.285 4	0.312 9
2	57.74	0.292 1	0.326 2	57.72	0.293 3	0.323 3	57.70	0.294 7	0.321 4	57.69	0.296 1	0.319 8
1	57.68	0.303 1	0.328 1	57.66	0.304 0	0.326 9	57.65	0.304 9	0.326 0	57.65	0.305 5	0.325 5
7/16	43.35	0.143 0	0.267 7	—	—	—	—	—	—	—	—	—
14	42.79	0.162 2	0.276 0	43.03	0.161 3	0.248 9	—	—	—	—	—	—
12	42.58	0.179 9	0.284 1	42.55	0.178 0	0.259 2	42.64	0.182 2	0.246 6	42.76	0.188 8	0.236 7
10	42.48	0.200 1	0.293 9	42.45	0.199 4	0.273 8	42.40	0.202 6	0.262 0	42.34	0.209 1	0.253 1
8	42.38	0.221 9	0.302 9	42.35	0.221 7	0.288 4	42.31	0.224 0	0.278 3	42.26	0.229 4	0.270 7
6	42.29	0.243 3	0.311 3	42.26	0.242 7	0.300 5	42.23	0.245 5	0.293 5	42.19	0.249 9	0.287 3
4	42.19	0.264 8	0.318 4	42.17	0.265 3	0.311 7	42.15	0.267 3	0.307 1	42.12	0.270 8	0.302 8
3	42.14	0.276 8	0.321 9	42.12	0.277 6	0.316 9	42.11	0.279 3	0.313 6	42.08	0.282 2	0.310 4
2	42.09	0.289 0	0.324 9	42.08	0.289 9	0.321 6	42.06	0.291 3	0.319 5	42.05	0.293 4	0.317 5
1	42.04	0.301 1	0.327 5	42.03	0.301 8	0.325 9	42.02	0.302 6	0.324 9	42.01	0.303 8	0.324 0
6/16	30.42	0.128 2	0.255 3	30.39	0.129 6	0.224 0	30.20	0.136 4	0.205 2	30.02	0.144 4	0.193 5
14	30.11	0.147 3	0.265 0	29.96	0.148 9	0.236 6	29.75	0.155 2	0.219 7	29.69	0.162 7	0.209 4
12	29.76	0.165 8	0.273 2	29.72	0.168 5	0.250 1	29.68	0.173 6	0.235 8	29.63	0.180 8	0.226 2
10	29.68	0.188 3	0.284 8	29.65	0.188 8	0.264 7	29.61	0.194 2	0.252 8	29.56	0.201 1	0.244 7
8	29.61	0.208 9	0.295 0	29.58	0.209 9	0.279 2	29.55	0.214 5	0.268 9	29.51	0.220 4	0.261 6
6	29.54	0.232 6	0.305 4	29.51	0.233 5	0.294 1	29.49	0.236 9	0.285 7	29.45	0.241 9	0.279 6
4	29.46	0.258 9	0.315 6	29.44	0.259 9	0.308 4	29.42	0.262 3	0.302 5	29.40	0.266 0	0.298 2
3	29.42	0.272 4	0.319 9	29.40	0.273 3	0.314 7	29.39	0.275 1	0.310 3	29.37	0.277 9	0.306 8
2	29.38	0.285 8	0.323 7	29.37	0.286 6	0.320 2	29.36	0.287 9	0.317 5	29.35	0.289 7	0.314 9
1	29.34	0.299 3	0.326 8	29.33	0.299 9	0.325 1	29.33	0.300 5	0.324 0	29.32	0.301 4	0.322 4
5/18	—	—	—	—	—	—	—	—	—	19.47	0.118 4	0.161 8
16	19.60	0.107 4	0.230 8	19.54	0.111 5	0.199 1	19.58	0.121 1	0.184 8	19.60	0.131 1	0.176 9
14	19.75	0.126 8	0.246 8	19.69	0.130 5	0.218 3	19.62	0.139 3	0.202 9	19.57	0.148 5	0.194 1
12	19.69	0.145 2	0.258 2	19.61	0.149 8	0.233 5	19.55	0.158 1	0.219 5	19.52	0.166 6	0.211 0
10	19.56	0.169 6	0.271 7	19.53	0.173 0	0.250 7	19.50	0.179 6	0.238 3	19.47	0.186 7	0.229 6
8	19.50	0.195 3	0.285 0	19.48	0.196 6	0.267 7	19.45	0.201 7	0.257 0	19.43	0.208 0	0.249 2
6	19.44	0.222 2	0.298 0	19.43	0.222 8	0.285 5	19.41	0.226 3	0.276 2	19.38	0.231 7	0.269 4
4	19.39	0.250 9	0.310 3	19.38	0.251 2	0.302 7	19.36	0.253 1	0.295 4	19.34	0.256 9	0.290 0
3	19.36	0.266 0	0.316 0	19.35	0.266 3	0.310 2	19.34	0.267 7	0.304 9	19.32	0.270 6	0.300 3
2	19.33	0.281 3	0.321 1	19.32	0.281 7	0.317 2	19.31	0.282 7	0.313 9	19.30	0.284 6	0.310 4
1	19.30	0.297 0	0.325 7	19.29	0.297 3	0.323 5	19.29	0.297 9	0.322 2	19.29	0.298 9	0.320 1
4/16	11.41	0.089 3	0.202 3	—	—	—	—	—	—	11.43	0.114 4	0.147 4
14	11.55	0.101 8	0.213 6	11.52	0.108 7	0.186 2	11.62	0.119 0	0.175 2	11.75	0.129 7	0.169 3
12	11.81	0.123 4	0.235 0	11.81	0.128 7	0.209 8	11.84	0.138 3	0.197 5	11.88	0.148 0	0.190 1
10	11.89	0.145 6	0.251 6	11.88	0.150 7	0.230 5	11.87	0.159 8	0.217 9	11.84	0.168 2	0.209 9
8	11.87	0.173 8	0.269 0	11.85	0.176 1	0.250 4	11.83	0.182 6	0.238 4	11.81	0.190 1	0.230 6
6	11.82	0.205 7	0.286 8	11.81	0.207 0	0.272 7	11.80	0.211 5	0.262 1	11.78	0.217 2	0.255 3
4	11.78	0.237 5	0.302 4	11.78	0.238 0	0.293 2	11.77	0.240 7	0.285 1	11.75	0.245 0	0.279 2
3	11.76	0.255 9	0.310 4	11.76	0.255 8	0.303 5	11.75	0.257 6	0.297 1	11.74	0.260 9	0.292 0
2	11.74	0.274 9	0.318 0	11.74	0.274 5	0.313 3	11.73	0.275 7	0.308 7	11.73	0.277 8	0.304 9
1	11.72	0.294 0	0.324 4	11.72	0.293 7	0.322 1	11.71	0.294 2	0.319 6	11.71	0.295 2	0.317 5



Annex Attached Table 1. (continued)

	2.5B			5B			7.5B			10B		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
3/14	—	—	—	—	—	—	—	—	—	6.014	0.106 8	0.128 6
12	6.156	0.098 8	0.200 3	6.123	0.104 2	0.171 0	6.173	0.112 8	0.158 4	6.266	0.122 1	0.152 8
10	6.375	0.121 3	0.224 3	6.373	0.125 1	0.198 6	6.422	0.133 4	0.187 6	6.472	0.142 4	0.180 7
8	6.481	0.150 7	0.248 8	6.483	0.152 3	0.227 3	6.482	0.158 0	0.213 6	6.469	0.165 8	0.204 7
6	6.472	0.183 0	0.269 8	6.466	0.184 0	0.253 1	6.458	0.188 2	0.240 8	6.448	0.194 3	0.231 8
4	6.446	0.219 5	0.290 3	6.442	0.218 9	0.278 4	6.436	0.221 5	0.268 4	6.428	0.226 3	0.261 1
3	6.431	0.242 0	0.301 7	6.429	0.240 6	0.292 5	6.424	0.241 7	0.284 1	6.419	0.245 0	0.277 3
2	6.417	0.265 7	0.312 6	6.415	0.263 8	0.306 4	6.413	0.263 8	0.299 8	6.409	0.265 5	0.294 1
1	6.402	0.289 6	0.322 1	6.402	0.288 2	0.318 9	6.401	0.287 6	0.315 2	6.398	0.288 1	0.311 4
2/10	2.870	0.091 4	0.184 1	2.861	0.096 8	0.156 6	2.885	0.105 3	0.143 6	2.932	0.115 7	0.137 8
8	3.038	0.122 5	0.217 8	3.026	0.124 0	0.191 8	3.048	0.130 6	0.179 5	3.077	0.138 7	0.172 4
6	3.091	0.162 0	0.251 6	3.090	0.161 6	0.231 6	3.086	0.165 8	0.217 3	3.081	0.171 9	0.207 7
4	3.076	0.207 0	0.280 3	3.075	0.205 9	0.266 9	3.072	0.207 6	0.254 7	3.068	0.211 7	0.245 5
3	3.068	0.233 0	0.294 8	3.067	0.231 4	0.284 7	3.065	0.231 3	0.274 4	3.062	0.234 0	0.265 6
2	3.060	0.259 8	0.308 2	3.059	0.258 0	0.301 5	3.058	0.256 7	0.293 9	3.056	0.258 2	0.286 3
1	3.052	0.286 8	0.319 8	3.052	0.285 4	0.316 5	3.052	0.283 9	0.312 3	3.051	0.284 4	0.307 4
1/ 8	—	—	—	—	—	—	1.104	0.096 9	0.128 1	1.114	0.107 8	0.122 9
6	1.151	0.111 7	0.196 8	1.161	0.121 0	0.181 3	1.172	0.129 9	0.172 2	1.185	0.138 6	0.166 8
4	1.194	0.165 1	0.246 7	1.193	0.166 9	0.230 8	1.192	0.172 0	0.218 8	1.190	0.179 0	0.210 9
3	1.191	0.198 0	0.270 2	1.190	0.196 8	0.256 4	1.188	0.199 1	0.244 3	1.187	0.203 5	0.235 2
2	1.186	0.233 9	0.292 1	1.185	0.230 9	0.281 6	1.185	0.231 0	0.271 6	1.184	0.233 0	0.262 5
1	1.181	0.272 4	0.311 9	1.181	0.269 6	0.306 0	1.181	0.268 7	0.299 9	1.180	0.269 0	0.293 3

Annex Attached Table 1. (continued)

2.5PB				5PB			7.5PB			10PB		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/ 4	—	—	—	—	—	—	—	—	—	76.69	0.294 0	0.298 2
3	—	—	—	—	—	—	—	—	—	77.77	0.301 4	0.281 2
2	76.75	0.300 2	0.319 7	76.73	0.301 9	0.319 0	76.71	0.304 3	0.318 4	76.70	0.306 7	0.318 5
1	76.72	0.306 5	0.324 6	76.71	0.307 4	0.324 2	76.71	0.308 6	0.323 9	76.70	0.310 6	0.325 0
8/ 8	—	—	—	—	—	—	—	—	—	57.87	0.270 6	0.257 9
6	57.79	0.258 6	0.285 1	57.72	0.264 0	0.280 8	57.65	0.273 1	0.278 3	57.60	0.282 3	0.278 0
4	57.73	0.278 4	0.301 8	57.68	0.282 5	0.299 8	57.64	0.288 5	0.298 0	57.61	0.294 1	0.298 0
3	57.69	0.288 8	0.310 3	57.66	0.291 8	0.308 9	57.63	0.296 2	0.307 7	57.61	0.300 2	0.307 8
2	57.66	0.298 4	0.318 2	57.65	0.300 2	0.317 2	57.63	0.303 1	0.316 6	57.62	0.305 6	0.316 6
1	57.64	0.306 7	0.324 8	57.63	0.307 4	0.324 2	57.62	0.308 9	0.324 0	57.62	0.310 0	0.323 9
7/12	—	—	—	—	—	—	—	—	—	42.05	0.249 4	0.218 3
10	42.23	0.217 8	0.245 2	42.13	0.227 4	0.240 4	42.02	0.243 6	0.235 4	41.95	0.259 4	0.236 6
8	42.17	0.237 2	0.264 1	42.10	0.245 0	0.259 6	42.01	0.257 4	0.255 1	41.96	0.270 2	0.255 4
6	42.12	0.256 1	0.281 9	42.07	0.262 2	0.278 1	42.01	0.271 6	0.274 6	41.97	0.280 8	0.274 3
4	42.07	0.275 5	0.298 7	42.04	0.280 0	0.296 5	42.00	0.286 2	0.294 3	41.98	0.291 7	0.293 3
3	42.05	0.285 8	0.307 6	42.02	0.289 2	0.305 7	42.00	0.293 8	0.304 1	41.98	0.297 6	0.303 4
2	42.03	0.295 9	0.316 0	42.01	0.298 0	0.314 5	41.99	0.301 1	0.313 5	41.99	0.303 4	0.313 1
1	42.00	0.305 1	0.323 5	42.00	0.306 0	0.322 5	41.99	0.307 5	0.322 0	41.99	0.308 6	0.321 9
6/16	—	—	—	—	—	—	—	—	—	29.25	0.229 1	0.177 9
14	29.57	0.175 7	0.200 5	29.46	0.188 2	0.195 1	29.32	0.213 8	0.191 8	29.24	0.238 1	0.195 3
12	29.52	0.192 2	0.217 8	29.43	0.204 0	0.213 2	29.32	0.226 4	0.209 9	29.25	0.247 0	0.211 7
10	29.48	0.211 0	0.236 7	29.40	0.221 6	0.232 4	29.32	0.240 4	0.229 7	29.26	0.257 2	0.229 9
8	29.44	0.229 3	0.254 8	29.38	0.238 3	0.250 2	29.31	0.253 3	0.247 8	29.27	0.266 9	0.247 9
6	29.40	0.248 7	0.274 1	29.36	0.255 8	0.269 6	29.31	0.266 7	0.266 4	29.28	0.277 2	0.266 2
4	29.36	0.270 9	0.294 3	29.33	0.276 1	0.291 5	29.31	0.282 8	0.288 6	29.29	0.289 4	0.287 8
3	29.35	0.281 7	0.303 8	29.32	0.285 8	0.301 5	29.30	0.290 7	0.299 2	29.29	0.295 7	0.298 6
2	29.33	0.292 4	0.312 6	29.32	0.295 1	0.311 2	29.30	0.298 4	0.309 5	29.29	0.301 8	0.309 2
1	29.31	0.302 7	0.321 2	29.31	0.304 1	0.320 4	29.30	0.305 8	0.319 5	29.30	0.307 6	0.319 4
5/22	—	—	—	—	—	—	—	—	—	18.99	0.210 0	0.129 8
20	—	—	—	—	—	—	19.15	0.179 8	0.132 5	19.17	0.214 5	0.141 9
18	19.49	0.134 8	0.152 8	19.39	0.151 0	0.147 4	19.28	0.187 2	0.146 5	19.19	0.219 9	0.154 0
16	19.50	0.148 7	0.168 6	19.41	0.163 6	0.164 0	19.28	0.195 8	0.161 8	19.20	0.225 1	0.165 6
14	19.47	0.164 1	0.186 1	19.39	0.177 8	0.181 4	19.28	0.205 9	0.177 5	19.21	0.232 7	0.180 6
12	19.43	0.179 8	0.203 1	19.37	0.192 8	0.198 8	19.28	0.217 8	0.195 0	19.22	0.241 4	0.197 1
10	19.40	0.197 9	0.221 8	19.35	0.209 6	0.217 4	19.28	0.230 9	0.214 5	19.23	0.251 0	0.214 9
8	19.37	0.217 3	0.241 9	19.33	0.227 6	0.237 5	19.28	0.244 4	0.233 3	19.24	0.260 4	0.233 5
6	19.35	0.238 6	0.263 0	19.31	0.247 1	0.258 6	19.28	0.259 2	0.254 9	19.25	0.271 9	0.253 9
4	19.32	0.262 5	0.286 0	19.30	0.268 9	0.282 4	19.27	0.276 9	0.279 9	19.26	0.285 3	0.278 9
3	19.31	0.274 8	0.297 0	19.29	0.280 0	0.294 1	19.27	0.285 8	0.292 0	19.26	0.292 1	0.291 1
2	19.29	0.287 4	0.307 8	19.28	0.291 0	0.305 7	19.27	0.294 8	0.304 0	19.26	0.298 9	0.303 5
1	19.28	0.300 0	0.318 5	19.27	0.302 0	0.317 4	19.27	0.303 8	0.316 4	19.27	0.305 8	0.316 2
4/30	—	—	—	—	—	—	—	—	—	11.04	0.196 2	0.079 8
28	—	—	—	—	—	—	—	—	—	11.16	0.198 3	0.086 9
26	—	—	—	—	—	—	11.19	0.165 9	0.085 7	11.24	0.200 9	0.094 2
24	—	—	—	—	—	—	11.31	0.168 6	0.094 2	11.35	0.203 7	0.103 3
22	—	—	—	—	—	—	11.41	0.171 9	0.103 4	11.42	0.206 8	0.112 1
20	—	—	—	11.35	0.127 6	0.107 6	11.50	0.175 0	0.112 2	11.49	0.209 8	0.120 5
18	11.38	0.120 6	0.126 1	11.58	0.138 3	0.124 5	11.62	0.180 7	0.126 7	11.58	0.214 5	0.133 6
16	11.66	0.132 4	0.144 2	11.70	0.149 8	0.141 6	11.70	0.187 1	0.141 3	11.64	0.219 6	0.146 4
14	11.81	0.146 5	0.163 3	11.78	0.162 5	0.159 5	11.70	0.195 5	0.157 3	11.65	0.224 7	0.166 1
12	11.82	0.163 3	0.182 9	11.77	0.177 8	0.178 2	11.70	0.205 4	0.174 1	11.66	0.232 7	0.176 4
10	11.80	0.181 1	0.202 4	11.76	0.193 6	0.197 1	11.70	0.217 9	0.192 9	11.67	0.241 9	0.194 9
8	11.78	0.200 7	0.223 3	11.74	0.212 0	0.218 2	11.70	0.232 9	0.214 7	11.68	0.252 9	0.215 6
6	11.75	0.225 4	0.248 4	11.73	0.234 7	0.243 5	11.70	0.249 9	0.239 5	11.68	0.265 1	0.238 7
4	11.74	0.251 0	0.273 7	11.72	0.258 9	0.269 6	11.70	0.268 7	0.266 0	11.69	0.279 2	0.265 0
3	11.73	0.265 5	0.287 3	11.71	0.271 4	0.283 3	11.70	0.278 6	0.280 0	11.69	0.286 5	0.278 6
2	11.72	0.280 9	0.301 3	11.71	0.284 4	0.297 6	11.70	0.289 1	0.295 1	11.69	0.294 3	0.293 3
1	11.71	0.296 7	0.315 4	11.70	0.298 2	0.312 9	11.70	0.300 4	0.311 4	11.70	0.303 0	0.310 0

Annex Attached Table 1. (continued)

	2.5PB			5PB			7.5PB			10PB		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
3/34	—	—	—	—	—	—	5.963	0.160 7	0.048 9	5.998	0.192 3	0.051 5
32	—	—	—	—	—	—	5.998	0.161 2	0.052 3	6.033	0.193 3	0.055 8
30	—	—	—	—	—	—	6.037	0.162 3	0.057 3	6.076	0.194 7	0.062 1
28	—	—	—	—	—	—	6.087	0.163 8	0.063 1	6.103	0.196 1	0.067 6
26	—	—	—	—	—	—	6.121	0.164 8	0.068 2	6.134	0.197 9	0.073 8
24	—	—	—	—	—	—	6.160	0.166 5	0.074 5	6.173	0.200 2	0.080 9
22	—	—	—	—	—	—	6.204	0.168 4	0.082 4	6.211	0.202 7	0.089 1
20	—	—	—	—	—	—	6.248	0.171 0	0.091 9	6.243	0.205 4	0.098 2
18	—	—	—	5.994	0.122 8	0.089 7	6.279	0.173 9	0.100 7	6.272	0.208 5	0.108 0
16	—	—	—	6.159	0.131 2	0.106 4	6.325	0.177 4	0.111 9	6.301	0.211 8	0.118 7
14	6.175	0.124 5	0.126 3	6.337	0.142 5	0.126 3	6.363	0.183 4	0.127 3	6.335	0.216 8	0.133 1
12	6.394	0.139 0	0.149 5	6.422	0.155 3	0.146 2	6.386	0.191 6	0.145 1	6.356	0.223 4	0.149 9
10	6.458	0.157 2	0.172 7	6.429	0.172 1	0.168 0	6.389	0.202 2	0.164 2	6.363	0.230 8	0.166 5
8	6.443	0.178 5	0.196 6	6.420	0.191 9	0.192 5	6.390	0.217 1	0.187 6	6.370	0.241 9	0.189 5
6	6.429	0.203 6	0.223 8	6.412	0.214 0	0.218 3	6.390	0.233 7	0.213 2	6.376	0.254 4	0.214 8
4	6.415	0.233 3	0.254 4	6.404	0.241 7	0.249 5	6.390	0.254 9	0.244 7	6.381	0.269 4	0.244 2
3	6.409	0.250 2	0.271 3	6.400	0.257 0	0.266 7	6.390	0.267 1	0.262 3	6.383	0.278 1	0.260 7
2	6.402	0.268 9	0.289 3	6.396	0.273 6	0.285 3	6.390	0.280 8	0.281 7	6.385	0.288 0	0.279 7
1	6.395	0.289 7	0.308 6	6.393	0.292 2	0.306 0	6.390	0.295 9	0.303 8	6.388	0.299 5	0.302 2
2/38	—	—	—	—	—	—	2.859	0.162 1	0.028 8	—	—	—
36	—	—	—	—	—	—	2.878	0.162 8	0.032 0	—	—	—
34	—	—	—	—	—	—	2.900	0.163 1	0.035 3	2.859	0.191 7	0.035 5
32	—	—	—	—	—	—	2.916	0.163 7	0.039 0	2.878	0.192 5	0.039 3
30	—	—	—	—	—	—	2.931	0.164 3	0.043 0	2.891	0.193 4	0.043 6
28	—	—	—	—	—	—	2.945	0.165 0	0.047 5	2.917	0.195 1	0.049 2
26	—	—	—	—	—	—	2.951	0.165 6	0.051 8	2.940	0.196 7	0.054 7
24	—	—	—	—	—	—	2.971	0.166 3	0.057 1	2.957	0.198 2	0.061 0
22	—	—	—	—	—	—	2.983	0.167 4	0.063 2	2.970	0.199 9	0.068 1
20	—	—	—	—	—	—	2.993	0.169 0	0.071 0	2.980	0.202 0	0.076 2
18	—	—	—	—	—	—	3.002	0.170 7	0.079 2	2.991	0.204 4	0.085 9
16	—	—	—	—	—	—	3.012	0.173 6	0.089 6	3.001	0.207 6	0.096 8
14	—	—	—	2.886	0.125 5	0.088 0	3.022	0.177 1	0.102 2	3.011	0.211 2	0.109 3
12	2.886	0.116 8	0.108 4	2.977	0.135 8	0.109 7	3.032	0.182 4	0.117 2	3.020	0.216 6	0.124 6
10	3.013	0.132 5	0.134 9	3.055	0.149 5	0.133 3	3.042	0.189 5	0.134 9	3.027	0.222 9	0.141 6
8	3.079	0.153 5	0.165 2	3.065	0.168 7	0.160 5	3.045	0.202 3	0.159 8	3.033	0.232 5	0.164 8
6	3.069	0.183 3	0.198 8	3.059	0.195 5	0.193 5	3.046	0.221 3	0.190 4	3.037	0.247 4	0.194 8
4	3.061	0.219 3	0.238 1	3.054	0.228 6	0.232 2	3.046	0.244 9	0.227 1	3.041	0.263 6	0.227 9
3	3.057	0.239 7	0.259 0	3.052	0.246 8	0.253 0	3.046	0.258 7	0.247 7	3.042	0.272 9	0.246 7
2	3.053	0.261 8	0.281 0	3.050	0.266 7	0.275 5	3.046	0.274 4	0.270 9	3.044	0.283 8	0.269 0
1	3.049	0.286 1	0.304 2	3.048	0.288 5	0.300 6	3.047	0.292 3	0.297 6	3.046	0.297 0	0.295 8
1/38	—	—	—	—	—	—	1.072	0.168 0	0.014 2	—	—	—
36	—	—	—	—	—	—	1.089	0.168 2	0.016 4	—	—	—
34	—	—	—	—	—	—	1.101	0.168 4	0.018 6	—	—	—
32	—	—	—	—	—	—	1.111	0.168 4	0.021 1	—	—	—
30	—	—	—	—	—	—	1.122	0.168 7	0.024 7	1.091	0.194 5	0.025 1
28	—	—	—	—	—	—	1.129	0.168 9	0.028 6	1.100	0.194 9	0.029 3
26	—	—	—	—	—	—	1.137	0.169 2	0.032 9	1.119	0.196 0	0.034 4
24	—	—	—	—	—	—	1.144	0.169 5	0.037 6	1.134	0.197 3	0.040 4
22	—	—	—	—	—	—	1.150	0.170 0	0.043 1	1.142	0.198 8	0.046 6
20	—	—	—	—	—	—	1.155	0.170 6	0.048 7	1.147	0.199 9	0.052 3
18	—	—	—	—	—	—	1.159	0.171 4	0.055 7	1.151	0.201 5	0.060 5
16	—	—	—	—	—	—	1.162	0.172 6	0.062 7	1.155	0.203 3	0.068 5
14	—	—	—	—	—	—	1.166	0.174 6	0.074 0	1.160	0.206 5	0.079 9
12	—	—	—	—	—	—	1.169	0.177 2	0.086 4	1.163	0.209 8	0.093 1
10	—	—	—	1.126	0.128 6	0.088 2	1.172	0.181 5	0.101 9	1.167	0.215 0	0.109 9
8	1.148	0.127 1	0.119 8	1.176	0.144 1	0.120 1	1.175	0.188 7	0.122 1	1.170	0.222 2	0.130 6
6	1.190	0.153 6	0.160 6	1.185	0.168 2	0.155 5	1.177	0.202 1	0.151 7	1.172	0.232 4	0.155 8
4	1.186	0.190 7	0.203 7	1.182	0.203 0	0.198 6	1.178	0.226 0	0.193 0	1.175	0.249 7	0.192 9
3	1.184	0.212 2	0.227 4	1.181	0.222 2	0.221 6	1.178	0.240 0	0.215 0	1.176	0.259 1	0.212 7
2	1.182	0.238 5	0.254 9	1.180	0.245 5	0.249 2	1.178	0.258 1	0.242 7	1.177	0.271 6	0.239 1
1	1.180	0.271 5	0.287 8	1.179	0.275 2	0.283 6	1.179	0.281 8	0.279 1	1.178	0.289 0	0.276 0

Annex Attached Table 1. (continued)

	2.5P			5P			7.5P			10P		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/ 6	—	—	—	—	—	—	76.44	0.315 7	0.290 7	76.03	0.325 7	0.295 3
4	76.66	0.299 4	0.299 5	76.64	0.303 5	0.299 9	76.58	0.315 0	0.305 3	76.51	0.321 0	0.308 9
3	76.68	0.304 1	0.309 8	76.66	0.306 9	0.310 6	76.64	0.314 3	0.313 6	76.62	0.318 2	0.316 0
2	76.69	0.307 9	0.318 1	76.68	0.309 6	0.319 0	76.67	0.313 6	0.321 0	76.66	0.315 7	0.322 2
1	76.70	0.310 8	0.324 6	76.70	0.311 6	0.325 2	76.69	0.313 1	0.326 6	76.69	0.313 8	0.326 9
8/14	—	—	—	—	—	—	—	—	—	56.29	0.340 2	0.242 4
12	—	—	—	—	—	—	57.31	0.316 3	0.247 8	56.72	0.336 5	0.255 9
10	—	—	—	57.91	0.290 6	0.251 0	57.39	0.315 9	0.261 1	57.01	0.333 0	0.268 3
8	57.71	0.283 3	0.261 8	57.64	0.295 0	0.266 1	57.45	0.315 6	0.274 5	57.24	0.329 3	0.281 0
6	57.56	0.291 4	0.280 0	57.53	0.299 8	0.283 1	57.49	0.315 0	0.290 8	57.46	0.325 0	0.295 0
4	57.59	0.299 4	0.298 0	57.57	0.304 4	0.299 7	57.54	0.314 7	0.304 1	57.53	0.320 9	0.307 9
3	57.60	0.303 7	0.307 9	57.59	0.307 0	0.309 0	57.57	0.314 2	0.312 2	57.56	0.318 5	0.314 8
2	57.61	0.307 7	0.317 0	57.60	0.309 4	0.317 7	57.59	0.313 7	0.319 9	57.59	0.316 1	0.321 2
1	57.62	0.310 9	0.324 5	57.62	0.311 4	0.324 8	57.61	0.313 1	0.325 9	57.61	0.314 1	0.326 2
7/22	—	—	—	—	—	—	—	—	—	40.96	0.350 6	0.194 7
20	—	—	—	—	—	—	—	—	—	41.09	0.348 2	0.205 9
18	—	—	—	—	—	—	41.51	0.315 1	0.205 0	41.22	0.345 9	0.216 6
16	—	—	—	—	—	—	41.61	0.315 4	0.217 0	41.35	0.343 1	0.227 7
14	—	—	—	42.03	0.284 1	0.218 4	41.68	0.315 2	0.229 4	41.49	0.339 8	0.240 1
12	42.05	0.269 8	0.225 0	41.94	0.287 3	0.231 5	41.76	0.315 1	0.242 9	41.61	0.336 6	0.252 4
10	41.89	0.276 5	0.241 1	41.85	0.291 2	0.246 2	41.80	0.315 2	0.255 6	41.72	0.333 5	0.264 0
8	41.92	0.283 4	0.258 4	41.89	0.295 6	0.262 7	41.84	0.315 0	0.270 2	41.81	0.329 9	0.276 9
6	41.94	0.290 7	0.276 1	41.92	0.299 6	0.278 9	41.88	0.314 9	0.285 2	41.86	0.326 0	0.290 5
4	41.96	0.298 2	0.293 9	41.94	0.304 2	0.295 9	41.92	0.314 5	0.300 5	41.91	0.321 6	0.304 3
3	41.97	0.302 2	0.303 6	41.96	0.306 6	0.305 0	41.94	0.314 3	0.308 7	41.93	0.319 1	0.311 4
2	41.98	0.306 1	0.313 0	41.97	0.308 9	0.313 9	41.96	0.313 9	0.316 5	41.96	0.316 9	0.318 1
1	41.99	0.309 6	0.321 7	41.98	0.311 1	0.322 2	41.98	0.313 5	0.323 5	41.98	0.314 7	0.324 1
6/26	—	—	—	—	—	—	—	—	—	28.72	0.354 0	0.167 0
24	—	—	—	—	—	—	28.71	0.312 9	0.161 2	28.74	0.352 0	0.176 7
22	—	—	—	—	—	—	28.79	0.313 0	0.171 0	28.78	0.350 3	0.185 7
20	—	—	—	28.99	0.274 8	0.170 7	28.87	0.313 3	0.182 5	28.84	0.348 2	0.196 0
18	29.15	0.253 8	0.175 7	29.04	0.277 6	0.183 1	28.95	0.313 5	0.195 8	28.90	0.345 6	0.207 9
16	29.16	0.258 4	0.187 2	29.09	0.280 6	0.195 2	29.01	0.313 6	0.207 0	28.95	0.343 3	0.218 5
14	29.17	0.263 1	0.201 9	29.13	0.283 8	0.208 6	29.06	0.313 6	0.219 6	29.01	0.340 7	0.229 9
12	29.20	0.268 4	0.216 7	29.16	0.287 2	0.223 3	29.11	0.313 9	0.232 9	29.07	0.337 4	0.243 2
10	29.22	0.274 0	0.232 3	29.19	0.290 3	0.237 6	29.14	0.313 8	0.246 2	29.11	0.334 2	0.255 8
8	29.24	0.280 6	0.249 5	29.21	0.294 4	0.254 1	29.18	0.314 1	0.261 8	29.16	0.330 3	0.269 7
6	29.26	0.287 7	0.267 6	29.24	0.298 7	0.270 9	29.21	0.314 0	0.277 0	29.19	0.326 6	0.283 3
4	29.27	0.296 5	0.288 8	29.26	0.303 5	0.290 5	29.25	0.314 2	0.295 5	29.24	0.321 7	0.299 3
3	29.28	0.300 6	0.298 9	29.27	0.305 9	0.300 0	29.26	0.314 1	0.303 9	29.25	0.319 8	0.306 9
2	29.29	0.304 6	0.309 0	29.28	0.308 1	0.309 6	29.27	0.313 8	0.312 0	29.27	0.317 8	0.314 4
1	29.29	0.308 7	0.319 1	29.29	0.310 4	0.319 2	29.29	0.313 5	0.320 3	29.28	0.315 5	0.321 8
5/30	—	—	—	—	—	—	18.85	0.308 5	0.122 4	18.98	0.358 8	0.137 7
28	—	—	—	18.65	0.267 1	0.118 0	18.85	0.309 1	0.131 1	18.95	0.356 9	0.145 4
26	18.67	0.238 1	0.118 9	18.76	0.268 6	0.127 9	18.86	0.309 3	0.139 2	18.94	0.355 5	0.152 6
24	18.82	0.240 6	0.128 4	18.84	0.270 2	0.136 6	18.89	0.309 8	0.148 8	18.93	0.353 3	0.162 3
22	18.94	0.243 7	0.138 7	18.93	0.272 2	0.146 9	18.92	0.310 4	0.157 0	18.94	0.351 6	0.171 5
20	19.07	0.247 6	0.150 3	19.01	0.274 3	0.158 0	18.97	0.310 5	0.168 3	18.96	0.349 7	0.181 0
18	19.12	0.251 5	0.162 4	19.08	0.276 6	0.169 3	19.02	0.311 1	0.179 5	18.98	0.347 0	0.192 0
16	19.14	0.255 4	0.174 2	19.10	0.279 1	0.181 3	19.06	0.311 7	0.192 1	19.02	0.344 7	0.203 7
14	19.16	0.259 9	0.187 8	19.13	0.282 1	0.194 8	19.09	0.312 2	0.204 7	19.05	0.342 1	0.215 8
12	19.18	0.264 6	0.202 2	19.15	0.285 1	0.208 3	19.12	0.312 3	0.218 2	19.09	0.339 2	0.228 4
10	19.20	0.270 3	0.219 0	19.18	0.288 8	0.224 9	19.15	0.312 8	0.233 8	19.12	0.336 0	0.243 1
8	19.22	0.276 5	0.236 0	19.20	0.292 6	0.241 2	19.17	0.313 2	0.248 7	19.15	0.332 8	0.257 3
6	19.23	0.284 2	0.256 8	19.22	0.297 0	0.260 8	19.20	0.313 4	0.267 3	19.19	0.328 6	0.274 5
4	19.25	0.293 2	0.279 4	19.24	0.302 1	0.282 4	19.22	0.313 7	0.287 2	19.22	0.323 6	0.292 7
3	19.25	0.298 1	0.291 7	19.25	0.304 9	0.293 9	19.24	0.313 7	0.297 8	19.23	0.320 8	0.302 0
2	19.26	0.303 1	0.304 1	19.25	0.307 7	0.305 6	19.25	0.313 5	0.308 5	19.25	0.318 0	0.311 1
1	19.26	0.308 0	0.316 7	19.26	0.310 4	0.317 4	19.26	0.313 3	0.319 1	19.26	0.315 4	0.320 2

Annex Attached Table 1. (continued)

	2.5P			5P			7.5P			10P		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
4/32	11.07	0.228 9	0.079 5	11.22	0.261 6	0.086 5	11.32	0.302 8	0.094 9	—	—	—
30	11.16	0.231 2	0.087 6	11.27	0.263 1	0.094 5	11.35	0.303 5	0.102 6	11.37	0.354 7	0.114 3
28	11.23	0.233 1	0.094 5	11.29	0.264 4	0.101 2	11.36	0.304 2	0.110 9	11.39	0.351 9	0.122 9
26	11.30	0.235 3	0.102 2	11.34	0.266 3	0.109 9	11.39	0.304 9	0.118 6	11.42	0.351 2	0.130 5
24	11.36	0.238 1	0.111 3	11.38	0.268 3	0.118 5	11.42	0.305 8	0.128 1	11.45	0.350 3	0.139 7
22	11.42	0.240 7	0.120 2	11.43	0.270 2	0.127 8	11.45	0.306 6	0.136 7	11.47	0.349 2	0.148 8
20	11.48	0.243 2	0.128 8	11.48	0.272 0	0.136 7	11.48	0.307 4	0.146 3	11.48	0.347 9	0.156 7
18	11.55	0.246 9	0.141 0	11.54	0.274 3	0.148 5	11.51	0.307 9	0.157 3	11.49	0.346 1	0.169 7
16	11.60	0.250 6	0.153 9	11.57	0.276 8	0.160 4	11.54	0.308 9	0.170 1	11.51	0.344 0	0.183 3
14	11.61	0.254 8	0.167 9	11.59	0.279 5	0.175 1	11.56	0.309 3	0.184 2	11.54	0.341 7	0.195 8
12	11.63	0.259 8	0.183 1	11.61	0.282 5	0.190 6	11.59	0.310 0	0.199 9	11.56	0.339 2	0.210 4
10	11.64	0.265 8	0.201 1	11.63	0.285 9	0.207 2	11.61	0.310 8	0.216 1	11.59	0.336 3	0.225 9
8	11.66	0.272 3	0.220 3	11.64	0.289 8	0.226 1	11.63	0.311 4	0.233 5	11.61	0.333 2	0.242 2
6	11.67	0.280 0	0.242 0	11.66	0.294 4	0.246 4	11.65	0.312 0	0.253 0	11.63	0.329 5	0.260 3
4	11.68	0.289 1	0.265 6	11.67	0.299 6	0.268 7	11.66	0.312 4	0.274 1	11.66	0.325 1	0.280 2
3	11.68	0.294 0	0.278 7	11.68	0.302 4	0.281 2	11.67	0.312 6	0.285 6	11.67	0.322 5	0.290 9
2	11.69	0.299 5	0.293 5	11.69	0.305 6	0.295 1	11.68	0.312 7	0.298 3	11.68	0.319 7	0.302 4
1	11.69	0.305 6	0.310 1	11.69	0.309 0	0.310 9	11.69	0.312 8	0.312 6	11.69	0.316 4	0.315 1
3/34	6.022	0.224 7	0.055 9	—	—	—	—	—	—	—	—	—
32	6.055	0.226 1	0.060 7	6.036	0.259 2	0.065 4	—	—	—	—	—	—
30	6.082	0.227 2	0.066 2	6.067	0.260 2	0.071 7	6.034	0.298 8	0.078 6	—	—	—
28	6.107	0.228 9	0.072 6	6.094	0.261 3	0.078 0	6.065	0.298 5	0.084 6	—	—	—
26	6.140	0.231 1	0.079 8	6.132	0.262 7	0.085 7	6.104	0.298 9	0.092 8	6.066	0.342 8	0.102 5
24	6.172	0.233 5	0.087 1	6.166	0.264 3	0.093 1	6.144	0.299 7	0.100 8	6.114	0.341 3	0.110 0
22	6.209	0.236 4	0.095 7	6.206	0.266 6	0.102 5	6.187	0.301 0	0.110 5	6.164	0.341 2	0.119 6
20	6.244	0.239 2	0.105 7	6.240	0.268 9	0.112 9	6.232	0.302 4	0.120 7	6.207	0.340 6	0.129 5
18	6.269	0.242 0	0.115 5	6.263	0.270 8	0.122 4	6.254	0.303 3	0.130 0	6.240	0.340 6	0.139 3
16	6.292	0.245 0	0.126 7	6.284	0.273 2	0.134 0	6.275	0.304 5	0.142 4	6.266	0.339 6	0.152 3
14	6.316	0.249 0	0.140 3	6.302	0.275 9	0.147 3	6.288	0.305 5	0.154 8	6.279	0.338 2	0.164 3
12	6.334	0.253 9	0.156 8	6.318	0.278 9	0.162 3	6.303	0.306 3	0.169 8	6.288	0.337 0	0.179 1
10	6.345	0.258 9	0.173 4	6.332	0.282 1	0.179 9	6.320	0.307 6	0.188 3	6.308	0.335 0	0.197 4
8	6.356	0.265 5	0.194 9	6.345	0.286 6	0.201 1	6.335	0.309 0	0.207 8	6.326	0.332 7	0.216 9
6	6.366	0.273 0	0.218 5	6.357	0.291 4	0.224 4	6.350	0.310 5	0.231 4	6.343	0.329 5	0.239 6
4	6.374	0.283 0	0.246 2	6.368	0.296 9	0.250 2	6.363	0.311 5	0.256 1	6.358	0.325 9	0.262 8
3	6.378	0.288 8	0.262 0	6.373	0.299 9	0.265 0	6.369	0.312 1	0.270 0	6.365	0.323 7	0.275 8
2	6.382	0.295 7	0.280 5	6.379	0.303 3	0.282 3	6.375	0.312 5	0.286 0	6.373	0.320 8	0.290 8
1	6.386	0.303 6	0.302 5	6.384	0.307 6	0.303 3	6.383	0.312 8	0.305 4	6.382	0.317 2	0.308 3
2/30	2.843	0.225 2	0.044 8	—	—	—	—	—	—	—	—	—
28	2.868	0.226 3	0.050 9	2.827	0.261 0	0.055 1	—	—	—	—	—	—
26	2.896	0.228 2	0.057 8	2.854	0.260 5	0.061 8	—	—	—	—	—	—
24	2.922	0.230 4	0.065 0	2.884	0.261 7	0.069 6	2.851	0.293 3	0.074 8	—	—	—
22	2.950	0.233 2	0.073 3	2.916	0.263 6	0.078 4	2.881	0.293 7	0.083 1	2.850	0.330 2	0.089 9
20	2.970	0.235 8	0.082 4	2.948	0.265 9	0.088 1	2.919	0.295 3	0.094 0	2.885	0.329 1	0.100 0
18	2.983	0.238 5	0.092 5	2.971	0.268 5	0.098 6	2.950	0.297 0	0.104 3	2.921	0.329 6	0.110 8
16	2.993	0.241 3	0.103 9	2.985	0.270 6	0.110 4	2.974	0.298 6	0.116 3	2.957	0.330 6	0.123 6
14	3.001	0.244 7	0.116 6	2.994	0.273 0	0.122 8	2.988	0.300 3	0.130 0	2.981	0.330 9	0.138 1
12	3.009	0.249 1	0.131 9	3.002	0.276 2	0.139 2	2.997	0.302 0	0.146 4	2.993	0.330 6	0.154 7
10	3.017	0.254 3	0.150 5	3.010	0.280 0	0.158 0	3.004	0.303 9	0.164 6	2.999	0.329 8	0.173 4
8	3.024	0.261 2	0.172 8	3.019	0.284 1	0.179 7	3.014	0.305 6	0.186 8	3.009	0.328 1	0.194 6
6	3.032	0.270 2	0.202 6	3.027	0.289 7	0.209 4	3.024	0.307 6	0.215 7	3.020	0.326 2	0.222 8
4	3.037	0.279 8	0.232 1	3.034	0.295 2	0.237 1	3.031	0.309 4	0.242 9	3.029	0.323 7	0.249 5
3	3.039	0.285 7	0.249 4	3.037	0.298 3	0.253 3	3.035	0.310 2	0.258 0	3.033	0.322 3	0.263 6
2	3.042	0.292 9	0.270 3	3.040	0.302 2	0.273 0	3.039	0.311 1	0.276 2	3.037	0.320 2	0.280 4
1	3.044	0.301 9	0.296 2	3.044	0.307 0	0.297 5	3.043	0.312 0	0.299 2	3.042	0.317 1	0.301 6

Annex Attached Table 1. (continued)

	2.5P			5P			7.5P			10P		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
1/26	1.090	0.228 7	0.037 2	—	—	—	—	—	—	—	—	—
24	1.098	0.229 6	0.043 7	—	—	—	—	—	—	—	—	—
22	1.113	0.231 3	0.049 8	1.094	0.263 2	0.052 9	—	—	—	—	—	—
20	1.131	0.233 5	0.057 5	1.103	0.264 5	0.061 2	1.093	0.288 5	0.065 1	—	—	—
18	1.143	0.235 7	0.066 0	1.122	0.266 1	0.070 2	1.105	0.289 5	0.073 8	1.094	0.312 5	0.077 6
16	1.149	0.237 7	0.074 4	1.136	0.268 1	0.079 0	1.122	0.291 1	0.083 0	1.110	0.313 8	0.087 5
14	1.154	0.240 8	0.086 6	1.148	0.270 5	0.091 8	1.140	0.293 5	0.095 5	1.129	0.315 2	0.100 0
12	1.158	0.244 1	0.100 3	1.155	0.273 1	0.107 0	1.151	0.295 4	0.112 2	1.147	0.316 9	0.117 1
10	1.162	0.248 8	0.118 3	1.159	0.276 0	0.124 9	1.157	0.297 3	0.130 0	1.155	0.317 6	0.135 1
8	1.165	0.254 2	0.138 0	1.162	0.279 8	0.145 1	1.161	0.299 6	0.150 4	1.159	0.318 4	0.155 5
6	1.169	0.261 6	0.164 4	1.166	0.284 7	0.170 9	1.165	0.301 9	0.176 1	1.163	0.318 9	0.181 3
4	1.172	0.271 3	0.197 1	1.170	0.290 4	0.202 0	1.169	0.304 5	0.206 4	1.168	0.318 9	0.212 0
3	1.174	0.277 0	0.215 3	1.172	0.293 6	0.219 3	1.171	0.305 9	0.223 1	1.170	0.318 7	0.228 2
2	1.175	0.285 0	0.240 3	1.174	0.298 1	0.243 4	1.173	0.307 7	0.246 2	1.173	0.318 0	0.250 3
1	1.177	0.296 7	0.276 3	1.177	0.304 4	0.278 0	1.176	0.310 0	0.279 6	1.176	0.316 3	0.282 0

Annex Attached Table 1. (continued)

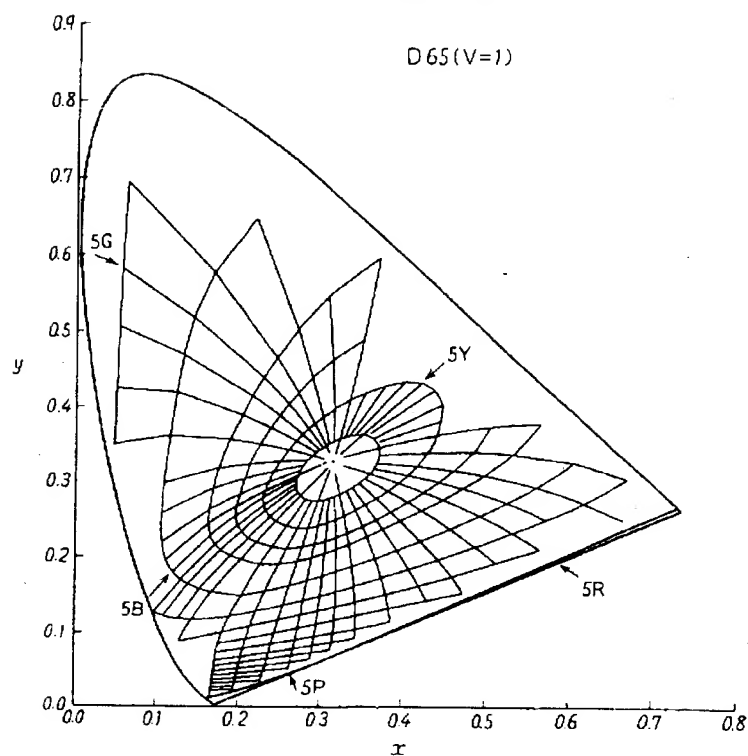
2.5RP				SRP			7.5RP			10RP		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
9/ 6	75.87	0.336 6	0.301 3	75.90	0.347 6	0.309 1	75.86	0.355 8	0.315 4	75.94	0.363 4	0.322 1
4	76.47	0.326 8	0.313 0	76.45	0.333 5	0.317 9	76.45	0.338 4	0.321 7	76.43	0.343 4	0.325 6
3	76.61	0.322 0	0.318 7	76.59	0.326 4	0.321 9	76.58	0.329 6	0.324 5	76.56	0.332 8	0.327 0
2	76.65	0.317 9	0.323 5	76.63	0.320 1	0.325 3	76.62	0.322 0	0.326 7	76.60	0.323 5	0.328 0
1	76.68	0.314 6	0.327 2	76.66	0.315 4	0.327 8	76.65	0.316 0	0.328 3	76.64	0.316 4	0.328 8
8/14	56.21	0.368 6	0.256 8	—	—	—	—	—	—	—	—	—
12	56.50	0.361 1	0.267 6	56.32	0.388 2	0.281 6	56.23	0.406 9	0.293 2	—	—	—
10	56.83	0.353 1	0.279 2	56.80	0.373 8	0.291 8	56.66	0.388 5	0.301 3	56.57	0.403 9	0.312 8
8	57.13	0.345 1	0.289 8	57.10	0.361 5	0.300 1	57.10	0.372 7	0.308 2	57.11	0.384 3	0.317 9
6	57.44	0.336 5	0.301 6	57.43	0.347 7	0.309 3	57.41	0.355 8	0.315 5	57.39	0.363 5	0.322 2
4	57.51	0.327 3	0.312 3	57.50	0.334 1	0.317 3	57.48	0.339 3	0.321 1	57.47	0.344 5	0.325 2
3	57.55	0.322 6	0.317 7	57.53	0.327 2	0.321 2	57.52	0.330 7	0.323 7	57.51	0.334 2	0.326 5
2	57.58	0.318 4	0.322 7	57.56	0.321 0	0.324 6	57.55	0.323 0	0.326 1	57.54	0.324 8	0.327 6
1	57.60	0.315 0	0.326 7	57.59	0.316 0	0.327 4	57.58	0.316 8	0.328 0	57.57	0.317 4	0.328 5
7/20	41.03	0.389 1	0.221 5	—	—	—	—	—	—	—	—	—
18	41.17	0.382 5	0.231 6	41.06	0.427 1	0.253 5	—	—	—	—	—	—
16	41.30	0.375 6	0.242 4	41.20	0.414 8	0.261 5	41.13	0.442 7	0.276 6	41.06	0.473 2	0.295 1
14	41.43	0.368 1	0.253 7	41.40	0.402 1	0.271 1	41.32	0.426 0	0.284 0	41.24	0.452 2	0.300 2
12	41.56	0.361 0	0.264 2	41.54	0.389 6	0.280 2	41.53	0.409 4	0.292 2	41.51	0.431 0	0.306 2
10	41.70	0.353 5	0.275 4	41.70	0.376 0	0.290 0	41.69	0.391 6	0.300 4	41.68	0.408 2	0.312 3
8	41.79	0.346 0	0.285 7	41.77	0.364 6	0.297 7	41.76	0.376 3	0.306 8	41.75	0.389 0	0.316 8
6	41.85	0.337 7	0.297 1	41.83	0.350 8	0.306 3	41.82	0.360 0	0.313 3	41.81	0.368 4	0.320 6
4	41.90	0.328 9	0.309 3	41.89	0.336 6	0.315 1	41.88	0.342 3	0.319 7	41.87	0.347 9	0.324 1
3	41.93	0.324 4	0.314 9	41.92	0.329 9	0.319 2	41.91	0.334 0	0.322 4	41.89	0.338 1	0.325 6
2	41.95	0.320 1	0.320 2	41.94	0.323 7	0.322 9	41.93	0.326 3	0.324 9	41.92	0.328 8	0.327 1
1	41.97	0.316 2	0.325 0	41.96	0.317 9	0.326 2	41.95	0.319 2	0.327 1	41.94	0.320 4	0.328 3
6/24	28.79	0.401 9	0.196 7	—	—	—	—	—	—	—	—	—
22	28.81	0.396 1	0.205 2	28.81	0.454 5	0.229 6	—	—	—	—	—	—
20	28.84	0.391 3	0.213 2	28.84	0.445 3	0.235 6	28.84	0.482 6	0.254 0	—	—	—
18	28.90	0.384 7	0.224 0	28.89	0.431 9	0.245 8	28.88	0.465 3	0.261 9	28.88	0.503 7	0.282 0
16	28.94	0.378 6	0.233 8	28.93	0.420 4	0.254 8	28.92	0.451 2	0.269 7	28.91	0.483 9	0.287 8
14	29.00	0.371 3	0.244 8	28.98	0.408 3	0.263 9	28.97	0.434 2	0.278 6	28.96	0.460 3	0.295 5
12	29.06	0.363 7	0.256 1	29.04	0.395 4	0.274 0	29.03	0.417 7	0.287 2	29.01	0.440 7	0.301 8
10	29.11	0.355 9	0.268 3	29.09	0.381 8	0.283 8	29.08	0.400 7	0.295 5	29.06	0.419 4	0.307 8
8	29.15	0.348 2	0.279 8	29.13	0.369 3	0.292 5	29.12	0.383 4	0.303 1	29.11	0.397 1	0.313 5
6	29.18	0.340 3	0.291 4	29.17	0.356 1	0.301 5	29.16	0.367 5	0.309 5	29.15	0.377 8	0.317 9
4	29.23	0.330 8	0.304 9	29.22	0.340 7	0.311 9	29.21	0.347 4	0.317 1	29.20	0.354 3	0.322 5
3	29.24	0.326 4	0.311 1	29.24	0.333 4	0.316 5	29.23	0.338 1	0.320 5	29.22	0.343 0	0.324 4
2	29.26	0.322 0	0.317 3	29.26	0.326 4	0.320 8	29.25	0.329 2	0.323 5	29.24	0.332 3	0.326 2
1	29.28	0.317 5	0.323 3	29.27	0.319 6	0.325 0	29.27	0.320 9	0.326 5	29.26	0.322 3	0.327 8
5/26	19.01	0.411 8	0.172 9	—	—	—	—	—	—	—	—	—
24	19.00	0.406 2	0.181 0	19.04	0.480 4	0.206 2	—	—	—	—	—	—
22	18.98	0.401 5	0.188 6	19.02	0.467 8	0.213 9	19.04	0.514 1	0.231 8	—	—	—
20	18.96	0.395 5	0.198 2	18.99	0.457 1	0.221 8	19.02	0.499 9	0.239 3	19.04	0.547 9	0.259 8
18	18.97	0.389 6	0.208 4	18.95	0.444 9	0.231 0	18.94	0.483 3	0.248 2	18.97	0.525 2	0.267 3
16	19.00	0.383 3	0.219 0	18.98	0.433 2	0.240 5	18.97	0.468 4	0.257 3	18.96	0.504 5	0.275 2
14	19.04	0.376 8	0.229 8	19.02	0.420 8	0.250 8	19.01	0.451 6	0.267 0	19.00	0.482 2	0.284 2
12	19.08	0.369 5	0.241 8	19.06	0.408 2	0.260 9	19.05	0.436 0	0.275 5	19.04	0.463 1	0.291 4
10	19.11	0.361 5	0.255 2	19.10	0.393 5	0.272 3	19.09	0.416 0	0.286 1	19.08	0.438 0	0.300 0
8	19.14	0.354 0	0.267 5	19.13	0.379 7	0.282 9	19.12	0.397 9	0.294 7	19.12	0.414 9	0.307 0
6	19.18	0.344 0	0.283 0	19.17	0.362 8	0.294 9	19.16	0.376 8	0.304 5	19.15	0.389 1	0.313 9
4	19.21	0.333 6	0.298 7	19.20	0.345 9	0.306 9	19.20	0.355 2	0.313 6	19.19	0.363 0	0.319 9
3	19.23	0.328 4	0.306 5	19.22	0.337 3	0.312 8	19.21	0.344 0	0.317 8	19.21	0.349 5	0.322 6
2	19.24	0.323 2	0.314 2	19.23	0.328 8	0.318 7	19.23	0.332 8	0.321 9	19.22	0.336 4	0.325 0
1	19.25	0.318 0	0.321 8	19.25	0.320 7	0.324 1	19.24	0.322 4	0.325 6	19.24	0.324 0	0.327 2

Annex Attached Table 1. (continued)

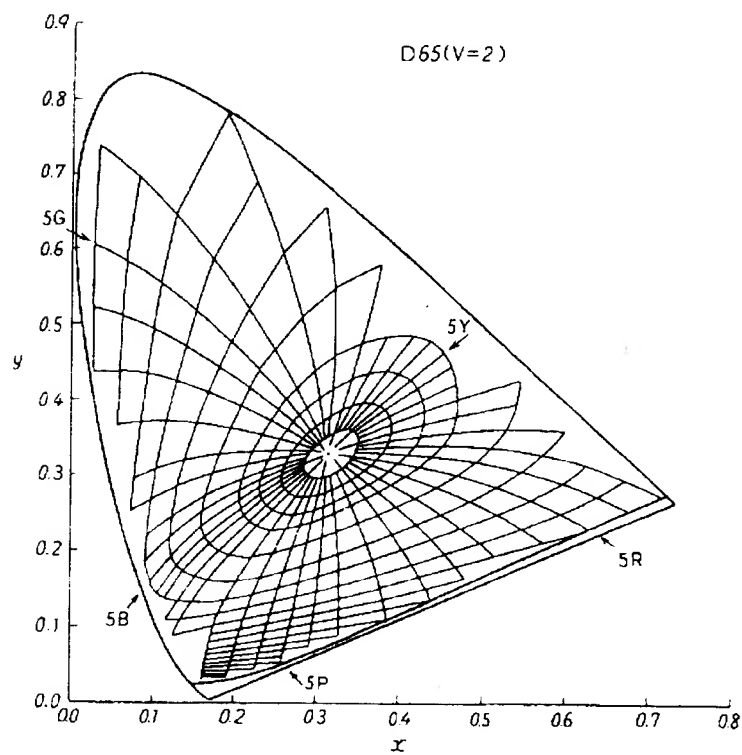
	2.5RP			SRP			7.5RP			10RP		
	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$	$Y_D$	$x_D$	$y_D$
4/26	11.42	0.418 1	0.150 8	—	—	—	—	—	—	—	—	—
24	11.46	0.412 0	0.157 4	—	—	—	—	—	—	—	—	—
22	11.49	0.406 8	0.166 3	11.46	0.477 3	0.189 5	—	—	—	—	—	—
20	11.51	0.402 2	0.174 9	11.51	0.467 3	0.197 5	11.49	0.523 1	0.216 7	11.47	0.576 9	0.238 0
18	11.51	0.395 2	0.187 4	11.53	0.454 8	0.209 1	11.53	0.505 4	0.228 0	11.54	0.554 3	0.247 8
16	11.51	0.388 5	0.199 6	11.51	0.442 2	0.220 7	11.53	0.488 0	0.239 1	11.54	0.530 5	0.258 4
14	11.53	0.382 0	0.211 8	11.52	0.429 9	0.232 1	11.51	0.469 9	0.250 1	11.50	0.508 3	0.267 8
12	11.56	0.374 9	0.224 8	11.54	0.417 1	0.244 0	11.54	0.451 4	0.261 3	11.53	0.484 7	0.278 1
10	11.58	0.366 8	0.239 4	11.57	0.402 1	0.257 6	11.56	0.431 7	0.273 2	11.56	0.458 1	0.288 4
8	11.60	0.358 8	0.253 7	11.60	0.388 8	0.269 4	11.59	0.412 4	0.283 8	11.58	0.433 1	0.297 3
6	11.63	0.349 0	0.270 2	11.62	0.371 9	0.283 5	11.62	0.389 6	0.295 7	11.61	0.404 3	0.306 5
4	11.65	0.338 2	0.288 4	11.65	0.353 2	0.298 2	11.64	0.365 2	0.307 0	11.64	0.375 4	0.314 6
3	11.66	0.332 5	0.297 5	11.66	0.344 0	0.305 4	11.65	0.353 2	0.312 4	11.65	0.360 5	0.318 4
2	11.67	0.326 6	0.307 2	11.67	0.334 5	0.312 9	11.67	0.340 6	0.317 8	11.66	0.345 1	0.322 1
1	11.69	0.320 2	0.317 6	11.68	0.324 3	0.320 7	11.68	0.327 3	0.323 3	11.67	0.329 4	0.325 6
3/22	6.081	0.411 1	0.135 4	—	—	—	—	—	—	—	—	—
20	6.151	0.405 0	0.146 4	6.101	0.467 9	0.164 9	—	—	—	—	—	—
18	6.205	0.401 2	0.156 3	6.175	0.459 3	0.175 1	6.114	0.522 4	0.194 6	—	—	—
16	6.253	0.396 1	0.169 3	6.240	0.450 8	0.187 0	6.208	0.507 4	0.206 5	6.165	0.569 8	0.228 5
14	6.279	0.390 1	0.182 7	6.278	0.440 1	0.201 1	6.267	0.491 4	0.219 9	6.256	0.545 0	0.241 8
12	6.286	0.383 1	0.197 1	6.286	0.427 9	0.215 8	6.287	0.473 3	0.233 6	6.287	0.520 9	0.254 2
10	6.302	0.375 1	0.213 5	6.297	0.414 5	0.231 1	6.293	0.451 4	0.248 8	6.286	0.491 4	0.267 7
8	6.321	0.366 0	0.232 3	6.316	0.399 3	0.248 0	6.311	0.429 6	0.263 4	6.306	0.460 9	0.281 1
6	6.339	0.355 5	0.252 4	6.334	0.382 0	0.266 3	6.330	0.404 3	0.279 7	6.326	0.426 8	0.294 7
4	6.354	0.344 7	0.273 1	6.351	0.363 3	0.284 5	6.347	0.378 5	0.295 0	6.344	0.393 3	0.306 4
3	6.362	0.338 3	0.284 8	6.359	0.352 7	0.294 6	6.356	0.364 3	0.303 0	6.352	0.375 5	0.312 1
2	6.371	0.331 0	0.297 7	6.368	0.340 8	0.305 4	6.365	0.348 8	0.311 2	6.361	0.356 3	0.317 7
1	6.379	0.322 6	0.312 3	6.376	0.327 6	0.316 7	6.374	0.331 8	0.319 8	6.371	0.335 7	0.323 2
2/20	2.851	0.383 9	0.109 8	—	—	—	—	—	—	—	—	—
18	2.879	0.385 3	0.123 1	2.853	0.437 7	0.135 9	—	—	—	—	—	—
16	2.921	0.382 1	0.135 9	2.888	0.434 7	0.150 0	2.863	0.482 9	0.163 9	—	—	—
14	2.965	0.379 2	0.151 0	2.941	0.425 9	0.165 3	2.918	0.469 8	0.178 5	2.894	0.519 9	0.193 0
12	2.989	0.375 0	0.168 7	2.983	0.416 4	0.183 0	2.972	0.456 2	0.196 3	2.959	0.498 5	0.211 3
10	2.998	0.369 3	0.187 4	2.997	0.405 1	0.201 0	2.995	0.440 1	0.214 9	2.992	0.475 4	0.229 8
8	3.006	0.362 3	0.208 4	3.004	0.392 9	0.221 7	3.002	0.420 8	0.234 8	3.000	0.449 7	0.248 5
6	3.018	0.352 9	0.235 1	3.016	0.376 8	0.246 8	3.013	0.397 8	0.257 4	3.011	0.419 8	0.268 7
4	3.027	0.343 2	0.259 8	3.024	0.360 9	0.269 5	3.022	0.375 3	0.277 8	3.020	0.390 1	0.286 8
3	3.031	0.338 2	0.272 0	3.028	0.352 6	0.280 9	3.026	0.363 6	0.288 3	3.024	0.374 7	0.296 2
2	3.035	0.332 1	0.286 4	3.033	0.342 5	0.293 7	3.031	0.350 1	0.299 8	3.029	0.357 4	0.306 0
1	3.040	0.323 9	0.304 8	3.038	0.329 8	0.309 2	3.036	0.333 7	0.312 9	3.034	0.337 3	0.316 7
1/16	1.093	0.342 1	0.092 9	—	—	—	—	—	—	—	—	—
14	1.117	0.343 5	0.106 2	1.097	0.387 2	0.117 1	—	—	—	—	—	—
12	1.140	0.343 9	0.124 0	1.125	0.384 7	0.133 3	1.109	0.431 2	0.144 2	1.093	0.472 6	0.154 4
10	1.152	0.343 4	0.142 0	1.146	0.381 1	0.152 4	1.137	0.421 4	0.164 0	1.129	0.459 8	0.176 3
8	1.159	0.341 8	0.162 6	1.157	0.374 1	0.173 5	1.154	0.408 8	0.186 3	1.150	0.443 9	0.198 7
6	1.162	0.338 9	0.188 6	1.161	0.366 1	0.199 4	1.160	0.394 1	0.210 7	1.158	0.422 7	0.223 7
4	1.167	0.335 0	0.218 0	1.165	0.356 7	0.227 8	1.164	0.377 1	0.237 7	1.162	0.398 7	0.249 5
3	1.169	0.332 8	0.234 1	1.167	0.351 2	0.243 4	1.166	0.367 6	0.252 4	1.164	0.385 4	0.263 2
2	1.171	0.329 0	0.255 5	1.170	0.343 0	0.263 4	1.168	0.355 2	0.270 6	1.166	0.368 4	0.279 5
1	1.174	0.322 9	0.285 4	1.172	0.331 0	0.290 4	1.171	0.337 8	0.294 7	1.169	0.345 3	0.300 0



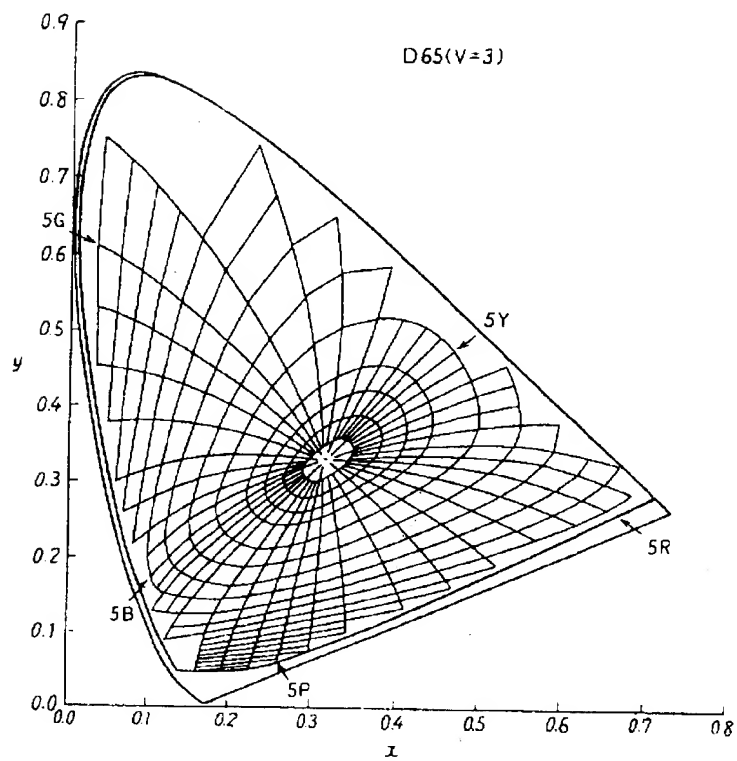
Annex Attached Fig. 1



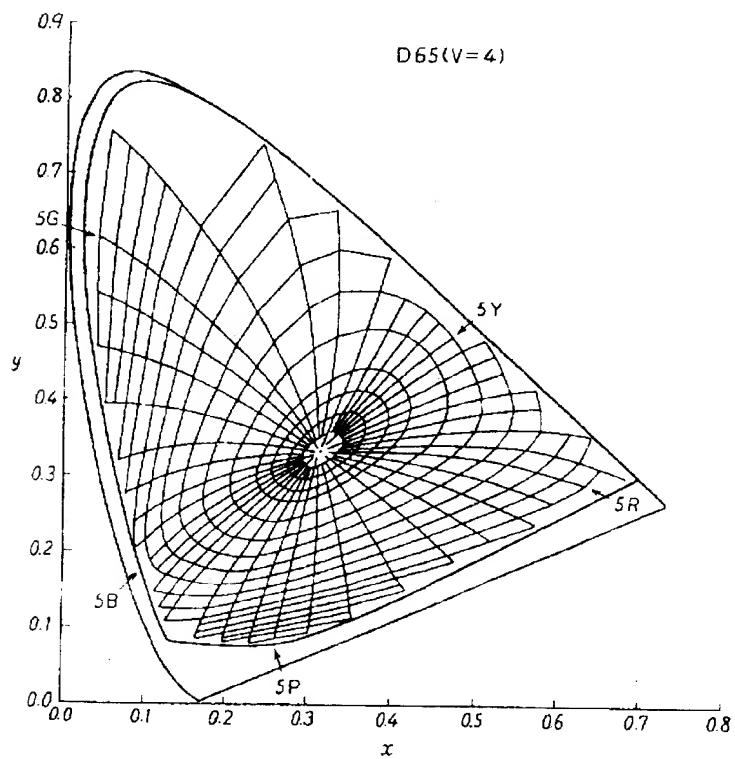
Annex Attached Fig. 2



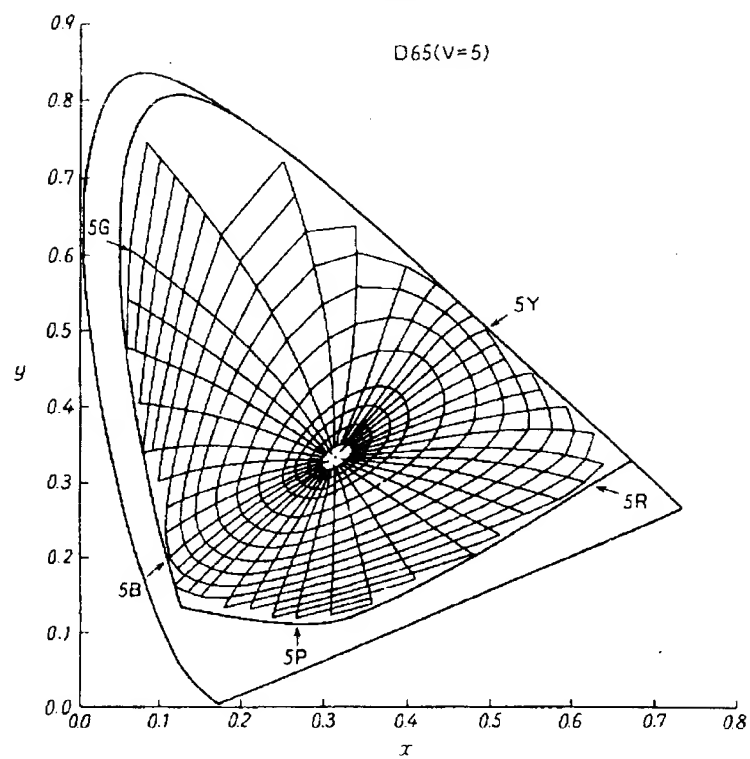
Annex Attached Fig. 3



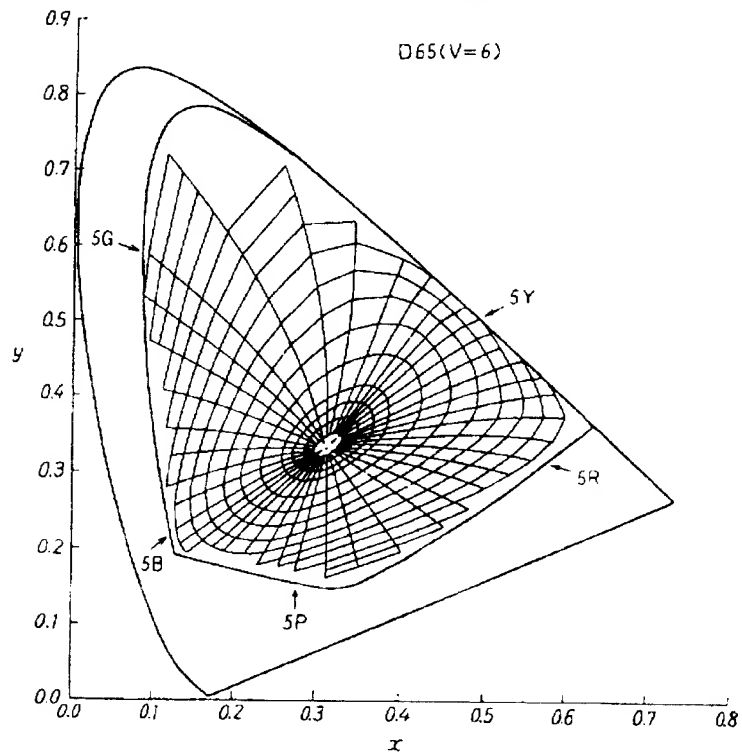
Annex Attached Fig. 4



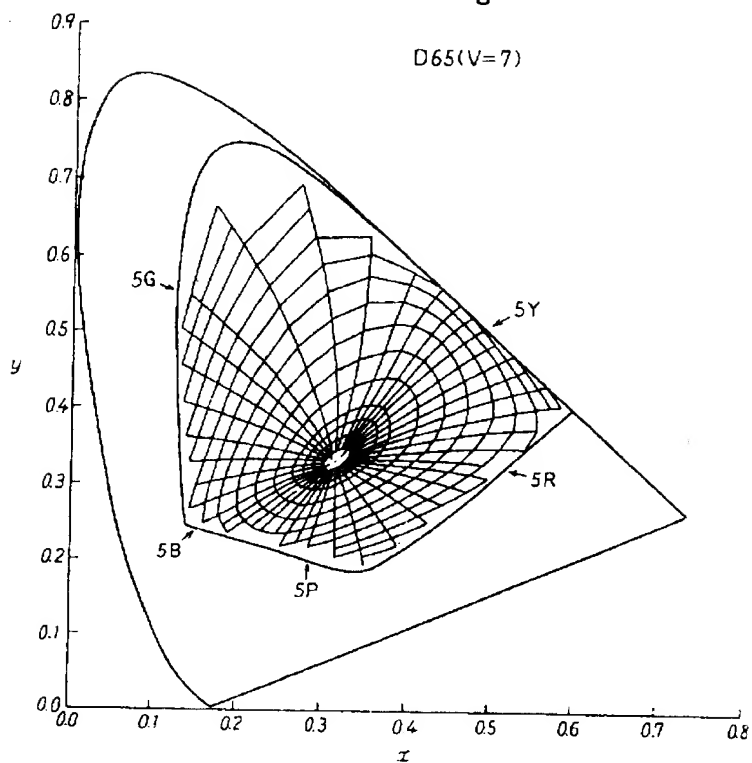
Annex Attached Fig. 5



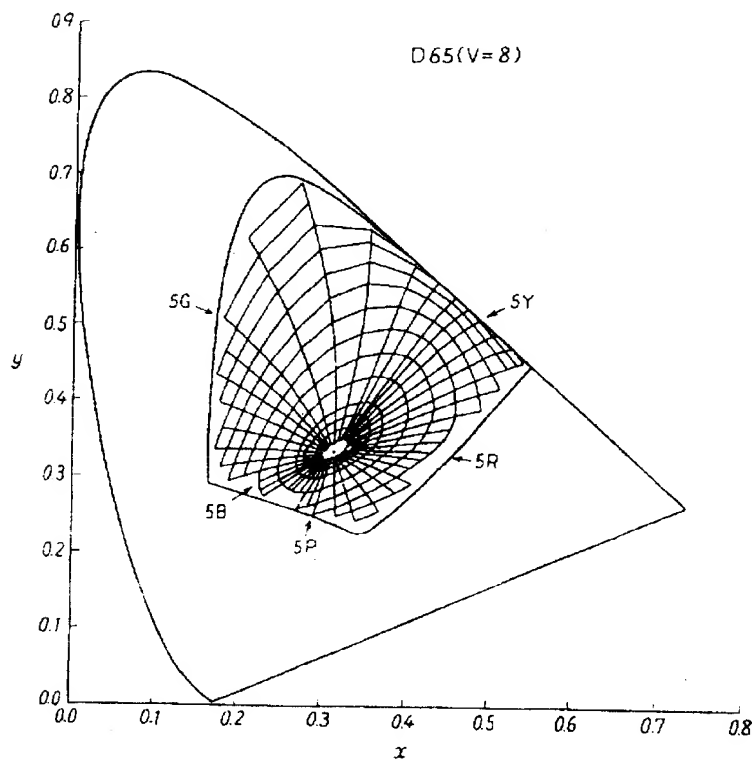
Annex Attached Fig. 6



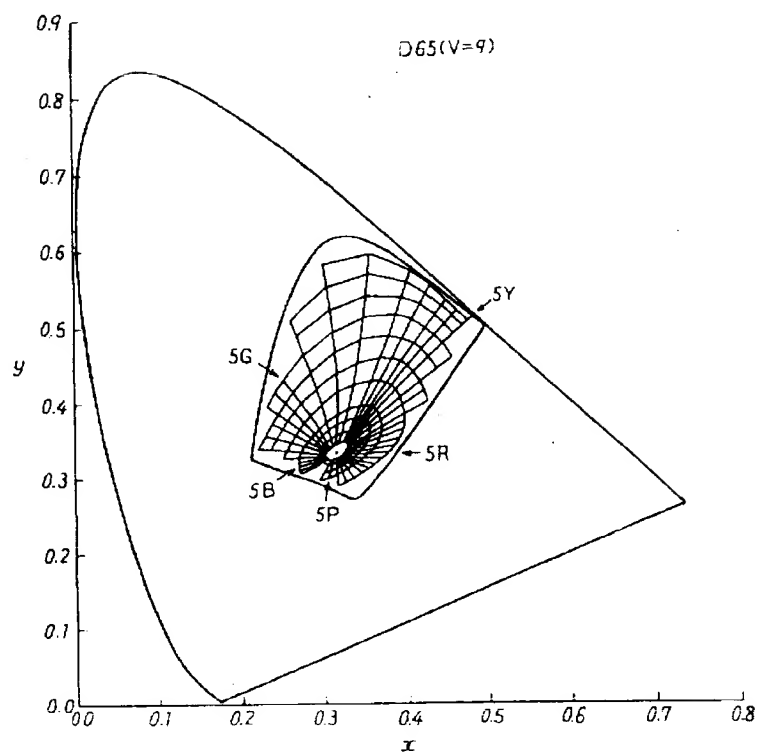
Annex Attached Fig. 7



Annex Attached Fig. 8



Annex Attached Fig. 9



Informative reference 1. Determination of notation for colour specification under standard illuminant C

Preface This Informative reference is to describe examples of methods to obtain the notation for colour specification  $H_c$ ,  $V_c$  and  $C_c$  (hereafter the suffixes are omitted) from the luminance factor  $Y_c$  and chromaticity coordinates  $x_c$ ,  $y_c$  (hereafter the suffixes are omitted) by using the Attached Table 1 and Attached Table 2 of this Standard and does not form a part of the standard.

The examples shown below are described about the search of the chromaticity coordinates in Attached Table 1 composing a quadrangle which surrounds the chromaticity coordinates  $x$ ,  $y$  of the sample colour and about the subroutine subprogram in accordance with JIS X 3003 to obtain the hue  $H$  and chroma  $C$  of the sample colour from the values of its coordinates by the linear interpolation. The notation for colour specification can be determined by citing this subroutine by means of GOSUB sentence after calculating the chromaticity coordinates and the value  $V$  by the main program or another subprogram.

Besides, the value  $V$  of the sample colour to be used shall be the value obtained by calculating directly by using the formula in the remarks of Attached Table 1 from luminance factor  $Y$  of the sample colour.

1. Method for searching chromaticity coordinates forming a quadrangle which surrounds chromaticity coordinates  $x$ ,  $y$  of sample colour As the methods for searching chromaticity coordinates forming a quadrangle which surrounds chromaticity coordinates  $x$ ,  $y$  (hereafter referred to as chromaticity coordinates. See Informative reference 1 Fig. 1), the method by vector product, the method by interior division ratio, the method by polar coordinates, etc. are known. An example of searching by the use of vector is shown here.

The chromaticity coordinates exist on two integer value planes adjacent to the value  $V$  of sample colour (in accordance with Attached Table 1), so that the search of chromaticity coordinates is necessary to be carried out respectively on both planes of high value side and low value side adjacent to each other.

2. Method for obtaining hue  $H$  and chroma  $C$  of sample colour The hue  $H$  and the chroma  $C$  of sample colour can be determined by an interpolation method from the searched chromaticity coordinates. As for the interpolation method, some methods are proposed according to the degree of the interpolation or the interpolation space. An example of utilizing the linear interpolation based on the interior division ratio  $m$  and  $n$  in  $x$   $y$  plane is shown here.

The hue  $H$  and the chroma  $C$  of the sample colour are determined from the value  $V$  of the sample colour by interpolating, by the following formula,  $H$  and  $C$  obtained by the interpolation from the chromaticity coordinates of the value plane adjacent to the value  $V$  of the sample colour:

$$H = H_i + k(H_s - H_i) \dots\dots\dots (1)$$

$$C = C_i + k(C_s - C_i) \dots\dots\dots (2)$$

$$k = (V - V_i) / (V_s - V_i) \dots\dots\dots (3)$$

where,  $H$  : hue of the sample colour

$C$  : chroma of the sample colour

$V$  : value of the sample colour

$H_h, C_h$  : hue and chroma obtained by interpolation from chromaticity coordinates of the integer value plane on high value side adjacent to value of the sample colour.

$H_l, C_l$  : hue and chroma obtained by interpolation from chromaticity coordinates of value plane on low value side adjacent to value of the sample colour

3. Subroutine subprogram The numerical values in Attached Table 1 are read in the main program in compliance with the value  $V$  of the sample colour by an appropriate method and transferred to this subroutine.

In this subroutine, the relation between the name of variable that appears as dummy argument and the symbols in Informative reference 1 Attached Fig. 1 is as follows:

$SX, SY$  : chromaticity coordinates of sample colour P

$X1, X2, X3, X4$  : values of  $x$  in chromaticity coordinates  $x, y$  of points A, B, C, D

$Y1, Y2, Y3, Y4$  : values of  $y$  in chromaticity coordinates  $x, y$  of points A, B, C, D

$H1, H2$  : straight line AB and straight line CD indicating constant hue line

when giving hue number so as to be in sequence from  $10RP = 0$  to  $7.5RP = 39, H1 < H2$

$C1, C2$  : straight line AC and straight line BD indicating constant chroma line

chroma of  $C1$  and  $C2, C1 < C2$

$M$  : interior division ratio used for interpolation of chroma

$N$  : interior division ratio used for interpolation of hue

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```
10000 REM *** search ***
10010 REM *** zero correction ***
10020 DEF FNZC(X) = X - (X = 0) * 1E-10
10030 REM *** comparison of P (SX, SY) with C2 ***
10040 LET XD = X2 - X4
10050 LET XD = FNZC(XD)
10060 LET A1 = (Y2 - Y4) / XD
10070 LET B1 = (X2 * Y4 - X4 * Y2) / XD
10080 LET YD = SY - (A1 * SY + B1)
10090 IF XD * YD > 0 THEN 10110
10100 IF XD * YD <= 0 THEN 10130
10110 LET F1 = 0
10120 GOTO 10140
10130 LET F1 = 1
10140 REM *** comparison of P(SX, SY) with H2 ***
10150 LET XD = X3 - X4
10160 LET XD = FNZC(XD)
10170 LET A3 = (Y3 - Y4) / XD
10180 LET B3 = (X3 * Y4 - X4 * Y3) / XD
10190 LET YD = SY - (A3 * SX + B3)
10200 IF XD * YD < 0 THEN 10220
10210 IF XD * YD >= 0 THEN 10240
10220 LET F2 = 0
10230 GOTO 10250
10240 LET F2 = 1
10250 REM *** decision ***
10260 IF F1 = 1 AND F2 = 1 THEN 10280
10270 IF F1 < 1 OR F2 < 1 THEN 10300
10280 PRINT "CONTAINED"
10290 GOTO 10310
10300 PRINT "NOT CONTAINED"
10310 RETURN
20000 REM *** calculation of interior division ratio m, n ***
```

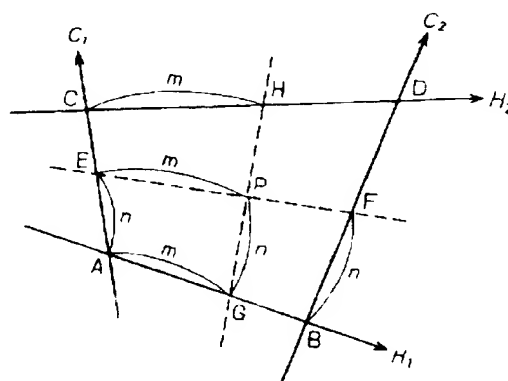


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20010 REM *** calculation of interior division ratio m ***
20020 LET E1=X1-SX
20030 LET E2=X2-X1
20040 LET E3=X3-X1
20050 LET E4=X4-X3-X2+X1
20060 LET E5=Y1-SY
20070 LET E6=Y2-Y1
20080 LET E7=Y3-Y1
20090 LET E8=Y4-Y3-Y2+Y1
20100 LET BB1=E2*E8-E4*E6
20110 LET BB1=FNZC(BB1)
20120 LET BB2=E1*E8+E2*E7-E3*E6-E4*E5
20130 LET BB3=E1*E7-E3*E5
20140 LET D=BB2*BB2-4*BB1*BB3
20150 LET M=INT((-BB2+D0.5)/2/BB1*10000+0.5)/10000
20160 REM *** calculation of interior division ratio n ***
20170 LET BB1=E3+M*E4
20180 LET BB1=FNZC(BB1)
20190 LET N=INT(-(E1+M*E2)/BB1*10000+0.5)/10000
20200 REM *** interpolation of hue ***
20210 LET HH=H1+1.0*N
20220 REM *** interpolation of chroma ***
20230 LET CC=C1+2.0*M
20240 RETURN

```

Informative reference 1 Fig. 1.  
Relation between locations of chromaticity coordinates



Informative reference 2.  
Determination of notation for colour specification  
under standard illuminant D<sub>65</sub>

**Preface** This informative reference is to describe the examples of methods to obtain the notation for colour specification  $H_D$ ,  $V_D$  and  $C_D$  from the luminance factor  $Y_D$  and chromaticity coordinates  $x_D$ ,  $y_D$  by using Annex Attached Table 1 of this Standard and does not form a part of the standard.

In the bases of the colour system under the standard illuminant D<sub>65</sub>, the luminance factor  $Y_D$  may differ when the hue  $H_D$  or the chroma  $V_D$  differs, even if the value  $C_D$  is the same. There are both cases where the variation of luminance factor  $Y_D$  maybe ignored and shall be taken into account and in the latter case, the interpolation method cannot be applied as it is under the illuminant C.

An example of determination of the symbol for colour specification taking into account the variation of luminance factor  $Y_D$  on the constant value plane is shown below:

1. Method for obtaining hue  $H_D$  and chroma  $C_D$  of sample colour The method for obtaining hue  $H_D$  and chroma  $C_D$  is composed of search and interpolation as under the illuminant C. In the search, the variation of luminance factor  $Y_D$  is ignored and the judgment is given to the chromaticity coordinates  $x_D$ ,  $y_D$  by the method shown in Informative reference 1.

Besides, the interpolation for hue  $H_D$  and chroma  $C_D$  is carried out in the same way.

2. Method for obtaining value  $V_D$  of sample colour As for the lightness function for obtaining the value  $V_D$  from the luminance factor  $Y_D$ , the CIE 1976 lightness function is applied by defining its parameters divisionally in compliance with each part of lightness as shown below.

$$V_D = a \left( \frac{Y_D}{Y_n} \right)^{\frac{1}{3}} - b \dots\dots\dots (1)$$

where,  $a = \frac{(V_h - V_l)}{(A_h - A_l)}$

$$b = \frac{(V_h A_l - V_l A_h)}{(A_h - A_l)}$$

$$A_l = \left( \frac{Y_l}{Y_n} \right)^{\frac{1}{3}}$$

$$A_h = \left( \frac{Y_h}{Y_n} \right)^{\frac{1}{3}}$$

In the case  $\frac{Y_D}{Y_n}$  is not more than 0.008856, the formula (2) is used instead of the formula(1).

$$V_o = a \left( \frac{Y}{Y_n} \right) - b \quad \dots \dots \dots (2)$$

where,

$$a = \frac{(V_h - V_l)}{(A_h - A_l)}$$

$$b = \frac{(V_h A_l - V_l A_h)}{(A_h - A_l)}$$

$$A_l = \frac{Y_l}{Y_n}$$

$$A_h = \frac{Y_h}{Y_n}$$

In this case,  $Y_n$  is the luminance factor  $Y_o$  of the perfect reflecting diffuser.

Here,  $V_l$ ,  $V_h$  and  $Y_l$ ,  $Y_h$  are the values, of two values  $V_o$  on the lower and higher levels between which the sample colour is put, and of luminance factor  $Y_o$  corresponding to them.

$V_l$  and  $V_h$  are obtained by the following formula (3).

$$V_l = \text{INT} (V') \quad \dots \dots \dots (3)$$

$$V_h = V_l + 1$$

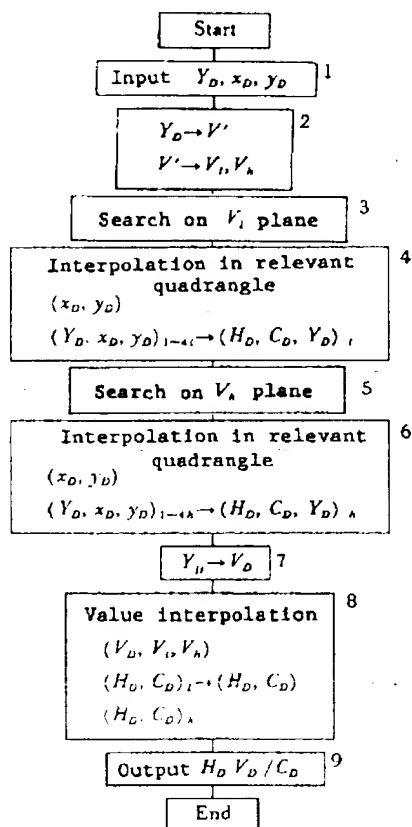
where,

$$V' = 11.6 \left( \frac{Y_o}{Y_n} \right)^{\frac{1}{3}} - 1.6$$

In this case,  $\text{INT} (V')$  gives only integer part of  $V'$ .

3. Example of program A flow chart for obtaining the symbol specification is shown in Informative reference 2 Fig. 1.

Informative reference 2 Fig. 1.  
A flow chart for obtaining the symbol specification



When luminance factor  $Y_D$  and chromaticity coordinates  $x_D$  and  $y_D$  of the sample colour are given (step 1) after the basis value data of colour system are read in, the two values of  $V_l$  and  $V_h$  between which the sample colour is put, (step 2) shall be at first determined by using the formula (3). Then, search on the value  $V_l$  plane (step 3) and do the interpolation in the relevant quadrangle (step 4).

It shall be noted that not only the interpolated values  $H_l$  and  $C_l$  of the hue and chroma corresponding to the sample colour on the value  $V_l$  plane are obtained but also the interpolated value of  $Y_l$  of luminance factor is obtained by using the same interpolation ratio.

Repeat the above steps as well with respect to the value  $V_h$  plane (steps 5 and 6).

Substitute  $V_l$ ,  $V_h$  and  $Y_l$ ,  $Y_h$  thus obtained for the relevant values in the formula (1) or (2) to determine the lightness function and convert  $Y_D$  of luminance factor of sample colour to the value  $V_D$  (step 7). Carry out the value interpolation for the hue  $H_l$  and  $H_h$  and the chroma  $C_l$  and  $C_h$  on the value  $V_l$  and  $V_h$  planes, by using the value of this value  $V_D$  [formulas (1), (2) and (3) in Informative reference 1] and obtain the final hue  $H_D$  and chroma  $C_D$  (step 8).

Z 8721-1993  
Edition 1

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**Japanese Text**

Established by Minister of International Trade and Industry

Date of Establishment: 1958-03-29

Date of Revision: 1993-02-01

Date of Public Notice in Official Gazette: 1993-02-19

Investigated by: Japanese Industrial Standards Committee

Divisional Council on Basic Items

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This English translation is published by:  
Japanese Standards Association  
1-24, Akasaka 4, Minato-ku,  
Tokyo 107 Japan  
© JSA, 1995

Printed in Tokyo by  
Hohbunsha Co., Ltd.